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Appendices

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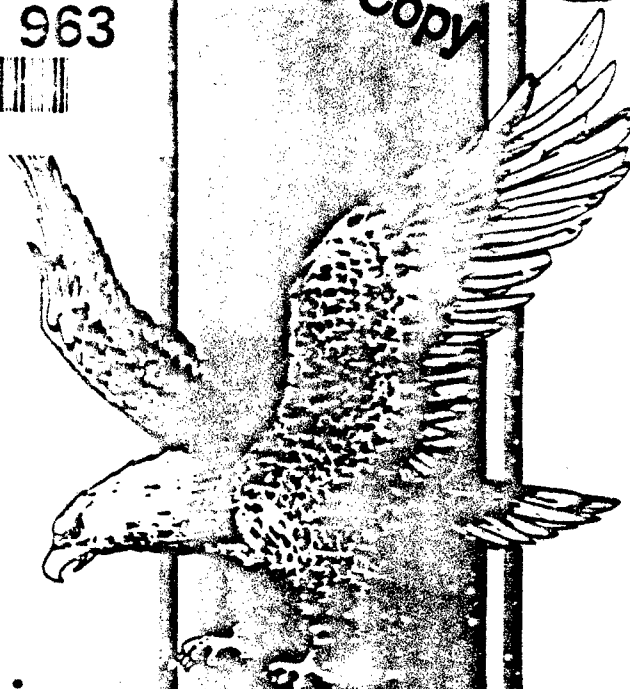


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# USATHAMA

U.S. Army Toxic and Hazardous Materials Agency



Task Order - 2  
Pilot Test of Hot Gas  
Decontamination of Explosives-  
Contaminated Equipment at  
Hawthorne Army Ammunition  
Plant (HWAAP)  
Hawthorne, Nevada

Report No. CETHA-TE-CR-90036

July 1990

20030204163

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## INTRODUCTION TO APPENDICES

The following appendices are included in this report:

- Appendix A - Description of Spiking Procedures
- Appendix B - Sampling and Analytical Methods
- Appendix C - Description of CEM System
- Appendix D - Raw Operational Data Sheets
- Appendix E - Hourly Averages for CEM System Data
- Appendix F - Raw Analytical Data Sheets for Test Items
- Appendix G - Analytical Data Summary Tables for Stack Test Program
- Appendix H - Analytical Data Summary Tables for Test Items
- Appendix I - Example Calculations

Breaker pages are provided to identify each appendix listed above. A brief summary is included at the beginning of each appendix describing the contents.

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**APPENDIX A**  
**DESCRIPTION OF SPIKING PROCEDURES**

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## A. Description of Spiking Procedures

A description of the spiking procedures is discussed in the following subsections. Sparkless equipment was used when preparing and applying the spike solutions. WESTON personnel, in conjunction with HWAAP laboratory personnel, prepared the liquid spike solutions. HWAAP laboratory personnel prepared the paste spike solutions. HWAAP laboratory personnel applied all spike liquid/paste solutions.

A.1 TNT spiking procedures. A homogenous liquid solution (i.e., no solid TNT) was used to spike the following items of equipment:

- o powder boxes
- o steam-heated risers
- o steam-heated discharge valves
- o steel pipe
- o aluminum pipe

Prior to spiking, a batch solution was made to spike all test equipment. One hundred grams of TNT were added to 250 mL of acetone; 25 mL of the homogenous solution were added to the test equipment outlined above (using a pipet). After adding the solution to the equipment, the pipet was flushed with acetonitrile to remove residual TNT. The rinsate was added to the equipment. This resulted in a spike of 10 grams of TNT for each piece of equipment.

The liquid spike solution was added directly into the powder boxes. The boxes were agitated to swirl the liquid, exposing it to the internal surfaces. Holes or cracks in the powder boxes were plugged with parafilm wax.

For steam-heated vessels (risers and discharge valves), the bottom steam connection was covered with parafilm wax. Although it was originally planned to use rubber stoppers, parafilm was used to avoid potential analytical interference associated with rubber products. The spike solution was added to the upper steam connection. The vessel was agitated to swirl the liquid and expose it to the internal surfaces.

For pipe (aluminum and steel), one end of the pipe section was covered with parafilm wax. Spike solution was added into the open end of the pipe. The pipe was agitated to swirl the liquid, exposing it to the internal surfaces.

A heterogenous mixture (i.e., a workable paste) was used to spike the support racks for shells. For the TNT spike, 1 gram of TNT was mixed with about 0.8 mL of acetone. Although it was originally planned to spike shell support racks with 10 grams of TNT, field operations indicated that 1 gram was sufficient to cover the spike area (4 inches by 4 inches) adequately. The mixing container and applicator (spatula) were rinsed with about

50 mL acetonitrile. The rinsate was collected for analysis to determine the amount of TNT that adhered to the container and applicator.

The spiked equipment was placed on the loading dock of Building 117-15 and allowed to air dry.

A.2 Ammonium picrate spiking procedures. A homogenous liquid solution (i.e., no solid ammonium picrate) was used to spike the following items of equipment:

- o powder box
- o steam-heated riser
- o steam-heated discharge valve
- o steel pipe
- o aluminum pipe

Prior to spiking, a batch solution was made to spike all test equipment. Forty grams of ammonium picrate were added to 2400 mL of acetone; 300 mL of the homogenous solution were added to the test equipment outlined above (using a pipet). After adding the solution to the equipment, the pipet was flushed with water to remove residual ammonium picrate. The rinsate was added to the equipment. This resulted in a spike of 5 grams of ammonium picrate for each piece of equipment.

The procedures for spiking with ammonium picrate are the same as those used for spiking with TNT (for each type of equipment).

A.3 Spike recovery procedures. As outlined in the Test Plan, it was originally planned to conduct spike recovery tests. Selected pieces of test equipment were to be spiked with TNT and ammonium picrate. The spiked equipment was to be sampled (wipe samples or rinsates) to determine the efficiency of the sampling methods. During spiking activities, however, it was determined that it would never be possible to fully recover the TNT or ammonium picrate spiked on the equipment. Residual levels of explosives on the parafilm, steam connections, etc. interfered with recovery. Therefore, based on conversations with USATHAMA personnel, it was decided to conduct multiple rinses on the treated test equipment rather than on spiked equipment. Treated equipment was sampled using a series of four rinses.

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**APPENDIX B**  
**SAMPLING AND ANALYTICAL METHODS**

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Appendix B provides a description of the following Sampling and Analytical Methods:

- EPA Method 1 - Sample and velocity traverses for stationary sources. (Page B-1)
- EPA Method 2 - Determination of stack gas velocity and volumetric flow rate. (Page B-5)
- EPA Method 25A - Determination of total gaseous organic concentration using a flame ionization analyzer. (Page B-17)
- EPA Method 3 - Gas analysis for carbon dioxide, oxygen, excess air, and dry molecular weight. (Page B-19)
- EPA Method 10 - Determination of carbon monoxide emissions from stationary sources. (Page B-21)
- EPA Method 4 - Determination of moisture content in stack gases. (B-25)
- EPA Wipe Sampling Technique (Page B-29)
- Modified Method LW02 - Analysis of explosives in soil, wipe, and rinsate samples. (Page B-33)
- Modified Method for nitrocellulose, nitroglycerin, and PETN in water. (Page B-45)
- Ammonium Picrate in water and wipe samples by high performance liquid chromatography. (Page B-49)
- EPA Modified Method 5 - Modified method 5 sampling train. (Page B-55)
- EPA Method 5 - Determination of particulate emissions from stationary sources. (Page B-105)
- EPA Method 3A - Determination of oxygen and carbon dioxide concentrations in emissions from stationary sources. (Page B-119)
- EPA Method 7E - Determination of nitrogen oxide emissions from stationary sources. (Page B-123)

Section 7 of the main report provides a summary of the sampling and analytical methods used to evaluate test items and air samples. The locations of the sampling points are shown in Figure 7-1 of the main report. A summary of the analytical parameters associated with each point is presented in Table 7-1 of the main report.

July 1990  
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**EPA METHOD 1**  
**SAMPLE AND VELOCITY TRAVERSES FOR STATIONARY SOURCES**



# METHOD 1—SAMPLE AND VELOCITY TRAVERSES FOR STATIONARY SOURCES

## 1. Principle and Applicability

1.1 Principle. To aid in the representative measurement of pollutant emissions and/or total volumetric flow rate from a stationary source, a measurement site where the effluent stream is flowing in a known direction is selected, and the cross-section of the stack is divided into a number of equal areas. A traverse point is then located within each of these equal areas.

1.2 Applicability. This method is applicable to flowing gas streams in ducts, stacks, and flues. The method cannot be used when: (1) flow is cyclonic or swirling (see Section 2.4); (2) a stack is smaller than about 0.30 meter (12 in.) in diameter, or 0.071 m<sup>2</sup> (113 in.<sup>2</sup>) cross-sectional area, or (3) the measurement site is less than two stack or duct diameters downstream or less than a half diameter upstream from a flow disturbance.

The requirements of this method must be considered before construction of a new facility from which emissions will be measured; failure to do so may require subsequent alterations to the stack or deviation from the standard procedure. Cases involving variants are subject to approval by the Administrator, U.S. Environmental Protection Agency.

## 2. Procedure

2.1 Selection of Measurement Site. Sampling or velocity measurement is performed at a site located at least eight stack or duct diameters downstream and two diameters upstream from any flow disturbance such as a bend, expansion, or contraction in the stack, or from a visible flame. If necessary, an alternative location may be selected, at a position at least two stack or duct diameters downstream and a half diameter upstream from any flow disturbance. For a rectangular cross section, an equivalent diameter ( $D_e$ ) shall be calculated from the following equation, to determine the upstream and downstream distances:

$$D_e = \frac{2LW}{L+W}$$

where  $L$  = length and  $W$  = width.

An alternative procedure is available for determining the acceptability of a measurement location not meeting the criteria above. This procedure, determination of gas flow angles at the sampling points and comparing the results with acceptability criteria, is described in Section 2.5.

## 2.2 Determining the Number of Traverse Points

2.2.1 Particulate Traverses. When the eight- and two-diameter criterion can be met, the minimum number of traverse points shall be: (1) twelve, for circular or rectangular stacks with diameters (or equivalent diameters) greater than 0.61 meter (24 in.); (2) eight, for circular stacks with diameters between 0.30 and 0.61 meter (12-24 in.); (3) nine, for rectangular stacks with equivalent diameters between 0.30 and 0.61 meter (12-24 in.).

When the eight- and two-diameter criterion cannot be met, the minimum number of traverse points is determined from Figure 1-1. Before referring to the figure, however, determine the distances from the chosen

measurement site to the nearest upstream and downstream disturbances, and divide each distance by the stack diameter or equivalent diameter, to determine the distance in terms of the number of duct diameters. Then, determine from Figure 1-1 the minimum number of traverse points that corresponds: (1) to the number of duct diameters upstream, and (2) to the number of diameters downstream. Select the higher of the two minimum numbers of traverse points, or a greater value, so that for circular stacks the number is a multiple of 4, and for rectangular stacks, the number is one of those shown in Table 1-1.

TABLE 1-1 CROSS-SECTION LAYOUT FOR RECTANGULAR STACKS

Number of Traverse Points	Minimum Distance (m)
8	7.62
12	11.43
16	15.24
20	19.05
24	22.86
28	26.67
32	30.48
36	34.29
40	38.10
44	41.91
48	45.72

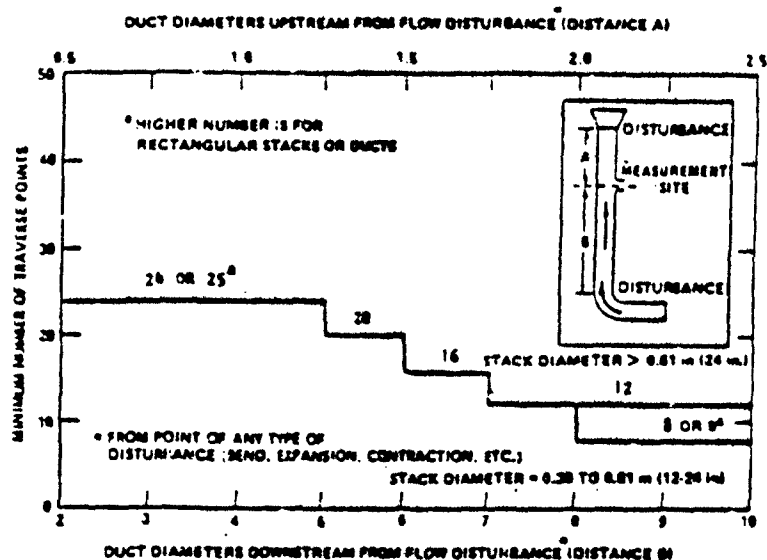


Figure 1-1. Minimum number of traverse points for particulate traverses.

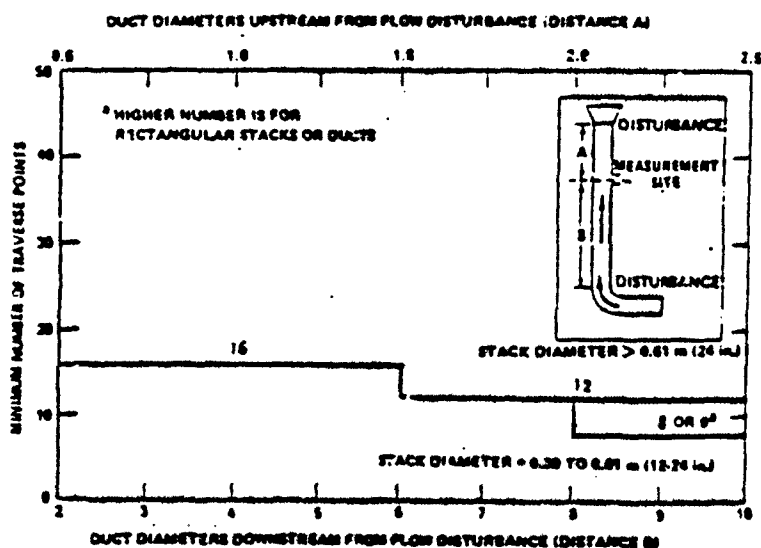


Figure 1-2. Minimum number of traverse points for velocity (nonparticulate) traverses.

2.2.2 Velocity (Non-Particulate) Traverses. When velocity or volumetric flow rate is to be determined (but not particulate matter), the same procedure as that for particulate traverses (Section 2.2.1) is followed, except that Figure 1-2 may be used instead of Figure 1-1.

### 2.3 Cross-sectional Layout and Location of Traverse Points.

2.3.1 Circular Stacks. Locate the traverse points on two perpendicular diameters according to Table 1-2 and the example shown in Figure 1-3. Any equation (for examples, see Citations 2 and 3 in the Bibliography) that gives the same values as those in Table 1-2 may be used in lieu of Table 1-2.

For particulate traverses, one of the diameters must be in a plane containing the greatest expected concentration variation, e.g., after bends, one diameter shall be in the plane of the bend. This requirement becomes less critical as the distance from the disturbance increases; therefore, other diameter locations may be used, subject to approval of the Administrator.

In addition for stacks having diameters greater than 0.61 m (24 in.) no traverse points shall be located within 2.5 centimeters (1.00 in.) of the stack walls; and for stack diameters equal to or less than 0.61 m (24 in.), no traverse points shall be located within 1.3 cm (0.50 in.) of the stack walls.

To meet these criteria, observe the procedures given below.

2.3.1.1 Stacks With Diameters Greater Than 0.61 m (24 in.). When any of the traverse points is located in Section 2.3.1 (all within 2.5 cm (1.00 in.) of the stack walls, relocate them away from the stack walls to:

(1) a distance of 2.5 cm (1.00 in.); or (2) a distance equal to the nozzle inside diameter, whichever is larger. These relocated traverse points (on each end of a diameter) shall be the "adjusted" traverse points.

Whenever two successive traverse points are combined to form a single adjusted traverse point, treat the adjusted point as two separate traverse points, both in the sampling (or velocity measurement) procedure, and in recording the data.

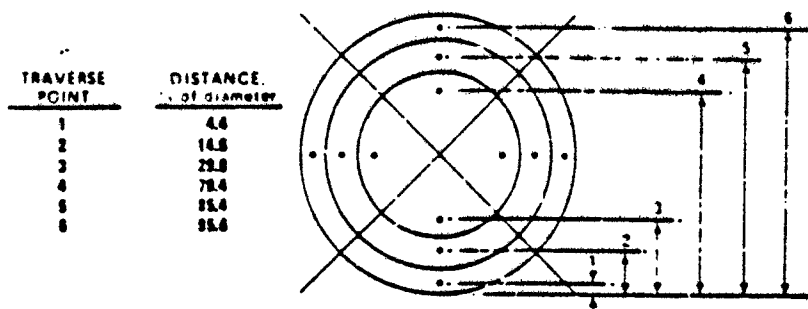


Figure 1-3. Example showing circular stack cross section divided into 12 equal areas, with location of traverse points indicated.

TABLE 1-2. LOCATION OF TRAVERSE POINTS IN CIRCULAR STACKS

(Percent of stack diameter from inside wall to traverse point)

Traverse point number on a diameter	Number of traverse points on a diameter—											
	2	4	6	8	10	12	14	16	18	20	22	24
1	14.6	8.7	4.4	2.2	2.9	2.1	1.8	1.6	1.4	1.3	1.1	1.1
2	25.0	14.6	10.5	8.2	6.7	5.7	4.9	4.4	3.9	3.5	3.2	2.9
3	35.4	25.0	18.4	14.6	11.8	9.9	8.5	7.5	6.7	6.0	5.5	5.0
4	45.8	35.4	25.0	19.9	16.7	14.0	12.5	10.9	9.7	8.7	7.9	7.2
5	56.2	45.8	35.4	27.7	23.0	20.1	18.0	16.0	14.0	12.5	11.8	10.5
6	66.6	56.2	45.8	37.7	31.8	27.7	24.0	21.0	18.4	16.0	14.6	13.2
7	77.0	66.6	56.2	47.7	40.9	35.4	31.8	28.0	24.0	21.0	18.4	16.0
8	87.4	77.0	66.6	57.7	50.0	43.5	38.9	34.4	30.0	26.0	23.0	20.1
9	97.8	87.4	77.0	67.7	59.0	51.4	45.8	40.9	36.6	32.0	28.0	24.0
10		97.8	87.4	77.0	67.7	59.0	51.4	45.8	40.9	36.6	32.0	28.0
11			97.8	87.4	77.0	67.7	59.0	51.4	45.8	40.9	36.6	32.0
12				97.8	87.4	77.0	67.7	59.0	51.4	45.8	40.9	36.6
13					97.8	87.4	77.0	67.7	59.0	51.4	45.8	40.9
14						97.8	87.4	77.0	67.7	59.0	51.4	45.8
15							97.8	87.4	77.0	67.7	59.0	51.4
16								97.8	87.4	77.0	67.7	59.0
17									97.8	87.4	77.0	67.7
18										97.8	87.4	77.0
19											97.8	87.4
20												97.8
21												
22												
23												
24												

2.3.1.2 Stacks With Diameters Equal to or Less Than 0.61 m (24 in.). Follow the procedure in Section 2.3.1.1, noting only that any "adjusted" points should be relocated away from the stack walls to: (1) a distance of 1.3 cm (0.50 in.) or (2) a distance equal to the nozzle inside diameter, whichever is larger.

2.3.2 Rectangular Stacks. Determine the number of traverse points as explained in Sections 2.1 and 2.2 of this method. From Table 1-1, determine the grid configuration. Divide the stack cross-section into as many equal rectangular elemental areas as traverse points, and then locate a traverse point at the centroid of each equal area according to the example in Figure 1-4.

If the tester desires to use more than the minimum number of traverse points, expand the "minimum number of traverse points" matrix (see Table 1-1) by adding the extra traverse points along one or the other or both legs of the matrix; the final matrix need not be balanced. For example, if a 4x3 "minimum number of points" matrix were expanded to 36 points, the final matrix could be 9x4 or 12x3, and would not necessarily have to be 6x6. After constructing the final matrix, divide the stack cross-section into as many equal rectangular, elemental areas as traverse points, and locate a traverse point at the centroid of each equal area.

The situation of traverse points being too close to the stack walls is not expected to arise with rectangular stacks. If this problem should ever arise, the Administrator must be contacted for resolution of the matter.

2.4 Verification of Absence of Cyclonic Flow. In most stationary sources, the direction of stack gas flow is essentially parallel to the stack walls. However, cyclonic flow may exist (1) after such devices as cyclones and inertial demisters following venturi scrubbers, or (2) in stacks having tangential inlets or other duct configurations which tend to induce swirling; in these instances, the presence or absence of cyclonic flow at the sampling location must be determined. The following techniques are acceptable for this determination.

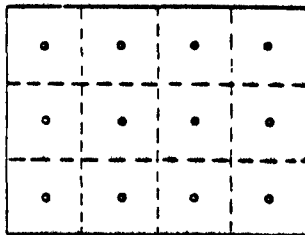


Figure 1-4. Example showing rectangular stack cross section divided into 12 equal areas, with a traverse point at centroid of each area.

Level and zero the manometer. Connect a Type S pitot tube to the manometer. Position the Type S pitot tube at each traverse point, in succession, so that the planes of the face openings of the pitot tube are perpendicular to the stack cross-sectional plane; when the Type S pitot tube is in this position, it is at "0" reference. Note the differential pressure ( $\Delta p$ ) reading at each traverse point. If a null (zero) pitot reading is obtained at 0° reference at a given traverse point, an acceptable flow condition exists at that point. If the pitot reading is not zero at 0° reference, rotate the pitot tube (up to  $\pm 90^\circ$  yaw angle), until a null reading is obtained. Carefully determine and record the value of the rotation angle ( $\alpha$ ) to the nearest degree. After the null technique has been applied at each traverse point, calculate the average of the absolute values of  $\alpha$ ; assign a value of 0° to those points for which no rotation was required, and include these in the overall average. If the average value of  $\alpha$  is greater than 20°, the overall flow condition in the stack is unacceptable and alternative methodology, subject to the approval of the Administrator, must be used to perform accurate sample and velocity traverses.

The alternative procedure described in Section 2.5 may be used to determine the rotation angles in lieu of the procedure described above. The limit of acceptability for the average value of  $\alpha$  would remain 20°.

2.5 Alternative Measurement Site Selection Procedure. This alternative applies to sources where measurement locations are less than 2 equivalent stack or duct diameters downstream or less than  $\frac{1}{4}$  duct diameter upstream from a flow disturbance. The alternative should be limited to ducts larger than 24 in. in diameter where blockage and wall effects are minimal. A directional flow-sensing probe is used to measure pitch and yaw angles of the gas flow at 40 or more traverse points; the resultant angle is calculated and compared with acceptable criteria for mean and standard deviation.

Note.—Both the pitch and yaw angles are measured from a line passing through the traverse point and parallel to the stack axis. The pitch angle is the angle of the gas flow component in the plane that INCLUDES the traverse line and is parallel to the stack axis. The yaw angle is the angle of the gas flow component in the plane PERPENDICULAR to the traverse line at the traverse point and is measured from the line passing through the traverse point and parallel to the stack axis.

#### 2.5.1 Apparatus.

2.5.1.1 Directional Probe. Any directional probe, such as United Sensor Type DA Three-Dimensional Directional Probe, capable of measuring both the pitch and yaw angles of gas flows is acceptable. (Note: Mention of trade name or specific products does not constitute endorsement by the U.S. Environmental Protection Agency.) Assign an identification number to the directional

probe, and permanently mark or engrave the number on the body of the probe. The pressure holes of directional probes are susceptible to plugging when used in particulate-laden gas streams. Therefore, a system for cleaning the pressure holes by "back-purging" with pressurized air is required.

2.5.1.2 Differential Pressure Gauges. Inclined manometers, U-tube manometers, or other differential pressure gauges (e.g., magnetic gauges) that meet the specifications described in Method 2, § 2.2.

Note.—If the differential pressure gauge produces both negative and positive readings, then both negative and positive pressure readings shall be calibrated at a minimum of three points as specified in Method 2, § 2.2.

2.5.2 Traverse Points. Use a minimum of 40 traverse points for circular ducts and 42 points for rectangular ducts for the gas flow angle determinations. Follow § 2.3 and Table 1-1 or 1-2 for the location and layout of the traverse points. If the measurement location is determined to be acceptable according to the criteria in this alternative procedure, use the same traverse point number and locations for sampling and velocity measurements.

#### 2.5.3 Measurement Procedure.

2.5.3.1 Prepare the directional probe and differential pressure gauges as recommended by the manufacturer. Capillary tubing or surge tanks may be used to dampen pressure fluctuations. It is recommended, but not required, that a pretest leak check be conducted. To perform a leak check, pressurize or use suction on the impact opening until a reading of at least 7.6 cm (3 in.) H<sub>2</sub>O registers on the differential pressure gauge, then plug the impact opening. The pressure of a leak-free system will remain stable for at least 15 seconds.

2.5.3.2 Level and zero the manometers. Since the manometer level and zero may drift because of vibrations and temperature changes, periodically check the level and zero during the traverses.

2.5.3.3 Position the probe at the appropriate locations in the gas stream, and rotate until zero deflection is indicated for the yaw angle pressure gauge. Determine and record the yaw angle. Record the pressure gauge readings for the pitch angle, and determine the pitch angle from the calibration curve. Repeat this procedure for each traverse point. Complete a "back-purge" of the pressure lines and the impact openings prior to measurements of each traverse point.

A post-test check as described in 4-2.3.1 is required. If the criteria for a leak-free system are not met, repair the equipment, and repeat the flow angle measurements.

2.5.4 Calculate the resultant angle at each traverse point, the average resultant angle, and the standard deviation using the following equations. Complete the calculations retaining at least one extra significant figure beyond that of the acquired data. Round the values after the final calculations.

2.5.4.1 Calculate the resultant angle at each traverse point

$$R_i = \arccosine [( \cosine Y_i ) ( \cosine P_i )] \quad \text{Eq. 1-2}$$

Where:

$R_i$  = Resultant angle at traverse point i, degree.

$Y_i$  = Yaw angle at traverse point i, degree.

$P_i$  = Pitch angle at traverse point i, degree.

2.5.4.2 Calculate the average resultant for the measurements:

$$\bar{R} = \frac{\sum R_i}{n} \quad \text{Eq. 1-3}$$

where:

$\bar{R}$  = Average resultant angle, degree.

$n$  = Total number of traverse points.

2.5.4.3 Calculate the standard deviations:

$$S_d = \sqrt{\frac{\sum_{i=1}^n (R_i - \bar{R})^2}{(n-1)}} \quad \text{Eq. 1-4}$$

Where:

$S_d$  = Standard deviation, degree.

2.5.5 The measurement location is acceptable if  $R < 20^\circ$  and  $S_d < 10^\circ$ .

2.5.6 Calibration. Use a flow system as described in Sections 4.1.2.1 and 4.1.2.2 of Method 2. In addition, the flow system shall have the capacity to generate two test-section velocities: one between 365 and 730 m/min (1200 and 2400 ft/min) and one between 730 and 1100 m/min (2400 and 3600 ft/min).

2.5.6.1 Cut two entry ports in the test section. The axes through the entry ports shall be perpendicular to each other and intersect in the centroid of the test section. The ports should be elongated slots parallel to the axis of the test section and of sufficient length to allow measurement of pitch angles while maintaining the pitot head position at the test-section centroid. To facilitate alignment of the directional probe during calibration, the test section should be constructed of plexiglass or some other transparent material. All calibration measurements should be made at the same point in the test section, preferably at the centroid of the test-section.

2.5.6.2 To ensure that the gas flow is parallel to the central axis of the test section, follow the procedure in Section 2.4 for cyclonic flow determination to measure the gas flow angles at the centroid of the test section from two test ports located  $90^\circ$  apart. The gas flow angle measured in each port must be  $\pm 2^\circ$  of  $0^\circ$ . Straightening vanes should be installed, if necessary, to meet this criterion.

2.5.6.3 Pitch Angle Calibration. Perform a calibration traverse according to the manufacturer's recommended protocol in  $5^\circ$  increments for angles from  $-60^\circ$  to  $+60^\circ$  at one velocity in each of the two ranges

specified above. Average the pressure ratio values obtained for each angle in the two flow ranges, and plot a calibration curve with the average values of the pressure ratio (or other suitable measurement factor as recommended by the manufacturer) versus the pitch angle. Draw a smooth line through the data points. Plot also the data values for each traverse point. Determine the differences between the measured data values and the angle from the calibration curve at the same pressure ratio. The difference at each comparison must be within  $2^\circ$  for angles between  $0^\circ$  and  $40^\circ$  and within  $3^\circ$  for angles between  $40^\circ$  and  $60^\circ$ .

2.5.6.4 Yaw Angle Calibration. Mark the three-dimensional probe to allow the determination of the yaw position of the probe. This is usually a line extending the length of the probe and aligned with the impact opening. To determine the accuracy of measurements of the yaw angle, only the zero or null position need be calibrated as follows. Place the directional probe in the test section, and rotate the probe until the zero position is found. With a protractor or other angle measuring device, measure the angle indicated by the yaw angle indicator on the three-dimensional probe. This should be within  $2^\circ$  of  $0^\circ$ . Repeat this measurement for any other points along the length of the pitot where yaw angle measurements could be read in order to account for variations in the pitot markings used to indicate pitot head positions.

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July 1990  
Revision: Final

**EPA METHOD 2**  
**DETERMINATION OF STACK GAS VELOCITY AND**  
**VOLUMETRIC FLOW RATE**

1311R2

**METHOD 2—DETERMINATION OF STACK GAS VELOCITY AND VOLUMETRIC FLOW RATE (TYPE S PITOT TUBE)**

**1. Principle and Applicability**

1.1 Principle. The average gas velocity in a stack is determined from the gas density and from measurement of the average velocity head with a Type S (Stausscheibe or reverse type) pitot tube.

1.2 Applicability. This method is applicable for measurement of the average velocity of a gas stream and for quantifying gas flow.

This procedure is not applicable at measurement sites which fail to meet the criteria of Method 1, Section 2.1. Also, the method cannot be used for direct measurement in cyclonic or swirling gas streams; Section 2.4 of Method 1 shows how to determine cyclonic or swirling flow conditions. When unacceptable conditions exist, alternative procedures, subject to the approval of the Administrator, U.S. Environmental Protection Agency, must be employed to make accurate flow rate determinations; examples of such alternative procedures are: (1) to install straightening vanes; (2) to calculate the total volumetric flow rate stoichiometrically, or (3) to move to another measurement site at which the flow is acceptable.

**2. Apparatus**

Specifications for the apparatus are given below. Any other apparatus that has been demonstrated (subject to approval of the Administrator) to be capable of meeting the specifications will be considered acceptable.

2.1 Type S Pitot Tube. The Type S pitot tube (Figure 2-1) shall be made of metal tubing (e.g. stainless steel). It is recommended that the external tubing diameter (dimension  $D$ , Figure 2-2b) be between 0.48 and 0.95 centimeters ( $\frac{1}{8}$  and  $\frac{3}{16}$  inch). There shall be an equal distance from the base of each leg of the pitot tube to its face-opening plane (dimensions  $P_1$  and  $P_2$ , Figure 2-2b); it is recommended that this distance be between 1.05 and 1.50 times the external tubing diameter. The face openings of the pitot tube shall, preferably, be aligned as shown in Figure 2-2; however, slight misalignments of the openings are permissible (see Figure 2-3).

The Type S pitot tube shall have a known coefficient, determined as outlined in Section 4. An identification number shall be assigned to the pitot tube; this number shall be permanently marked or engraved on the body of the tube.

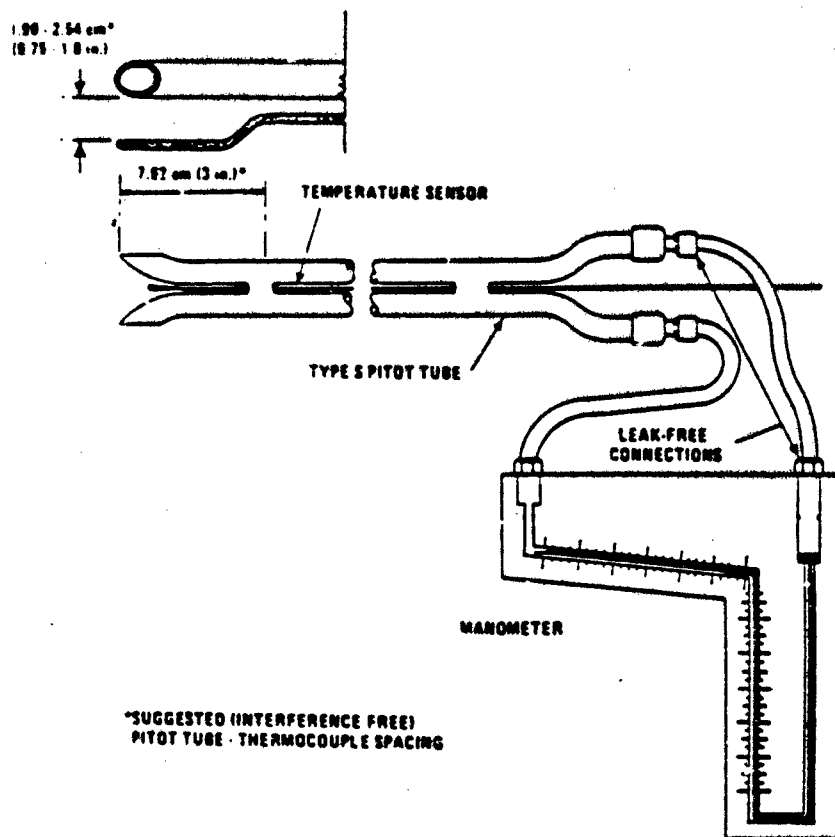


Figure 2-1. Type S pitot tube manometer assembly.

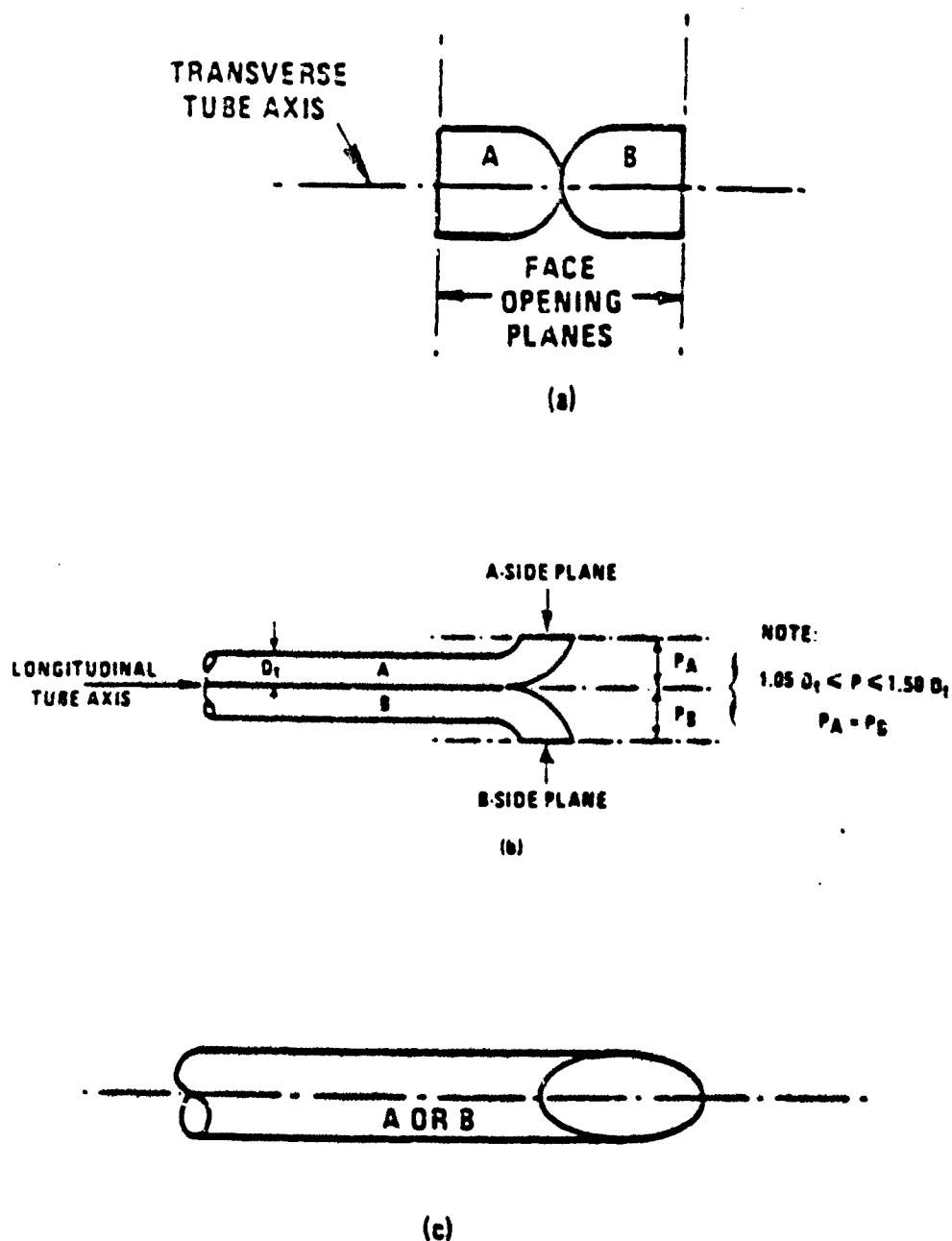


Figure 2-2. Properly constructed Type S pitot tube, shown in: (a) end view; face opening planes perpendicular to transverse axis; (b) top view; face opening planes parallel to longitudinal axis; (c) side view; both legs of equal length and centerlines coincident, when viewed from both sides. Baseline coefficient values of 0.84 may be assigned to pitot tubes constructed this way.

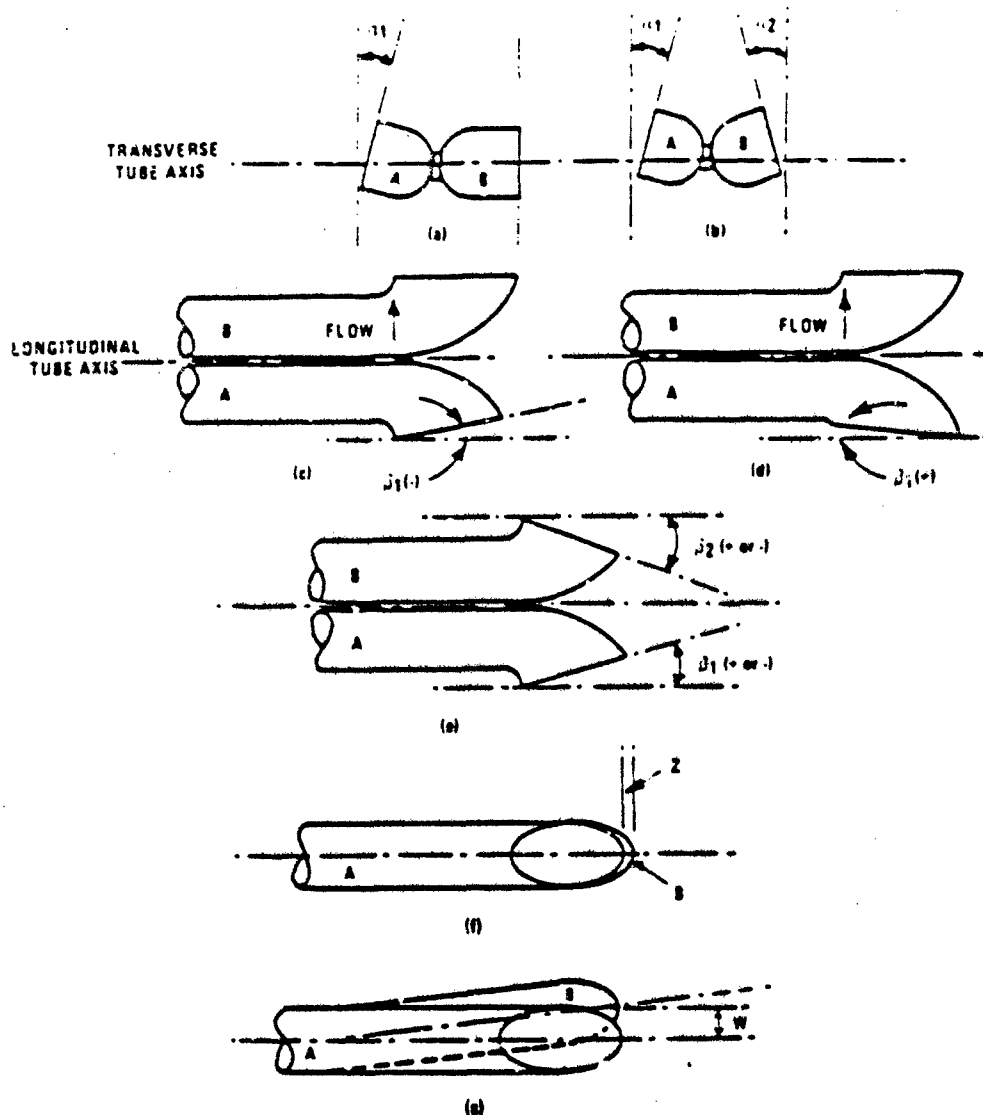


Figure 2-3. Types of face-opening misalignment that can result from field use or improper construction of Type S pitot tubes. These will not affect the baseline value of  $C_p(s)$  so long as  $\alpha_1$  and  $\alpha_2 \leq 10^\circ$ ,  $\beta_1$  and  $\beta_2 \leq 5^\circ$ ,  $z \leq 0.32$  cm (1/8 in.) and  $w \leq 0.08$  cm (1/32 in.) (citation 11 in Section 6).

A standard pitot tube may be used instead of a Type S, provided that it meets the specifications of Sections 2.7 and 4.2; note, however, that the static and impact pressure holes of standard pitot tubes are susceptible to plugging in particulate-laden gas streams. Therefore, whenever a standard pitot tube is used to perform a traverse, adequate proof must be furnished that the openings of the pitot tube have not plugged up during the traverse period; this can be done by taking a velocity head ( $\Delta p$ ) reading at

the final traverse point, cleaning out the impact and static holes of the standard pitot tube by "back-purging" with pressurized air, and then taking another  $\Delta p$  reading. If the  $\Delta p$  readings made before and after the air purge are the same ( $\pm 5$  percent), the traverse is acceptable. Otherwise, reject the run. Note that if  $\Delta p$  at the final traverse point is unsuitably low, another point may be selected. If "back-purging" at regular intervals is part of the procedure, then comparative  $\Delta p$  readings shall be



taken, as above, for the last two back purges at which suitably high  $\Delta p$  readings are observed.

2.2 Differential Pressure Gauge. An inclined manometer or equivalent device is used. Most sampling trains are equipped with a 10-in. (water column) inclined-vertical manometer, having 0.01-in. H<sub>2</sub>O divisions on the 0-to 1-in. inclined scale, and 0.1-in. H<sub>2</sub>O divisions on the 1- to 10-in. vertical scale. This type of manometer (or other gauge of equivalent sensitivity) is satisfactory for the measurement of  $\Delta p$  values as low as 1.3 mm (0.05 in.) H<sub>2</sub>O. However, a differential pressure gauge of greater sensitivity shall be used (subject to the approval of the Administrator), if any of the following is found to be true: (1) the arithmetic average of all  $\Delta p$  readings at the traverse points in the stack is less than 1.3 mm (0.05 in.) H<sub>2</sub>O; (2) for traverses of 12 or more points, more than 10 percent of the individual  $\Delta p$  readings are below 1.3 mm (0.05 in.) H<sub>2</sub>O; (3) for traverses of fewer than 12 points, more than one  $\Delta p$  reading is below 1.3 mm (0.05 in.) H<sub>2</sub>O. Citation 18 in Section 6 describes commercially available instrumentation for the measurement of low-range gas velocities.

As an alternative to criteria (1) through (3) above, the following calculation may be performed to determine the necessity of using a more sensitive differential pressure gauge:

$$T = \frac{\sum_{i=1}^n \sqrt{\Delta p_i} + K}{\sum_{i=1}^n \sqrt{\Delta p_i}}$$

where:

$\Delta p_i$  = Individual velocity head reading at a traverse point, mm H<sub>2</sub>O (in. H<sub>2</sub>O).

$n$  = Total number of traverse points.

$K$  = 0.13 mm H<sub>2</sub>O when metric units are used and 0.005 in. H<sub>2</sub>O when English units are used.

If  $T$  is greater than 1.05, the velocity head data are unacceptable and a more sensitive differential pressure gauge must be used.

Note: If differential pressure gauges other than inclined manometers are used (e.g., magnetic gauges), their calibration must be checked after each test series. To check

the calibration of a differential pressure gauge, compare  $\Delta p$  readings of the gauge with those of a gauge-oil manometer at a minimum of three points, approximately representing the range of  $\Delta p$  values in the stack. If, at each point, the values of  $\Delta p$  as read by the differential pressure gauge and gauge-oil manometer agree to within 5 percent, the differential pressure gauge shall be considered to be in proper calibration. Otherwise, the test series shall either be voided, or procedures to adjust the measured  $\Delta p$  values and final results shall be used subject to the approval of the Administrator.

2.3 Temperature Gauge. A thermocouple, liquid-filled bulb thermometer, bimetallic thermometer, mercury-in-glass thermometer, or other gauge, capable of measuring temperature to within 1.5 percent of the minimum absolute stack temperature shall be used. The temperature gauge shall be attached to the pitot tube such that the sensor tip does not touch any metal; the gauge shall be in an interference-free arrangement with respect to the pitot tube face openings (see Figure 2-1 and also Figure 2-7 in Section 4). Alternate positions may be used if the pitot tube-temperature gauge system is calibrated according to the procedure of Section 4. Provided that a difference of not more than 1 percent in the average velocity measurement is introduced, the temperature gauge need not be attached to the pitot tube; this alternative is subject to the approval of the Administrator.

2.4 Pressure Probe and Gauge. A piezometer tube and mercury- or water-filled U-tube manometer capable of measuring stack pressure to within 2.5 mm (0.1 in.) Hg is used. The static tap of a standard type pitot tube or one leg of a Type S pitot tube with the face opening planes positioned parallel to the gas flow may also be used as the pressure probe.

2.5 Barometer. A mercury, aneroid, or other barometer capable of measuring atmospheric pressure to within 2.5 mm Hg (0.1 in. Hg) may be used. In many cases, the barometric reading may be obtained from a nearby national weather service station, in which case the station value (which is the absolute barometric pressure) shall be requested and an adjustment for elevation differences between the weather station and the sampling point shall be applied at a rate of minus 2.5 mm (0.1 in.) Hg per 30-meter (100 foot) elevation increase or vice-versa for elevation decrease.

2.6 Gas Density Determination Equipment. Method 3 equipment, if needed (see Section 3.6), to determine the stack gas dry molecular weight, and Reference Method 4 or Method 5 equipment for moisture content determination; other methods may be used subject to approval of the Administrator.

2.7 Calibration Pitot Tube. When calibration of the Type S pitot tube is necessary (see Section 4), a standard pitot tube is used as a reference. The standard pitot tube shall, preferably, have a known coefficient, obtained either (1) directly from the National Bureau of Standards, Route 270, Quince Orchard Road, Gaithersburg, Maryland, or (2) by calibration against another standard pitot tube with an NBS-traceable coefficient. Alternatively, a standard pitot tube designed according to the criteria given in 2.7.1 through 2.7.5 below and illustrated in Figure 2-4 (see also Citations 7, 8, and 17 in Section 6) may be used. Pitot tubes designed according to these specifications will have baseline coefficients of about  $0.99 \pm 0.01$ .

2.7.1 Hemispherical (shown in Figure 2-4), ellipsoidal, or conical tip.

2.7.2 A minimum of six diameters straight run (based upon  $D$ , the external diameter of the tube) between the tip and the static pressure holes.

2.7.3 A minimum of eight diameters straight run between the static pressure holes and the centerline of the external tube, following the 90 degree bend.

2.7.4 Static pressure holes of equal size (approximately 0.1  $D$ ), equally spaced in a piezometer ring configuration.

2.7.5 Ninety degree bend, with curved or filtered junction.

2.8 Differential Pressure Gauge for Type S Pitot Tube Calibration. An inclined manometer or equivalent is used. If the single-velocity calibration technique is employed (see Section 4.1.2.3), the calibration differential pressure gauge shall be readable to the nearest 0.13 mm H<sub>2</sub>O (0.005 in. H<sub>2</sub>O). For multivelocity calibrations, the gauge shall be readable to the nearest 0.13 mm H<sub>2</sub>O (0.005 in. H<sub>2</sub>O) for  $\Delta p$  values between 1.3 and 25 mm H<sub>2</sub>O (0.05 and 1.0 in. H<sub>2</sub>O), and to the nearest 1.3 mm H<sub>2</sub>O (0.05 in. H<sub>2</sub>O) for  $\Delta p$  values above 25 mm H<sub>2</sub>O (1.0 in. H<sub>2</sub>O). A special, more sensitive gauge will be required to read  $\Delta p$  values below 1.3 mm H<sub>2</sub>O (0.05 in. H<sub>2</sub>O) (see Citation 18 in Section 6).

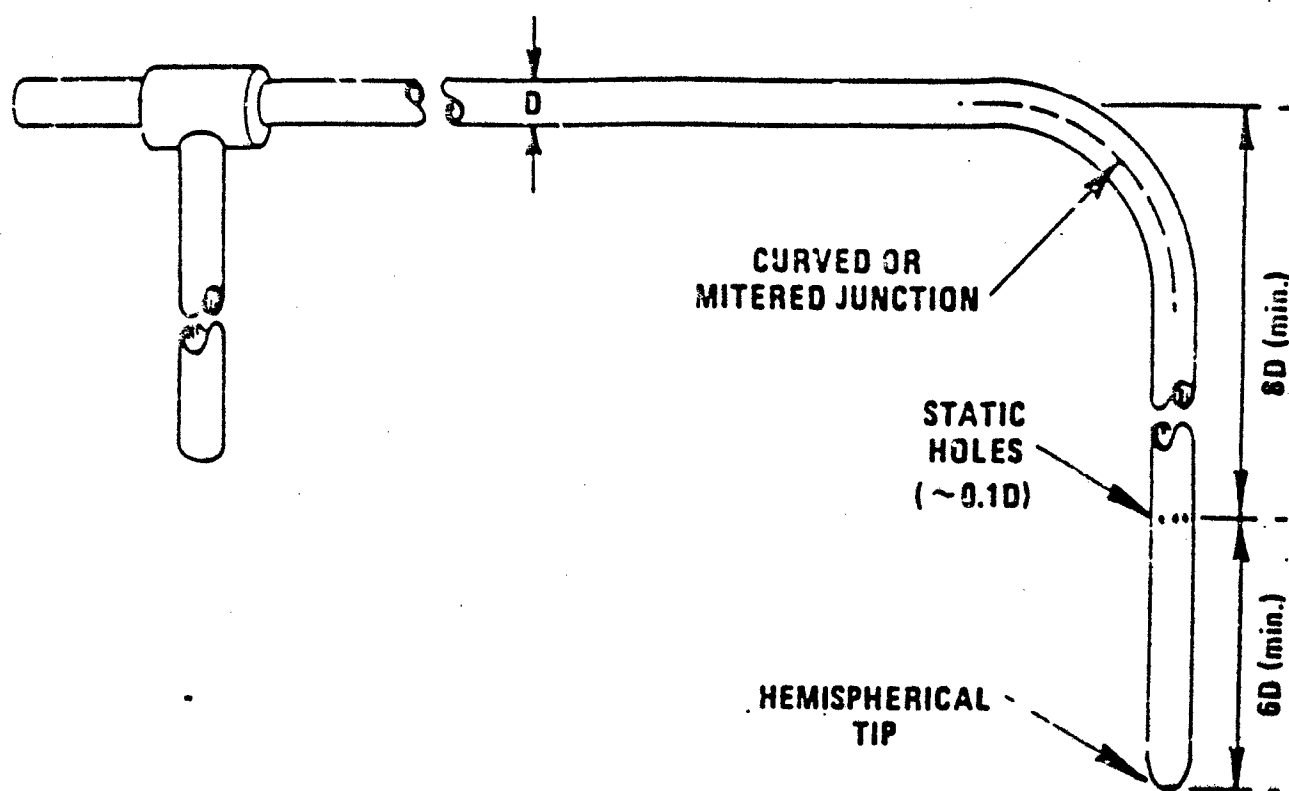


Figure 2-4. Standard pitot tube design specifications.

### 3. Procedure

3.1 Set up the apparatus as shown in Figure 2-1. Capillary tubing or surge tanks installed between the manometer and pitot tube may be used to dampen  $\Delta p$  fluctuations. It is recommended, but not required, that a pretest leak-check be conducted, as follows: (1) blow through the pitot impact opening until at least 7.6 cm (3 in.) H<sub>2</sub>O velocity pressure register on the manometer; then, close off the impact opening. The pressure shall remain stable for at least 15 seconds; (2) do the same for the static pressure side, except using suction to obtain the minimum of 7.6 cm (3 in.) H<sub>2</sub>O. Other leak-check procedures, subject to the approval of the Administrator may be used.

3.2 Level and zero the manometer. Because the manometer level and zero may

drift due to vibrations and temperature changes, make periodic checks during the traverse. Record all necessary data as shown in the example data sheet (Figure 2-3).

3.3 Measure the velocity head and temperature at the traverse points specified by Method 1. Ensure that the proper differential pressure gauge is being used for the range of  $\Delta p$  values encountered (see Section 2.2). If it is necessary to change to a more sensitive gauge, do so, and remeasure the  $\Delta p$  and temperature readings at each traverse point. Conduct a post-test leak-check (mandatory), as described in Section 3.1 above, to validate the traverse run.

3.4 Measure the static pressure in the stack. One reading is usually adequate.

3.5 Determine the atmospheric pressure.

**SCHEMATIC OF STACK  
CROSS SECTION**

[illegible]

**Figure 2.5. Velocity traverse data.**

**3.6 Determine the stack gas dry molecular weight.** For combustion processes or processes that emit essentially CO<sub>2</sub>, O<sub>2</sub>, CO, and N<sub>2</sub>, use Method 3. For processes emitting essentially air, an analysis need not be conducted; use a dry molecular weight of 29.0. For other processes, other methods, subject to the approval of the Administrator, must be used.

3.7 Obtain the moisture content from Reference Method 4 (or equivalent) or from Method 5.

3.8 Determine the cross-sectional area of the stack or duct at the sampling location. Whenever possible, physically measure the stack dimensions rather than using blueprints.

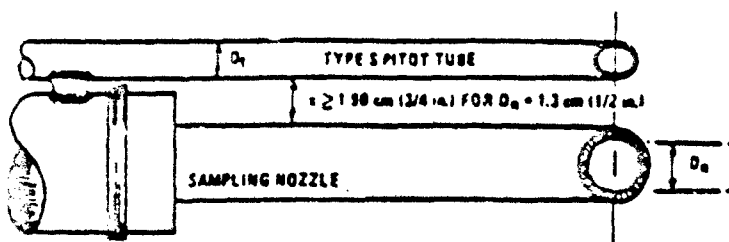
#### 4. Calibration

4.1 Type S Pitot Tube. Before its initial use, carefully examine the Type S pitot tube in top, side, and end views to verify that the face openings of the tube are aligned within the specifications illustrated in Figure 2-2 or 2-3. The pitot tube shall not be used if it fails to meet these alignment specifications.

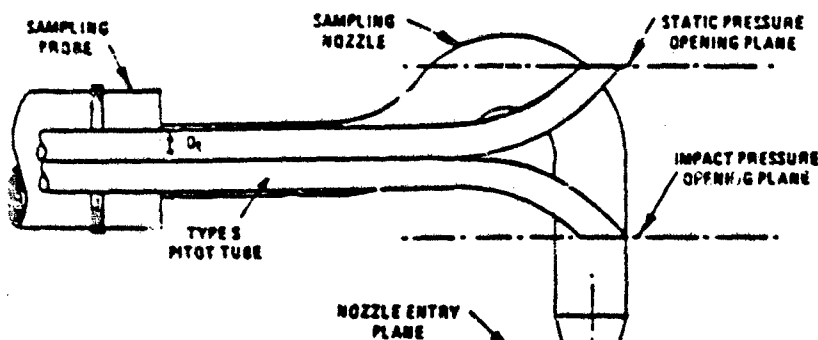
After verifying the face opening alignment, measure and record the following dimensions of the pitot tube: (a) the external tubing diameter (dimension  $D$ , Figure 2-2b); and (b) the base-to-opening plane distance (dimensions  $P$  and  $P_1$ , Figure 2-2b). If  $D$  is between 0.48 and 0.95 cm (1/4 and 3/8 in.), and

if  $P_1$  and  $P_2$  are equal and between 1.0 and 1.50 D, there are two possible options: the pitot tube may be calibrated according to the procedure outlined in Sections 4.1.3 below, or (2) a baseline (total) tube coefficient value of 0.84 may be assigned to the pitot tube. Note, however, if the pitot tube is part of an assembly bracket may still be required, despite knowledge of the baseline coefficient value (Section 4.1.1).

If  $D$ ,  $P_1$ , and  $P_2$  are outside the specified limits, the pitot tube must be calibrated outlined in 4.1.2 through 4.1.5 below.



A. BOTTOM VIEW: SHOWING MINIMUM PITOT NOZZLE SEPARATION.



B. SIDE VIEW: TO PREVENT PITOT TUBE FROM INTERFERING WITH GAS FLOW STREAMLINES APPROACHING THE NOZZLE, THE IMPACT PRESSURE OPENING PLANE OF THE PITOT TUBE SHALL BE EVEN WITH OR ABOVE THE NOZZLE ENTRY PLANE.

Figure 2-6. Proper pitot tube-sampling nozzle configuration to prevent aerodynamic interference: burndick-type nozzle; centers of nozzle and pitot opening aligned;  $D_t$  between 0.48 and 0.95 cm (3/16 and 3/8 in.).

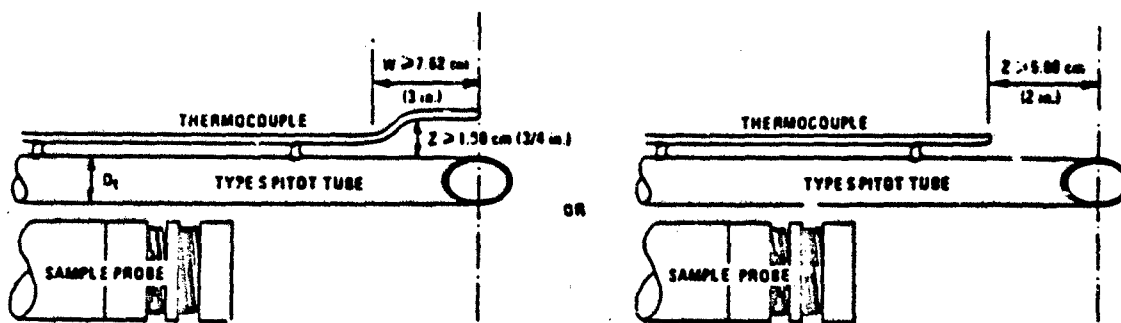


Figure 2-7. Proper thermocouple placement to prevent interference;  $D_t$  between 0.48 and 0.95 cm (3/16 and 3/8 in.).

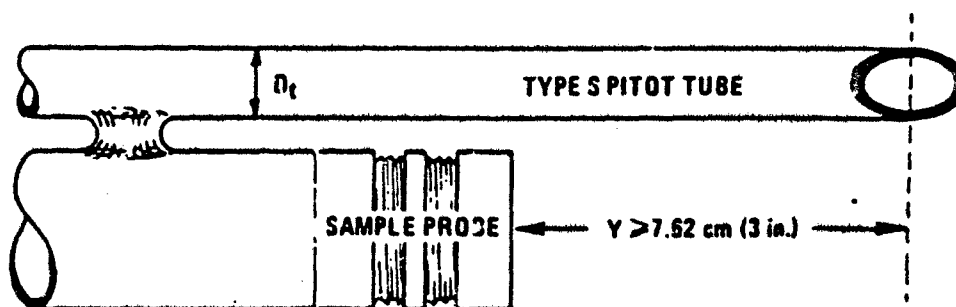


Figure 2-8. Minimum pitot-sample probe separation needed to prevent interference;  $D_t$  between 0.48 and 0.95 cm (3/16 and 3/8 in.).

4.1.1 Type S Pitot Tube Assemblies. During sample and velocity traverses, the isolated Type S pitot tube is not always used; in many instances, the pitot tube is used in combination with other source-sampling components (thermocouple, sampling probe, nozzle) as part of an "assembly." The presence of other sampling components can sometimes affect the baseline value of the Type S pitot tube coefficient (Citation 9 in Section 6); therefore, an assigned (or otherwise known) baseline coefficient value may or may not be valid for a given assembly. The baseline and assembly coefficient values will be identical only when the relative placement of the components in the assembly is such that aerodynamic interference effects are eliminated. Figures 2-6 through 2-8 illustrate interference-free component arrangements for Type S pitot tubes having external tubing diameters between 0.48 and 0.95 cm (3/16 and 3/8 in.). Type S pitot tube assemblies that fail to meet any or all of the specifications of Figures 2-6 through 2-8 shall be calibrated according to the procedure outlined in Sections 4.1.2 through 4.1.3 below, and prior to calibration, the values of the intercomponent spacings (pitot-nozzle, pitot-thermocouple, pitot-probe sheath) shall be measured and recorded.

Note: Do not use any Type S pitot tube assembly which is constructed such that the impact pressure opening plane of the pitot tube is below the entry plane of the nozzle (see Figure 2-6b).

4.1.2 Calibration Setup. If the Type S pitot tube is to be calibrated, one leg of the tube shall be permanently marked A, and the other, B. Calibration shall be done in a flow system having the following essential design features:

4.1.2.1 The flowing gas stream must be confined to a duct of definite cross-sectional area, either circular or rectangular. For circular cross-sections, the minimum duct diameter shall be 30.5 cm (12 in.); for rectangular cross-sections, the width (shorter side) shall be at least 25.4 cm (10 in.).

4.1.2.2 The cross-sectional area of the calibration duct must be constant over a distance of 10 or more duct diameters. For a rectangular cross-section, use an equivalent diameter, calculated from the following equation, to determine the number of duct diameters:

$$D = \frac{2LW}{(L+W)}$$

Equation 2-1

where:

D = Equivalent diameter  
L = Length  
W = Width

To ensure the presence of stable, fully developed flow patterns at the calibration site, or "test section," the site must be located at least eight diameters downstream and two diameters upstream from the nearest disturbances.

Note: The eight- and two-diameter criteria are not absolute; other test section locations may be used (subject to approval of the Administrator), provided that the flow at the test site is stable and demonstrably parallel to the duct axis.

4.1.2.3 The flow system shall have the capacity to generate a test-section velocity around 915 m/min (3,000 ft/min). This velocity must be constant with time to guarantee steady flow during calibration. Note that Type S pitot tube coefficients obtained by single-velocity calibration at 915 m/min (3,000 ft/min) will generally be valid to within  $\pm 3$  percent for the measurement of velocities above 305 m/min (1,000 ft/min) and to within  $\pm 5$  to 6 percent for the measurement of velocities between 180 and 305 m/min (600 and 1,000 ft/min). If a more precise correlation between  $C_p$  and velocity is desired, the flow system shall have the capacity to generate at least four distinct, time-invariant test-section velocities covering the velocity range from 180 to 1,525 m/min (600 to 5,000 ft/min), and calibration data shall be taken at regular velocity intervals over this range (see Citations 9 and 14 in Section 6 for details).

4.1.2.4 Two entry ports, one each for the standard and Type S pitot tubes, shall be cut in the test section; the standard pitot entry port shall be located slightly downstream of the Type S port, so that the standard and Type S impact openings will lie in the same cross-sectional plane during calibration. To facilitate alignment of the pitot tubes during calibration, it is advisable that the test section be constructed of plexiglas or some other transparent material.

4.1.3 Calibration Procedure. Note that this procedure is a general one and must not be used without first referring to the special considerations presented in Section 4.1.5. Note also that this procedure applies only to single-velocity calibration. To obtain calibration data for the A and B sides of the Type S pitot tube, proceed as follows:

4.1.3.1 Make sure that the manometer is properly filled and that the oil is free from contamination and is of the proper density. Inspect and leak-check all pitot lines; repair or replace if necessary.

PITOT TUBE IDENTIFICATION NUMBER: \_\_\_\_\_ DATE: \_\_\_\_\_

CALIBRATED BY: \_\_\_\_\_

"A" SIDE CALIBRATION				
RUN NO.	$\Delta P_{std}$ cm H <sub>2</sub> O (in. H <sub>2</sub> O)	$\Delta P_{(A)}$ cm H <sub>2</sub> O (in. H <sub>2</sub> O)	$C_{p(A)}$	DEVIATION $C_{p(A)} - \bar{C}_p(A)$
1				
2				
3				

$\bar{C}_p$  (SIDE A)

"B" SIDE CALIBRATION				
RUN NO.	$\Delta P_{std}$ cm H <sub>2</sub> O (in. H <sub>2</sub> O)	$\Delta P_{(B)}$ cm H <sub>2</sub> O (in. H <sub>2</sub> O)	$C_{p(B)}$	DEVIATION $C_{p(B)} - \bar{C}_p(B)$
1				
2				
3				

$\bar{C}_p$  (SIDE B)

$$\text{AVERAGE DEVIATION} = \frac{1}{3} \left( |C_{p(A)} - \bar{C}_p(A)| + |C_{p(B)} - \bar{C}_p(B)| \right) \leftarrow \text{MUST BE } < 0.01$$

$$|\bar{C}_p(\text{SIDE A}) - \bar{C}_p(\text{SIDE B})| \leftarrow \text{MUST BE } < 0.01$$

Figure 2-9. Pitot tube calibration data.

4.1.3.2 Level and zero the manometer. Turn on the fan and allow the flow to stabilize. Seal the Type S entry port.

4.1.3.3 Ensure that the manometer is level and zeroed. Position the standard pitot tube at the calibration point (determined as outlined in Section 4.1.3.1), and align the tube so that its tip is pointed directly into the flow. Particular care should be taken in aligning the tube to avoid yaw and pitch angles. Make sure that the entry port surrounding the tube is properly sealed.

4.1.3.4 Read  $\Delta P_{std}$  and record its value in a data table similar to the one shown in Figure 2-9. Remove the standard pitot tube from the duct and disconnect it from the manometer. Seal the standard entry port.

4.1.3.5 Connect the Type S pitot tube to the manometer. Open the Type S entry port. Check the manometer level and zero. Insert and align the Type S pitot tube so that its A side impact opening is at the same

point as was the standard pitot tube and is pointed directly into the flow. Make sure that the entry port surrounding the tube is properly sealed.

4.1.3.6 Read  $\Delta P_{(A)}$  and enter its value in the data table. Remove the Type S pitot tube from the duct and disconnect it from the manometer.

4.1.3.7 Repeat steps 4.1.3.3 through 4.1.3.6 above until three pairs of  $\Delta P$  readings have been obtained.

4.1.3.8 Repeat steps 4.1.3.3 through 4.1.3.7 above for the B side of the Type S pitot tube.

4.1.3.9 Perform calculations, as described in Section 4.1.4 below.

4.1.4 Calculations.

4.1.4.1 For each of the six pairs of  $\Delta P$  readings (i.e., three from side A and three from side B) obtained in Section 4.1.3 above, calculate the value of the Type S pitot tube coefficient as follows:

$$C_{p, \text{avg}} = C_{p, \text{std}} \sqrt{\frac{\Delta p_{\text{avg}}}{\Delta p_{\text{std}}}}$$

Equation 2-2

where:

$C_{p, \text{std}}$  = Type S pitot tube coefficient;

$C_{p, \text{avg}}$  = Standard pitot tube coefficient; use 0.99 if the coefficient is unknown and the tube is designed according to the criteria of Sections 2.7.1 to 2.7.3 of this method.

$\Delta p_{\text{std}}$  = Velocity head measured by the standard pitot tube, cm H<sub>2</sub>O (in. H<sub>2</sub>O)

$\Delta p_{\text{avg}}$  = Velocity head measured by the Type S pitot tube, cm H<sub>2</sub>O (in. H<sub>2</sub>O)

4.1.4.2 Calculate  $\bar{C}_p$  (side A), the mean A-side coefficient, and  $\bar{C}_p$  (side B), the mean B-side coefficient; calculate the difference between these two average values.

4.1.4.3 Calculate the deviation of each of the three A-side values of  $\bar{C}_p$  from  $\bar{C}_p$  (side A), and the deviation of each B-side value of  $\bar{C}_p$  from  $\bar{C}_p$  (side B). Use the following equation:

$$\text{Deviation} = C_{p, i} - \bar{C}_p (A \text{ or } B)$$

Equation 2-3

4.1.4.4 Calculate  $\sigma$ , the average deviation from the mean, for both the A and B sides of the pitot tube. Use the following equation:

$$\sigma (\text{side A or B}) = \frac{\sum |C_{p, i} - \bar{C}_p (A \text{ or } B)|}{3}$$

Equation 2-4

4.1.4.5 Use the Type S pitot tube only if the values of  $\sigma$  (side A) and  $\sigma$  (side B) are less than or equal to 0.01 and if the absolute value of the difference between  $\bar{C}_p$  (A) and  $\bar{C}_p$  (B) is 0.01 or less.

4.1.5 Special considerations.

4.1.5.1 Selection of calibration point.

4.1.5.1.1 When an isolated Type S pitot tube is calibrated, select a calibration point at or near the center of the duct, and follow the procedures outlined in Sections 4.1.3 and 4.1.4 above. The Type S pitot coefficients so obtained, i.e.,  $\bar{C}_p$  (side A) and  $\bar{C}_p$  (side B), will be valid, so long as either: (1) the isolated pitot tube is used; or (2) the pitot tube is used with other components (nozzle, thermocouple, sample probe) in an arrangement that is free from aerodynamic interference effects (see Figures 2-4 through 2-8).

4.1.5.1.2 For Type S pitot tube-thermocouple combinations (without sample probe), select a calibration point at or near the center of the duct, and follow the procedures outlined in Sections 4.1.3 and 4.1.4 above. The coefficients so obtained will be valid so long as the pitot tube-thermocouple combination is used by itself or with other components in an interference-free arrangement (Figures 2-6, and 2-8).

4.1.5.1.3 For assemblies with sample probes, the calibration point should be located at or near the center of the duct; however, insertion of a probe sheath into a small duct may cause significant cross-sectional area blockage and yield incorrect coefficient values (Citation 9 in Section 6). Therefore, to minimize the blockage effect, the calibration point may be a few inches

off-center if necessary. The actual blockage effect will be negligible when the theoretical blockage, as determined by a projected-area model of the probe sheath, is 2 percent or less of the duct cross-sectional area (for assemblies without external sheaths (Figure 2-10a), and 3 percent or less for assemblies with external sheaths (Figure 2-10b).

4.1.5.2 For those probe assemblies in which pitot tube-nozzle interference is a factor (i.e., those in which the pitot-nozzle separation distance fails to meet the specification illustrated in Figure 2-6a), the value of  $C_{p, \text{std}}$  depends upon the amount of free-space between the tube and nozzle, and therefore is a function of nozzle size. In these instances, separate calibrations shall be performed with each of the commonly used nozzle sizes in place. Note that the single-velocity calibration technique is acceptable for this purpose, even though the larger nozzle sizes (>0.635 cm or 1/4 in.) are not ordinarily used for isokinetic sampling at velocities around 215 m/min (3,000 ft/min), which is the calibration velocity; note also that it is not necessary to draw an isokinetic sample during calibration (see Citation 19 in Section 6).

4.1.5.3 For a probe assembly constructed such that its pitot tube is always used in the same orientation, only one side of the pitot tube need be calibrated (the side which will face the flow). The pitot tube must still meet the alignment specifications of Figure 2-2 or 2-3, however, and must have an average deviation ( $\sigma$ ) value of 0.01 or less (see Section 4.1.4.4).

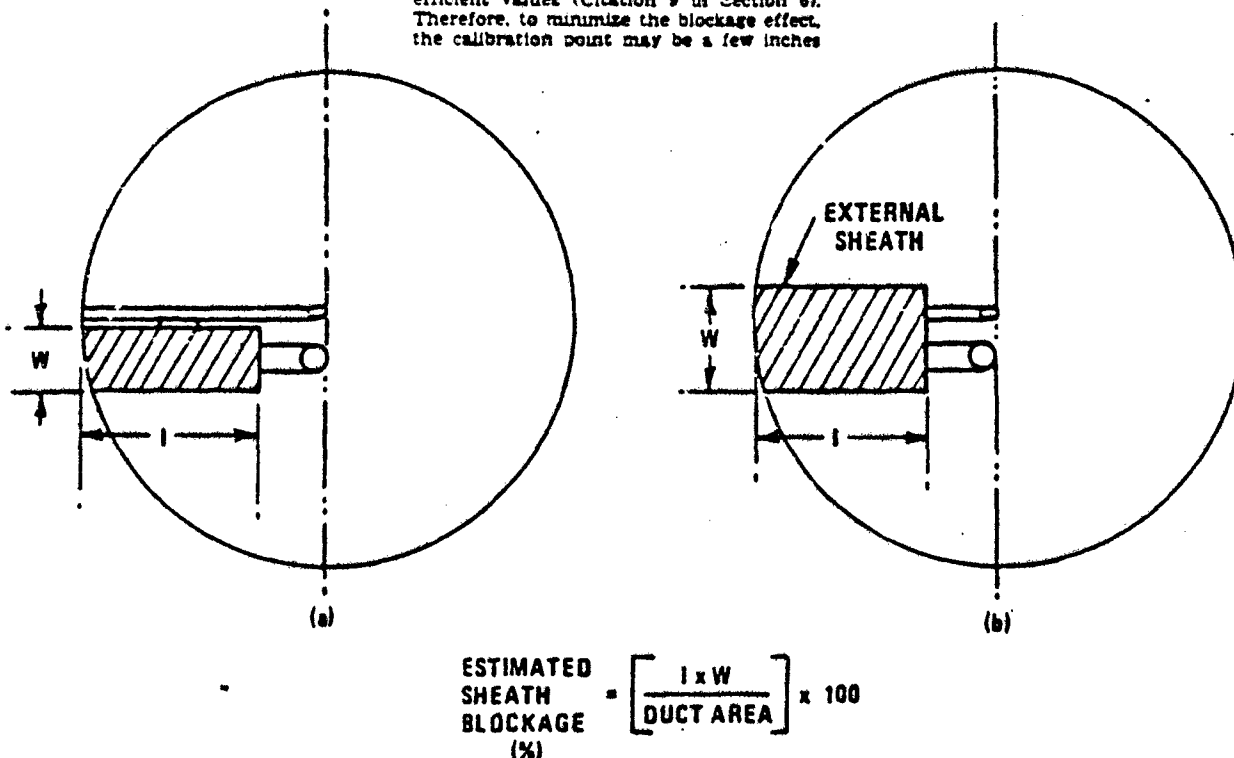


Figure 2-10. Projected-area models for typical pitot tube assemblies.

Figure 2-10. Projected-area models for typical pitot tube assemblies.

#### 4.1.6 Field Use and Recalibration.

##### 4.1.6.1 Field Use.

4.1.6.1.1 When a Type S pitot tube (isolated tube or assembly) is used in the field, the appropriate coefficient value (whether assigned or obtained by calibration) shall be used to perform velocity calculations. For calibrated Type S pitot tubes, the A side coefficient shall be used when the A side of the tube faces the flow, and the B side coefficient shall be used when the B side faces the flow; alternatively, the arithmetic average of the A and B side coefficient values may be used, irrespective of which side faces the flow.

4.1.6.1.2 When a probe assembly is used to sample a small duct (12 to 36 in. in diameter), the probe sheath sometimes blocks a significant part of the duct cross-section, causing a reduction in the effective value of  $C_p$ . Consult Citation 9 in Section 6 for details. Conventional pitot-sampling probe assemblies are not recommended for use in ducts having inside diameters smaller than 2 inches (Citation 16 in Section 6).

##### 4.1.6.2 Recalibration.

4.1.6.2.1 Isolated Pitot Tubes. After each field use, the pitot tube shall be carefully examined in top, side, and end views. If the pitot face openings are still aligned within the specifications illustrated in Figure 2-2 or 2-3, it can be assumed that the baseline coefficient of the pitot tube has not changed. If, however, the tube has been damaged to the extent that it no longer meets the specifications of Figure 2-2 or 2-3, the damage shall either be repaired to restore proper alignment of the face openings or the tube shall be discarded.

4.1.6.2.2 Pitot Tube Assemblies. After each field use, check the face opening alignment of the pitot tube, as in Section 1.8.2.1; also, remeasure the intercomponent spacings of the assembly. If the intercomponent spacings have not changed and the face opening alignment is acceptable, it can be assumed that the coefficient of the assembly has not changed. If the face opening alignment is no longer within the specifications of Figures 2-2 or 2-3, either repair or damage or replace the pitot tube (calibrating the new assembly, if necessary). If the intercomponent spacings have changed, restore the original spacings or recalibrate the assembly.

4.2 Standard pitot tube (if applicable). If standard pitot tube is used for the velocity traverse, the tube shall be constructed according to the criteria of Section 2.7 and shall be assigned a baseline coefficient value of 0.99. If the standard pitot tube is used as part of an assembly, the tube shall be in an interference-free arrangement (subject to the approval of the Administrator).

4.3 Temperature Gauges. After each field use, calibrate dial thermometer, liquid-filled bulb thermometers, thermocouple-potentiometer systems, and other gauges at a temperature within 10 percent of the average absolute stack temperature, or temperatures up to 405° C (761° F), use an ASTM mercury-in-glass reference thermometer, or equivalent, as a reference; alternatively, either a reference thermocouple and potentiometer (calibrated by NBS) or thermometric fixed points, e.g., ice bath and boiling water (corrected for barometric pressure) may be used. For temperatures above 15° C (761° F), use an NBS-calibrated reference thermocouple-potentiometer system or an alternate reference, subject to the approval of the Administrator.

If, during calibration, the absolute temperatures measured with the gauge being calibrated and the reference gauge agree within 1.5 percent, the temperature data taken in the field shall be considered valid. Otherwise, the pollutant emission test shall either be considered invalid or adjustments (if appropriate) of the test results shall be made, subject to the approval of the Administrator.

4.4 Barometer. Calibrate the barometer used against a mercury barometer.

#### 5. Calculations

Carry out calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after final calculation.

##### 5.1 Nomenclature.

$A$  = Cross-sectional area of stack, m<sup>2</sup> (ft<sup>2</sup>).  
 $S_w$  = Water vapor in the gas stream (from Method 5 or Reference Method 4), proportion by volume.  
 $C_p$  = Pitot tube coefficient, dimensionless.  
 $K_p$  = Pitot tube constant.

$$34.97 \frac{\text{in}}{\text{mm}} \left[ \frac{(\text{g/g-mole})(\text{mm Hg})}{(^{\circ}\text{K})(\text{mm H}_2\text{O})} \right]^{1/2}$$

for the metric system and

$$34.97 \frac{\text{ft}}{\text{in}} \left[ \frac{(\text{lb/lb-mole})(\text{in. Hg})}{(^{\circ}\text{R})(\text{in. H}_2\text{O})} \right]^{1/2}$$

for the English system.

$M_g$  = Molecular weight of stack gas, dry basis (see Section 3.6) g/g-mole (lb/lb-mole).  
 $M_w$  = Molecular weight of stack gas, wet basis, g/g-mole (lb/lb-mole).  
 $= M_g(1 - S_w) + 18.0 S_w$

Equation 2-5

$P_{atm}$  = Barometric pressure at measurement site, mm Hg (in. Hg).  
 $P_s$  = Stack static pressure, mm Hg (in. Hg).

$P_g$  = Absolute stack gas pressure, mm Hg (in. Hg).  
 $= P_{atm} + P_s$

Equation 2-6

$P_{std}$  = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).

$Q_{std}$  = Dry volumetric stack gas flow rate corrected to standard conditions, decm/hr (scf/hr).

$t$  = Stack temperature, °C (°F).  
 $T_g$  = Absolute stack temperature, °K (°R).  
 $= 273 + t$  for metric

Equation 2-7

$= 460 + t$  for English

Equation 2-8

$T_{std}$  = Standard absolute temperature, 293 °K (528 °R)

$u$  = Average stack gas velocity, m/sec (ft/sec).

$h_v$  = Velocity head of stack gas, mm H<sub>2</sub>O (in. H<sub>2</sub>O).

3.600 = Conversion factor, sec/hr.  
 $18.0$  = Molecular weight of water, g/g-mole (lb/lb-mole).

5.2 Average stack gas velocity.

$$u = K_p C_p (\sqrt{\Delta p}) \sqrt{\frac{T_{std}}{P_g M_g}}$$

Equation 2-9

5.3 Average stack gas dry volumetric flow rate.

$$Q_{std} = 3.600(1 - S_w)A \left( \frac{T_{std}}{T_g} \right) \left( \frac{P_g}{P_{std}} \right)$$

Equation 2-10

To convert  $Q_{std}$  from decm/hr (scf/hr) to decm/min (scf/min), divide  $Q_{std}$  by 60.

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July 1990  
Revision: Final

**EPA METHOD 25A**  
**DETERMINATION OF TOTAL GASEOUS ORGANIC CONCENTRATION**  
**USING A FLAME IONIZATION ANALYZER**

# METHOD 25A—DETERMINATION OF TOTAL GASEOUS ORGANIC CONCENTRATION USING A FLAME IONIZATION ANALYZER

## 1. Applicability and Principle.

**1.1 Applicability.** This method applies to the measurement of total gaseous organic concentration of vapors consisting primarily of alkanes, alkenes, and/or arenes (aromatic hydrocarbons). The concentration is expressed in terms of propane (or other appropriate organic calibration gas) or in terms of carbon.

**1.2 Principle.** A gas sample is extracted from the source through a heated sample line, if necessary, and glass fiber filter to a flame ionization analyzer (FIA). Results are reported as volume concentration equivalents of the calibration gas or as carbon equivalents.

## 2. Definitions.

**2.1 Measurement System.** The total equipment required for the determination of the gas concentration. The system consists of the following major subsystems:

**2.1.1 Sample Interface.** That portion of the system that is used for one or more of the following: sample acquisition, sample transportation, sample conditioning, or protection of the analyzer from the effects of the stack effluent.

**2.1.2 Organic Analyzer.** That portion of the system that senses organic concentration and generates an output proportional to the gas concentration.

**2.2 Span Value.** The upper limit of a gas concentration measurement range that is specified for affected source categories in the applicable part of the regulations. The span value is established in the applicable regulation and is usually 1.5 to 2.5 times the applicable emission limit. If no span value is provided, use a span value equivalent to 1.5 to 2.5 times the expected concentration. For convenience, the span value should correspond to 100 percent of the recorder scale.

**2.3 Calibration Gas.** A known concentration of a gas in an appropriate diluent gas.

**2.4 Zero Drift.** The difference in the measurement system response to a zero level calibration gas before and after a stated period of operation during which no unscheduled maintenance, repair, or adjustment took place.

**2.5 Calibration Drift.** The difference in the measurement system response to a mid-level calibration gas before and after a stated period of operation during which no unscheduled maintenance, repair or adjustment took place.

**2.6 Response Time.** The time interval from a step change in pollutant concentration at the inlet to the emission measurement system to the time at which 95 percent of the corresponding final value is reached as displayed on the recorder.

**2.7 Calibration Error.** The difference between the gas concentration indicated by the measurement system and the known concentration of the calibration gas.

## 3. Apparatus.

A schematic of an acceptable measurement system is shown in Figure 25A-1. The essential components of the measurement system are described below:

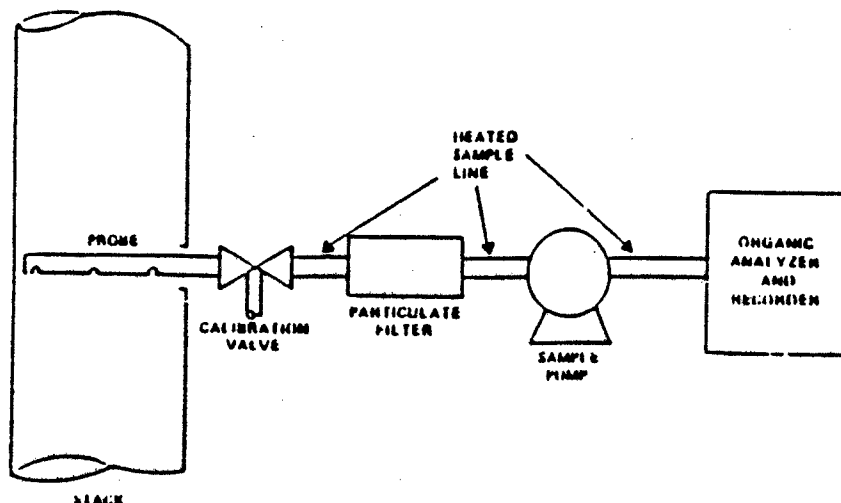


Figure 25A-1. Organic Concentration Measurement System.

**3.1 Organic Concentration Analyzer.** A flame ionization analyzer (FIA) capable of meeting or exceeding the specifications in this method.

**3.2 Sample Probe.** Stainless steel, or equivalent, three-hole rake type. Sample holes shall be 4 mm in diameter or smaller and located at 18.7, 50, and 83.3 percent of the equivalent stack diameter. Alternatively, a single opening probe may be used so that a gas sample is collected from the centrally located 10 percent area of the stack cross-section.

**3.3 Sample Line.** Stainless steel or Teflon® tubing to transport the sample gas to the analyzer. The sample line should be heated, if necessary, to prevent condensation in the line.

**3.4 Calibration Valve Assembly.** A three-way valve assembly to direct the zero and calibration gases to the analyzer is recommended. Other methods, such as quick-connect lines, to route calibration gas to the analyzer are applicable.

**3.5 Particulate Filter.** An in-stack or an out-of-stack glass fiber filter is recommended if exhaust gas particulate loading is significant. An out-of-stack filter should be heated to prevent any condensation.

**3.6 Recorder.** A strip-chart recorder, analog computer, or digital recorder for recording measurement data. The minimum data recording requirement is one measurement value per minute. Note: This method is often applied in highly explosive areas. Caution and care should be exercised in choice of equipment and installation.

## 4. Calibration and Other Gases.

Gases used for calibrations, fuel, and combustion air (if required) are contained in compressed gas cylinders. Preparation of calibration gases shall be done according to the procedure in Protocol No. 1, listed in Reference 9.2. Additionally, the manufacturer of the cylinder should provide a recommended shelf life for each calibration gas cylinder over which the concentration does not change more than ±2 percent from the certified value. For calibration gas values not generally available (i.e., organics between 1 and 10 percent by volume), alternative methods for preparing calibration gas mixtures, such as dilution systems, may be used with prior approval of the Administrator.

Calibration gases usually consist of propane in air or nitrogen and are determined in terms of the span value. Organic compounds other than propane can be used following the above guidelines and making the appropriate corrections for response factor.

**4.1 Fuel.** A 40 percent H<sub>2</sub>/60 percent He or 40 percent H<sub>2</sub>, 60 percent N<sub>2</sub> gas mixture is recommended to avoid an oxygen synergism effect that reportedly occurs when oxygen concentration varies significantly from a mean value.

**4.2 Zero Gas.** High purity air with less than 0.1 parts per million by volume (ppmv) of organic material (propane or carbon equivalent) or less than 0.1 percent of the span value, whichever is greater.

**4.3 Low-level Calibration Gas.** An organic calibration gas with a concentration equivalent to 25 to 35 percent of the applicable span value.

**4.4 Mid-level Calibration Gas.** An organic calibration gas with a concentration equivalent to 45 to 55 percent of the applicable span value.

**4.5 High-level Calibration Gas.** An organic calibration gas with a concentration equivalent to 80 to 90 percent of the applicable span value.

## 5. Measurement System Performance Specifications.

**5.1 Zero Drift.** Less than ±3 percent of the span value.

**5.2 Calibration Drift.** Less than ±3 percent of span value.

5.3 Calibration Error. Less than  $\pm 5$  percent of the calibration gas value.

#### 6. Pretest Preparations.

6.1 Selection of Sampling Site. The location of the sampling site is generally specified by the applicable regulation or purpose of the test; i.e., exhaust stack, inlet line, etc. The sample port shall be located at least 1.5 meters or 2 equivalent diameters (whichever is less) upstream of the gas discharge to the atmosphere.

6.2 Location of Sample Probe. Install the sample probe so that the probe is centrally located in the stack, pipe, or duct and is sealed tightly at the stack port connection.

6.3 Measurement System Preparation. Prior to the emission test, assemble the measurement system following the manufacturer's written instructions in preparing the sample interface and the organic analyzer. Make the system operable.

FLA equipment can be calibrated for almost any range of total organics concentrations. For high concentrations of organics ( $>1.0$  percent by volume as propane) modifications to most commonly available analyzers are necessary. One accepted method of equipment modification is to decrease the size of the sample to the analyzer through the use of a smaller diameter sample capillary. Direct and continuous measurement of organic concentration is a necessary consideration when determining any modification design.

6.4 Calibration Error Test. Immediately prior to the test series, (within 2 hours of the start of the test) introduce zero gas and high-level calibration gas at the calibration valve assembly. Adjust the analyzer output to the appropriate levels, if necessary. Calculate the predicted response for the low-level and mid-level gases based on a linear response line between the zero and high-level responses. Then introduce low-level and mid-level calibration gases successively to the measurement system. Record the analyzer responses for low-level and mid-level calibration gases and determine the differences between the measurement system responses and the predicted responses. These differences must be less than 5 percent of the respective calibration gas value. If not, the measurement system is not acceptable and must be replaced or repaired prior to testing. No adjustments to the measurement system shall be conducted after the calibration and before the drift check (Section 7.3). If adjustments are necessary before the completion of the test series, perform the drift checks prior to the required adjustments and repeat the calibration following the adjustments. If multiple electronic ranges are to be used, each additional range must be checked with a mid-level calibration gas to verify the multiplication factor.

6.5 Response Time Test. Introduce zero gas into the measurement system at the calibration valve assembly. When the system output has stabilized, switch quickly to the high-level calibration gas. Record the time from the concentration change to the measurement system response equivalent to 95 percent of the step change. Repeat the test three times and average the results.

#### 7. Emission Measurement Test

7.1 Organic Measurement. Begin sampling at the start of the test period, recording time and any required process information as appropriate. In particular, note on the recording chart periods of process interruption or cyclic operation.

7.2 Drift Determination. Immediately following the completion of the test period and hourly during the test period, reintroduce the zero and mid-level calibration gases, one at a time, to the measurement system at the calibration valve assembly. (Make no adjustments to the measurement system until after both the zero and calibration drift checks are made.) Record the analyzer response. If the drift values exceed the specified limits, invalidate the test results preceding the check and repeat the test following corrections to the measurement system. Alternatively, recalibrate the test measurement system as in Section 6.4 and report the results using both sets of calibration data (i.e., data determined prior to the test period and data determined following the test period).

#### 8. Organic Concentration Calculations.

Determine the average organic concentration in terms of ppmv as propane or other calibration gas. The average shall be determined by the integration of the output recording over the period specified in the applicable regulation.

If results are required in terms of ppmv as carbon, adjust measured concentrations using Equation 23A-1.

$$C_c = K C_m$$

Eq. 23A-1

Where:

$C_c$  = Organic concentration as carbon, ppmv.

$C_m$  = Organic concentration as measured, ppmv.

$K$  = Carbon equivalent correction factor.

$K=2$  for ethane.

$K=3$  for propane.

$K=4$  for butane.

$K$  = Appropriate response factor for other organic calibration gases.

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July 1990  
Revision: Final

**EPA METHOD 3**  
**GAS ANALYSIS FOR CARBON DIOXIDE, OXYGEN,**  
**EXCESS AIR, AND DRY MOLECULAR WEIGHT**

### METHOD 3—GAS ANALYSIS FOR CARBON DIOXIDE, OXYGEN, EXCESS AIR, AND DRY MOLECULAR WEIGHT

#### 1. Principle and Applicability

1.1 Principle. A gas sample is extracted from a stack, by one of the following methods: (1) single-point, grab sampling; (2) single-point, integrated sampling; or (3) multi-point, integrated sampling. The gas sample is analyzed for percent carbon dioxide ( $\text{CO}_2$ ), percent oxygen ( $\text{O}_2$ ), and, if necessary, percent carbon monoxide ( $\text{CO}$ ). If a dry molecular weight determination is to be made, either an Orsat or a Pyrite analyzer may be used for the analysis; for excess air or emission rate correction factor determination, an Orsat analyzer must be used.

1.2 Applicability. This method is applicable for determining  $\text{CO}_2$  and  $\text{O}_2$  concentrations, excess air, and dry molecular weight of a sample from a gas stream of a fossil-fuel combustion process. The method may also be applicable to other processes where it has been determined that compounds other than  $\text{CO}_2$ ,  $\text{O}_2$ ,  $\text{CO}$ , and nitrogen ( $\text{N}_2$ ) are not present in concentrations sufficient to affect the results.

Other methods, as well as modifications to the procedure described herein, are also applicable for some or all of the above determinations. Examples of specific methods and modifications include: (1) a multi-point sampling method using an Orsat analyzer to analyze individual grab samples obtained at each point; (2) a method using  $\text{CO}_2$  or  $\text{O}_2$  and stoichiometric calculations to determine dry molecular weight and excess air; (3) assigning a value of 30.0 for dry molecular weight, in lieu of actual measurements, for processes burning natural gas, coal, or oil. These methods and modifications may be used, but are subject to the approval of the Administrator, U.S. Environmental Protection Agency.

#### 2. Apparatus

As an alternative to the sampling apparatus and systems described herein, other sampling systems (e.g., liquid displacement) may be used provided such systems are capable of obtaining a representative sample and maintaining a constant sampling rate, and are otherwise capable of yielding acceptable results. Use of such systems is subject to the approval of the Administrator.

##### 2.1 Grab Sampling (Figure 3-1).

2.1.1 Probe. The probe should be made of stainless steel or borosilicate glass tubing and should be equipped with an in-stack or out-stack filter to remove particulate matter (a plug of glass wool is satisfactory for this purpose). Any other materials inert to  $\text{O}_2$ ,  $\text{CO}_2$ ,  $\text{CO}$ , and  $\text{N}_2$  and resistant to temperature at sampling conditions may be used for the probe; examples of such material are aluminum, copper, quartz glass and Teflon.

2.1.2 Pump. A one-way squeeze bulb, or equivalent, is used to transport the gas sample to the analyzer.

##### 2.2 Integrated Sampling (Figure 3-2).

2.2.1 Probe. A probe such as that described in Section 2.1.1 is suitable.

2.2.2 Condenser. An air-cooled or water-cooled condenser, or other condenser that will not remove  $\text{O}_2$ ,  $\text{CO}_2$ ,  $\text{CO}$ , and  $\text{N}_2$  may be used to remove excess moisture which would interfere with the operation of the pump and flow meter.

2.2.3 Valve. A needle valve is used to adjust sample gas flow rate.

2.2.4 Pump. A leak-free, diaphragm-type pump, or equivalent, is used to transport sample gas to the flexible bag. Install a small surge tank between the pump and rate meter to eliminate the pulsation effect of the diaphragm pump on the rotameter.

2.2.5 Rate Meter. The rotameter, or equivalent rate meter, used should be capable of measuring flow rate to within  $\pm 2$  percent of the selected flow rate. A flow rate range of 500 to 1000  $\text{cm}^3/\text{min}$  is suggested.

2.2.6 Flexible Bag. Any leak-free plastic (e.g., Tedlar, Mylar, Teflon) or plastic-coated aluminum (e.g., aluminized Mylar) bag, or equivalent, having a capacity consistent with the selected flow rate and time

length of the test run, may be used. A capacity in the range of 55 to 90 liters is suggested.

To leak-check the bag, connect it to a water manometer and pressurize the bag to 5 to 10 cm  $\text{H}_2\text{O}$  (2 to 4 in.  $\text{H}_2\text{O}$ ). Allow to stand for 10 minutes. Any displacement in the water manometer indicates a leak. An alternative leak-check method is to pressurize the bag to 5 to 10 cm  $\text{H}_2\text{O}$  (2 to 4 in.  $\text{H}_2\text{O}$ ) and allow to stand overnight. A deflated bag indicates a leak.

2.2.7 Pressure Gauge. A water-filled U-tube manometer, or equivalent, of about 30 cm (12 in.) is used for the flexible bag leak-check.

2.2.8 Vacuum Gauge. A mercury manometer, or equivalent, of at least 760 mm Hg (30 in. Hg) is used for the sampling train leak-check.

2.3 Analysis. For Orsat and Pyrite analyzer maintenance and operation procedures, follow the instructions recommended by the manufacturer, unless otherwise specified herein.

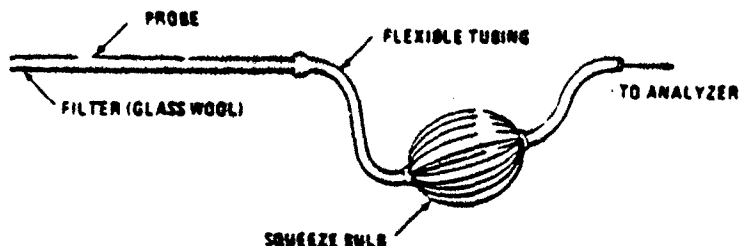


Figure 3-1. Grab sampling train.

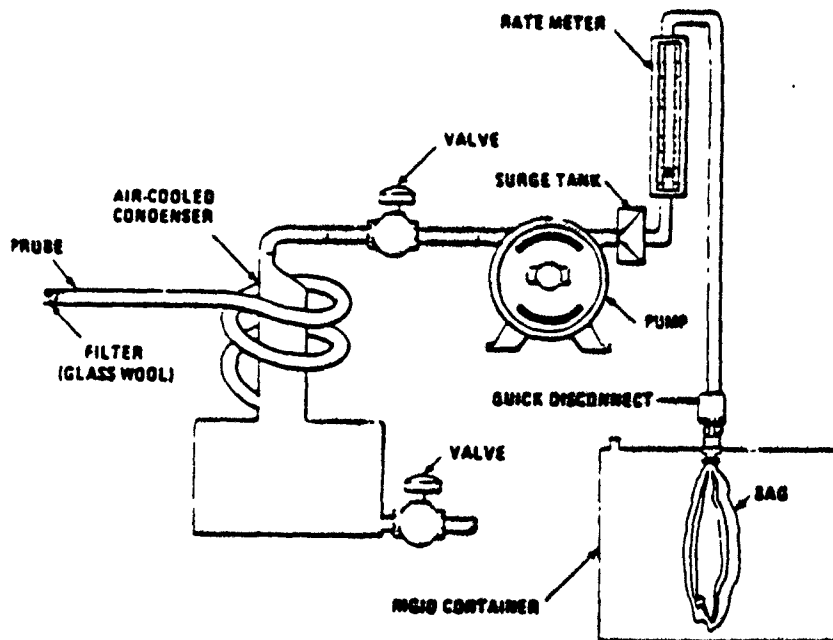


Figure 3-2. Integrated gas-sampling train.

<sup>1</sup>Mention of trade names or specific products does not constitute endorsement by the Environmental Protection Agency.

**2.3.2 Emission Rate Correction Factor or Excess Air Determination.** An Orsat analyzer must be used. For low CO<sub>2</sub> (less than 4.0 percent) or high O<sub>2</sub> (greater than 15.0 percent) concentrations, the measuring burette of the Orsat must have at least 0.1 percent subdivisions.

Any of the three sampling and analytical procedures described below may be used for determining the dry molecular weight.

3.1.1 The sampling point in the duct shall either be at the centroid of the cross section or at a point no closer to the walls than 1.00 m (3.3 ft), unless otherwise specified by the Administrator.

3.1.3 Place the probe in the stack, with the tip of the probe positioned at the sampling point; purge the sampling line. Draw a sample into the analyzer and immediately analyze it for percent CO<sub>2</sub> and percent O<sub>2</sub>. Determine the percentage of the gas that is N<sub>2</sub> and CO by subtracting the sum of the percent CO<sub>2</sub> and percent O<sub>2</sub> from 100 percent. Calculate the dry molecular weight as indicated in Section 6.3.

### 3.2 Single-Point, Integrated Sampling and Analytical Procedure.

3.2.2 Leak-check (optional) the flexible bag as in Section 2.2.6. Set up the equipment as shown in Figure 3-2. Just prior to sampling, leak-check (optional) the train by placing a vacuum gauge at the condenser inlet, pulling a vacuum of at least 250 mm Hg (10 in. Hg), plugging the outlet at the quick disconnect, and then turning off the pump. The vacuum should remain stable for at least 0.5 minute. Evacuate the flexible bag. Connect the probe and place it in the stack, with the tip of the probe positioned at the sampling point; purge the sampling line. Next, connect the bag and make sure that all connections are tight and leak free.

3.2.4 Obtain one integrated flue gas sample during each pollutant emission rate determination. Within 8 hours after the sample is taken, analyze it for percent CO<sub>2</sub> and percent O<sub>2</sub> using either an Orsat analyzer or a Fyrite-type combustion gas analyzer. If an Orsat analyzer is used, it is recommended that the Orsat leak-check described in Section 5 be performed before this determination; however, the check is optional.

3.2.5 Repeat the analysis and calculation procedures until the individual dry molecular weights for any three analyses differ from their mean by no more than 0.3 g/g-mole (0.3 lb/lb-mole). Average these three molecular weights, and report the results to the nearest 0.1 g/g-mole (0.1 lb/lb-mole).

3.3.1 Unless otherwise specified by the Administrator, a minimum of eight traverse

**3.3.2** Follow the procedures outlined in sections 3.2.2 through 3.2.5, except for the following: traverse all sampling points and sample at each point for an equal length of time. Record sampling data as shown in Figure 3-3.

**NOTE:** A Pyrite-type combustion gas analyzer is not acceptable for excess air or emission rate correction factor determination, unless approved by the Administrator. If both percent  $\text{CO}_2$  and percent  $\text{O}_2$  are measured, the analytical results of any of the three procedures given below may also be used for calculating the dry molecular weight.

Each of the three procedures below shall be used only when specified in an applicable subpart of the standards. The use of these procedures for other purposes must have specific prior approval of the Administrator.

4.1.1 The sampling point in the duct shall either be at the centroid of the cross-section or at a point no closer to the walls than 1.00 m (3.3 ft), unless otherwise specified by the Administrator.

4.1.2 Set up the equipment as shown in Figure 3-1, making sure all connections ahead of the analyzer are tight and leak-free. Leak-check the Orsat analyzer according to the procedure described in Section 3. This leak-check is mandatory.

[illegible]

$$\% \text{ Dev.} = (Q - Q_{\text{avg}}) / Q_{\text{avg}} \times 100 \quad (\text{Must be } < 10\%)$$

4.1.4 To insure complete absorption of the  $\text{CO}_2$ ,  $\text{O}_2$ , or if applicable,  $\text{CO}$ , make repeated passes through each absorbing solution until two consecutive readings are the same. Several passes (three or four) should be made between readings. (If consecutive readings cannot be obtained after three consecutive readings, replace the absorbing solution.)

4.1.3 After the analysis is completed, leak-check (mandatory) the Orsat analyzer once again, as described in Section 5. For the results of the analysis to be valid, the Orsat analyzer must pass this leak test before and after the analysis.

**NOTE:** Since this single-point, grab sampling and analytical procedure is normally conducted in conjunction with a single-point, grab sampling and analytical procedure for a pollutant, only one analysis is ordinarily conducted. Therefore, great care must be taken to obtain a valid sample and analysis. Although in most cases only CO, or O<sub>3</sub> is required, it is recommended that both CO, and O<sub>3</sub> be measured, and that Section 4.4 be used to validate the analytical data.

4.2.1 The sampling point in the duct shall be located as specified in Section 4.1.1.

ment as shown in Figure 3-2. Just prior to sampling, leak-check (mandatory) the train by placing a vacuum gauge at the condenser inlet, pulling a vacuum of a least 250 mm Hg (10 in. Hg), plugging the outlet at the quick disconnect, and then turning off the pump. The vacuum shall remain stable for at least 0.5 minute. Evacuate the flexible bag. Connect the probe and place it in the stack, with the tip of the probe positioned at the sampling point; purge the sampling line. Next, connect the bag and make sure that all connections are tight and leak free.

4.2.3 Sample at a constant rate, or as specified by the Administrator. The sampling run must be simultaneous with and for the same total length of time as, the pollutant emission rate determination. Collect at least 30 liters (1.00 ft<sup>3</sup>) of sample gas. Smaller volumes may be collected, subject to approval of the Administrator.

4.2.4 Obtain one integrated flue gas sample during each pollutant emission rate determination. For emission rate correction factor determination, analyze the sample within 4 hours after it is taken for percent CO, or percent O<sub>2</sub> (as outlined in Sections 4.2.5 through 4.2.7). The Orsat analyzer must be leak-checked (see Section 3) before the analysis. If excess air is desired, proceed as follows: (1) within 4 hours after the sample is taken, analyze it (as in Sections 4.2.5 through 4.2.7) for percent CO, O<sub>2</sub>, and CO<sub>2</sub>; (2) determine the percentage of the gas that is N<sub>2</sub> by subtracting the sum of the percent CO, percent O<sub>2</sub>, and percent CO<sub>2</sub> from 100 percent; (3) calculate percent excess air, as outlined in Section 6.2.

July 1990  
Revision: Final

**EPA METHOD 10**  
**DETERMINATION OF CARBON MONOXIDE EMISSIONS**  
**FROM STATIONARY SOURCES**

# **METHOD 10—DETERMINATION OF CARBON MONOXIDE EMISSIONS FROM STATIONARY SOURCES**

## **1. Principle and Applicability.**

1.1 **Principle.** An integrated or continuous gas sample is extracted from a sampling point and analyzed for carbon monoxide (CO) content using a Luft-type nondispersive infrared analyzer (NDIR) or equivalent.

1.2 **Applicability.** This method is applicable for the determination of carbon monoxide emissions from stationary sources only when specified by the test procedures for determining compliance with new source performance standards. The test procedure will indicate whether a continuous or an integrated sample is to be used.

## **2. Range and sensitivity.**

2.1 **Range.** 0 to 1,000 ppm.

2.2 **Sensitivity.** Minimum detectable concentration is 20 ppm for a 0 to 1,000 ppm span.

3. **Interferences.** Any substance having a strong absorption of infrared energy will interfere to some extent. For example, discrimination ratios for water (H<sub>2</sub>O) and carbon dioxide (CO<sub>2</sub>) are 3.5 percent H<sub>2</sub>O per 7 ppm CO and 10 percent CO<sub>2</sub> per 10 ppm CO, respectively, for devices measuring in the 1,500 to 3,000 ppm range. For devices measuring in the 0 to 100 ppm range, interference ratios can be as high as 3.5 percent H<sub>2</sub>O per 25 ppm CO and 10 percent CO<sub>2</sub> per 50 ppm CO. The use of silica gel and ascarite traps will alleviate the major interference problems. The measured gas volume must be corrected if these traps are used.

## **4. Precision and accuracy.**

4.1 **Precision.** The precision of most NDIR analyzers is approximately  $\pm 3$  percent of span.

4.2 **Accuracy.** The accuracy of most NDIR analyzers is approximately  $\pm 5$  percent of span after calibration.

## **5. Apparatus.**

5.1 **Continuous sample (Figure 10-1).**

5.1.1 **Probe.** Stainless steel or sheathed Pyrex<sup>®</sup> glass, equipped with a filter to remove particulate matter.

5.1.2 **Air-cooled condenser or equivalent.** To remove any excess moisture.

5.2 **Integrated sample (Figure 10-2).**

5.2.1 **Probe.** Stainless steel or sheathed Pyrex glass, equipped with a filter to remove particulate matter.

5.2.2 **Air-cooled condenser or equivalent.** To remove any excess moisture.

5.2.3 **Valve.** Needle valve, or equivalent, to adjust flow rate.

5.2.4 **Pump.** Leak-free diaphragm type, or equivalent, to transport gas.

5.2.5 **Rate meter.** Rotameter, or equivalent, to measure a flow range from 0 to 1.0 liter per min. (0.035 cfm).

5.2.6 **Flexible bag.** Tedlar, or equivalent, with a capacity of 60 to 90 liters (2 to 3 ft<sup>3</sup>). Leak-test the bag in the laboratory before using by evacuating bag with a pump fol-

<sup>1</sup>Mention of trade names or specific products does not constitute endorsement by the Environmental Protection Agency.

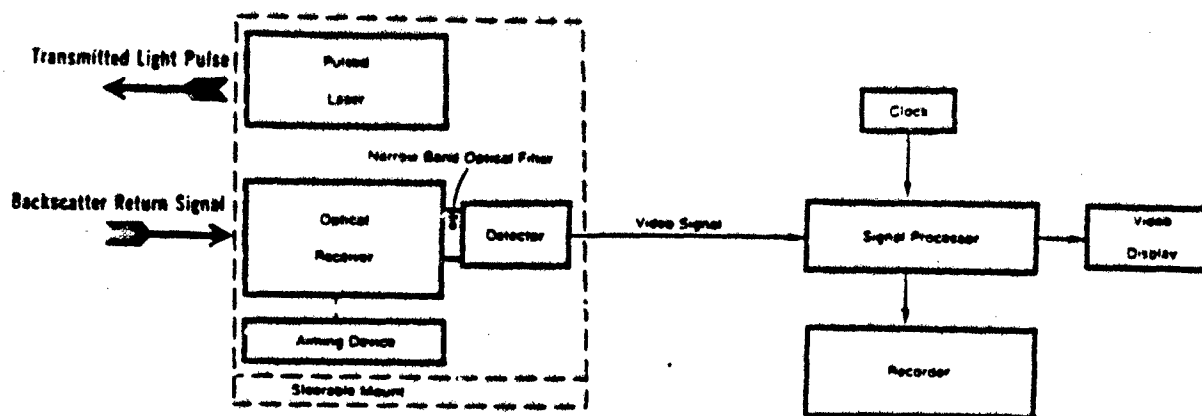


Figure AM1-VII. Functional Block Diagram of a Basic Lidar System



owed by a dry gas meter. When evacuation is complete, there should be no flow through the meter.

5.2.7 **Pilot tube.** Type S, or equivalent, attached to the probe so that the sampling rate can be regulated proportional to the stack gas velocity when velocity is varying with the time or a sample traverse is conducted.

5.3 **Analysis** (Figure 10-3).

5.3.1 **Carbon monoxide analyzer.** Nondisruptive infrared spectrometer, or equivalent. This instrument should be demonstrated, preferably by the manufacturer, to meet or exceed manufacturer's specifications and those described in this method.

5.3.2 **Drying tube.** To contain approximately 200 g of silica gel.

5.3.3 **Calibration gas.** Refer to paragraph 1.1.

5.3.4 **Filter.** As recommended by NDIR manufacturer.

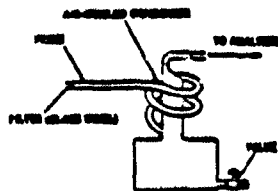


Figure 10-1. Sampling system.

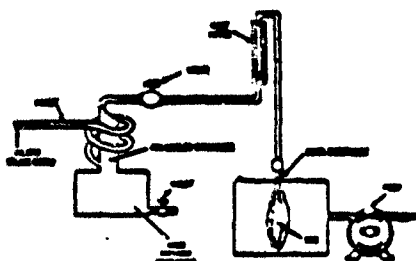


Figure 10-2. Integrated sampling system.

5.3.5 **CO<sub>2</sub> removal tube.** To contain approximately 500 g of ascarite.

5.3.6 **Ice water bath.** For ascarite and silica gel tubes.

5.3.7 **Valve.** Needle valve, or equivalent, to adjust flow rate.

5.3.8 **Rate meter.** Rotameter or equivalent to measure gas flow rate of 0 to 1.0 liter per min. (0.035 cfm) through NDIR.

5.3.9 **Recorder** (optional). To provide permanent record of NDIR readings.

## 6. Reagents

6.1 **Calibration gases.** Known concentration of CO in nitrogen (N<sub>2</sub>) for instrument span, prepurified grade of N<sub>2</sub> for zero, and two additional concentrations corresponding approximately to 60 percent and 30 percent span. The span concentration shall not exceed 1.5 times the applicable source performance standard. The calibration gases shall be certified by the manufacturer to be within  $\pm 2$  percent of the specified concentration.

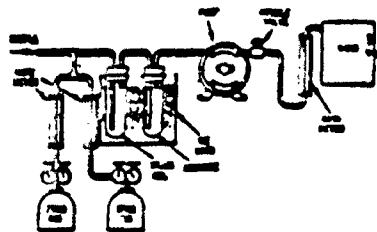


Figure 10-3. Analytical system.

6.2 **Silica gel.** Indicating type, 6 to 16 mesh, dried at 175° C (347° F) for 2 hours.

6.3 **Ascarite.** Commercially available.

## 7. Procedure

### 7.1 Sampling

7.1.1 **Continuous sampling.** Set up the equipment as shown in Figure 10-1 making sure all connections are leak free. Place the probe in the stack at a sampling point and purge the sampling line. Connect the analyzer and begin drawing sample into the analyzer. Allow 5 minutes for the system to stabilize, then record the analyzer reading as required by the test procedure. (See 7.2 and 8). CO<sub>2</sub> content of the gas may be determined by using the Method 3 integrated sample procedure (36 FR 24886), or by weighing the ascarite CO<sub>2</sub> removal tube and computing CO<sub>2</sub> concentration from the gas volume sampled and the weight gain of the tube.

7.1.2 **Integrated sampling.** Evacuate the flexible bag. Set up the equipment as shown in Figure 10-2 with the bag disconnected. Place the probe in the stack and purge the sampling line. Connect the bag, making sure that all connections are leak free. Sample at a rate proportional to the stack velocity. CO<sub>2</sub> content of the gas may be determined by using the Method 3 integrated sample procedure (36 FR 24886), or by weighing the ascarite CO<sub>2</sub> removal tube and computing CO<sub>2</sub> concentration from the gas volume sampled and the weight gain of the tube.

7.2 **CO Analysis.** Assemble the apparatus as shown in Figure 10-3, calibrate the instrument, and perform other required operations as described in paragraph 3. Purge analyzer with N<sub>2</sub> prior to introduction of each sample. Direct the sample stream through the instrument for the test period, recording the readings. Check the zero and span again after the test to assure that any drift or malfunction is detected. Record the sample data on Table 10-1.

8. **Calibration.** Assemble the apparatus according to Figure 10-3. Generally an instrument requires a warm-up period before stability is obtained. Follow the manufacturer's instructions for specific procedure. Allow a minimum time of 1 hour for warm-up. During this time check the sample conditioning apparatus, i.e., filter, condenser, drying tube, and CO<sub>2</sub> removal tube, to ensure that each component is in good operating condition. Zero and calibrate the instrument according to the manufacturer's procedures using, respectively, nitrogen and the calibration gases.

TABLE 10-1—FIELD DATA

Comments	
Location	
Date	
Operator	
Check time	Rotameter setting, flow per minute (check test per minute)

9. **Calculation—Concentration of carbon monoxide.** Calculate the concentration of carbon monoxide in the stack using equation 10-1.

$$C_{\text{CO}} = C_{\text{NDIR}}(1 - F_{\text{CO}_2})$$

where:

$C_{\text{CO}}$  = concentration of CO in stack, ppm by volume (dry basis).

$C_{\text{NDIR}}$  = concentration of CO measured by NDIR analyzer, ppm by volume (dry basis).

$F_{\text{CO}_2}$  = volume fraction of CO<sub>2</sub> in sample, i.e., percent CO<sub>2</sub> from Orsat analysis divided by 100.

## 10. Bibliography

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- Jacobs, M. R., et al. Continuous Determination of Carbon Monoxide and Hydrocarbons in Air by a Modified Infrared Analyzer. J. Air Pollution Control Association, 13: 119-114, August 1969.
- MSA LIRA Infrared Gas and Liquid Analyzer Instruction Book, Mine Safety Appliances Co., Technical Products Division, Pittsburgh, Pa.
- Models 215A, 315A, and 415A Infrared Analyzers, Beckman Instruments, Inc., Beckman Instructions 1635-B, Fullerton, Calif., October 1967.
- Continuous CO Monitoring System, Model AS611, InterTech Corp., Princeton, N.J.
- UNOP Infrared Gas Analyzers, Bendix Corp., Roncovere, West Virginia.

## Appendix—A. PERFORMANCE SPECIFICATIONS FOR NDIR CARBON MONOXIDE ANALYZERS.

Range (pressure)	0-1000 ppm.
Output (pressure)	0-100V.
Minimum detectable concentration	20 ppm.
Repeatability	20 percent.
Reliability	20 percent.
Zero drift (pressure)	10% in 8 hours.
Span drift (pressure)	10% in 8 hours.
Pressure (pressure)	±2% of full scale.
Moisture (pressure)	±1% of full scale.
Leakage (pressure)	2% of full scale.
Interference (pressure)	CO—1000 to 1, H <sub>2</sub> O—500 to 1.

### B. Definitions of Performance Specifications

**Range**—The minimum and maximum measurement limits.

**Output**—Electrical signal which is proportional to the measurement; intended for connection to readout or data processing devices. Usually expressed as millivolts or milliamperes full scale at a given impedance.

**Full scale**—The maximum measuring limit for a given range.

**Minimum detectable sensitivity**—The smallest amount of input concentration that can be detected as the concentration approaches zero.

**Accuracy**—The degree of agreement between a measured value and the true value; usually expressed as  $\pm$  percent of full scale.

**Time to 90 percent response**—The time interval from a step change in the input concentration at the instrument inlet to a reading of 90 percent of the ultimate recorded concentration.

**Rise Time (90 percent)**—The interval between initial response time and time to 90 percent response after a step increase in the inlet concentration.

**Fall Time (90 percent)**—The interval between initial response time and time to 90 percent response after a step decrease in the inlet concentration.

**Zero Drift**—The change in instrument output over a stated time period, usually 24 hours, of unadjusted continuous operation when the input concentration is zero; usually expressed as percent full scale.

**Span Drift**—The change in instrument output over a stated time period, usually 24 hours, of unadjusted continuous operation when the input concentration is a stated upscale value; usually expressed as percent full scale.

**Precision**—The degree of agreement between repeated measurements of the same concentration, expressed as the average deviation of the single results from the mean.

**Noise**—Spontaneous deviations from a mean output not caused by input concentration changes.

**Linearity**—The maximum deviation between an actual instrument reading and the reading predicted by a straight line drawn between upper and lower calibration points.

July 1990  
Revision: Final

**EPA METHOD 4**  
**DETERMINATION OF MOISTURE CONTENT IN STACK GASES**

#### METHOD 4—DETERMINATION OF MOISTURE CONTENT IN STACK GASES

##### 1. Principle and Applicability

1.1 Principle. A gas sample is extracted at a constant rate from the source; moisture is removed from the sample stream and determined either volumetrically or gravimetrically.

1.2 Applicability. This method is applicable for determining the moisture content of stack gas.

Two procedures are given. The first is a reference method, for accurate determinations of moisture content (such as are needed to calculate emission data). The second is an approximation method, which provides estimates of percent moisture to aid in setting isokinetic sampling rates prior to a pollutant emission measurement run. The approximation method described herein is only a suggested approach; alternative means for approximating the moisture content, e.g., drying tubes, wet bulb-dry bulb techniques, condensation techniques, stoichiometric calculations, previous experience, etc., are also acceptable.

The reference method is often conducted simultaneously with a pollutant emission measurement run; when it is, calculation of percent isokinetic, pollutant emission rate, etc., for the run shall be based upon the results of the reference method or its equivalent; these calculations shall not be based upon the results of the approximation method, unless the approximation method is shown, to the satisfaction of the Administrator, U.S. Environmental Protection Agency, to be capable of yielding results within 1 percent H<sub>2</sub>O of the reference method.

NOTE The reference method may yield questionable results when applied to saturated gas streams or to streams that contain water droplets. Therefore, when these conditions exist or are suspected, a second determination of the moisture content shall be made simultaneously with the reference method, as follows: Assume that the gas stream is saturated. Attach a temperature sensor (capable of measuring to  $\pm 1^\circ\text{C}$  ( $2^\circ\text{F}$ )) to the reference method probe. Measure the stack gas temperature at each traverse point (see Section 2.2.1) during the reference method traverse; calculate the average stack gas temperature. Next, determine the moisture percentage, either by: (1) using a psychrometric chart and making appropriate corrections if stack pressure is different from that of the chart, or (2) using saturation vapor pressure tables. In cases where the psychrometric chart or the saturation vapor pressure tables are not applicable (based on evaluation of the process), alternate methods, subject to the approval of the Administrator, shall be used.

##### 2. Reference Method

The procedure described in Method 5 for determining moisture content is acceptable as a reference method.

2.1 Apparatus. A schematic of the sampling train used in this reference method is shown in Figure 4-1. All components shall be maintained and calibrated according to the procedure outlined in Method 5.

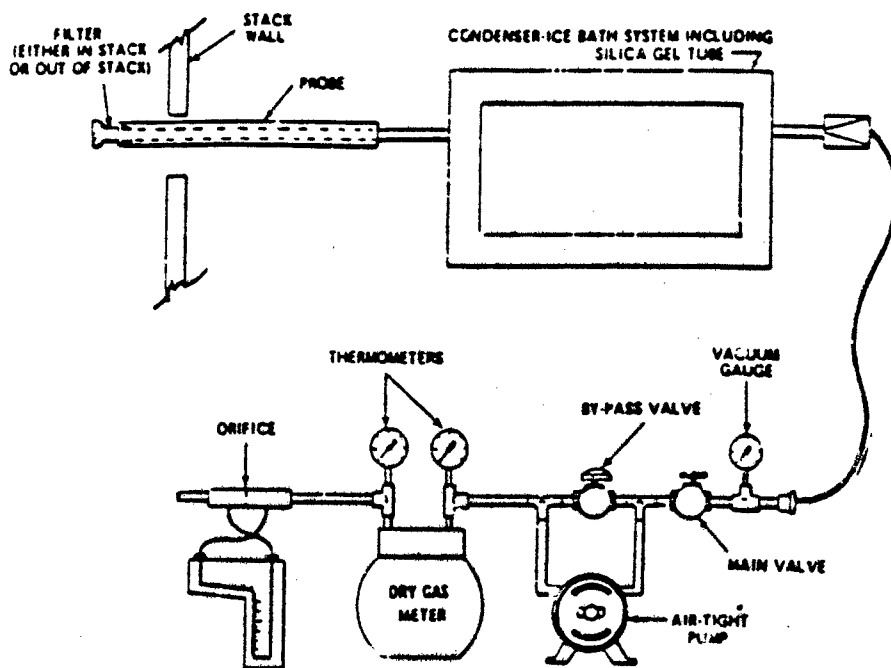


Figure 4-1. Moisture sampling train-reference method

2.1.1 Probe. The probe is constructed of stainless steel or glass tubing, sufficiently heated to prevent water condensation, and is equipped with a filter, either in-stack (e.g., a plug of glass wool inserted into the end of the probe) or heated out-stack (e.g., as described in Method 5), to remove particular matter.

When stack conditions permit, other metals or plastic tubing may be used for the probe, subject to the approval of the Administrator.

2.1.2 Condenser. The condenser consists of four impingers connected in series with ground glass, leak-free fittings or any similarly leak-free non-contaminating fittings. The first, third, and fourth impingers shall be of the Greenburg-Smith design, modified by replacing the tip with a 1.3 centimeter ( $\frac{1}{2}$  inch) ID glass tube extending to about 1.3 cm ( $\frac{1}{2}$  in.) from the bottom of the flask. The second impinger shall be of the Greenburg-Smith design with the standard tip. Modifications (e.g., using flexible connections between the impingers, using materials other than glass, or using flexible vacuum lines to connect the filter holder to the condenser) may be used, subject to the approval of the Administrator.

The first two impingers shall contain known volumes of water, the third shall be empty, and the fourth shall contain a known weight of 6- to 18-mesh indicating type silica gel, or equivalent desiccant. If the silica gel has been previously used, dry at  $175^\circ\text{C}$  ( $350^\circ\text{F}$ ) for 2 hours. New silica gel may be used as received. A thermometer, capable of measuring temperature to within  $1^\circ\text{C}$  ( $2^\circ\text{F}$ ), shall be placed at the outlet of the fourth impinger, for monitoring purposes.

Alternatively, any system may be used (subject to the approval of the Administrator) that cools the sample gas stream and allows measurement of both the water that has been condensed and the moisture leaving the condenser, each to within 1 ml or 1 g. Acceptable means are to measure the condensed water, either gravimetrically or volumetrically, and to measure the moisture leaving the condenser by: (1) monitoring the temperature and pressure at the exit of the condenser and using Dalton's law of partial pressures, or (2) passing the sample gas stream through a tared silica gel (or equivalent desiccant) trap, with exit gases kept below  $20^\circ\text{C}$  ( $68^\circ\text{F}$ ), and determining the weight gain.

If means other than silica gel are used to determine the amount of moisture leaving the condenser, it is recommended that silica gel (or equivalent) still be used between the condenser system and pump, to prevent moisture condensation in the pump and metering devices and to avoid the need to make corrections for moisture in the metered volume.

**2.1.6 Graduated Cylinder and/or Balance.** These items are used to measure condensed water and moisture caught in the silica gel to within 1 ml or 0.5 g. Graduated cylinders shall have subdivisions no greater than 2 ml. Most laboratory balances are capable of weighing to the nearest 0.5 g or less. These balances are suitable for use.

2.2.1 Unless otherwise specified by the Administrator, a minimum of eight traverse points shall be used for circular stacks having diameters less than 0.61 m (24 in.), a minimum of nine points shall be used for rectangular stacks having equivalent diameters less than 0.61 m (24 in.), and a minimum of twelve traverse points shall be used in all other cases. The traverse points shall be located according to Method 1. The use of fewer points is subject to the approval of the Administrator. Select a suitable probe and probe length such that all traverse points can be sampled. Consider sampling from opposite sides of the stack (four total sampling ports) for large stacks, to permit use of shorter probe lengths. Mark the probe with heat resistant tape or by some other method to denote the proper distance into the stack or duct for each sampling point. Place known volumes of water in the first two impingers. Weigh and record the weight of the silica gel to the nearest 0.5 g, and transfer the silica gel to the fourth impinger; alternatively, the silica gel may first be transferred to the impinger, and the weight of the silica gel plus impinger recorded.

2.2.4 During the sampling run, maintain a sampling rate within 10 percent of constant rate, or as specified by the Administrator. For each run, record the data re-

[illegible]

quired on the example data sheet shown in Figure 4-2. Be sure to record the dry gas meter reading at the beginning and end of each sampling time increment and whenever sampling is halted. Take other appropriate readings at each sample point, at least once during each time increment.

2.2.5 To begin sampling, position the probe tip at the first traverse point. Immediately start the pump and adjust the flow to the desired rate. Traverse the cross section, sampling at each traverse point for an equal length of time. Add more ice and, if necessary, salt to maintain a temperature of less 20° C (68° F) at the silica gel outlet.

2.2.6 After collecting the sample, disconnect the probe from the filter holder (or from the first impinger) and conduct a leak check (mandatory) as described in Section 2.2.3. Record the leak rate. If the leakage rate exceeds the allowable rate, the tester shall either reject the test results or shall correct the sample volume as in Section 6.3 of Method 5. Next, measure the volume of the moisture condensed to the nearest ml. Determine the increase in weight of the silica gel (or silica gel plus impinger) to the nearest 0.5 g. Record this information (see example data sheet, Figure 4-3) and calculate the moisture percentage, as described in 2.3 below.

2.2.7 A quality control check of the volume metering system at the field site is suggested before collecting the sample following the procedure in Method 5, Section 4.4.

2.3 Calculations. Carry out the following calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after final calculation.

FIGURE 4-3—ANALYTICAL DATA—REFERENCE METHOD

	Impinger volume, ml	Silica gel weight, g
Final		
Initial		
Difference		

### 2.3.1 Nomenclature.

$B_w$  = Proportion of water vapor, by volume, in the gas stream.

$M_w$  = Molecular weight of water, 18.0 g/g-mole (18.0 lb/lb-mole).

$P_a$  = Absolute pressure (for this method, same as barometric pressure) at the dry gas meter, mm Hg (in. Hg).

$P_{std}$  = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).

$R$  = Ideal gas constant, 0.08206 (mm Hg) (m<sup>3</sup>)/(g-mole) (°K) for metric units and 21.85 (in. Hg) (ft<sup>3</sup>)/(lb-mole) (°R) for English units.

$T_a$  = Absolute temperature at meter, °K (°R).

$T_{std}$  = Standard absolute temperature, 293 K (528°R).

$V_x$  = Dry gas volume measured by dry gas meter, dcm (dcf).

$\Delta V_x$  = Incremental dry gas volume measured by dry gas meter at each traverse point, dcm (dcf).

$V_{x, std}$  = Dry gas volume measured by the dry gas meter, corrected to standard conditions, dscm (dscf).

$V_{w, std}$  = Volume of water vapor condensed corrected to standard conditions, scm (scf).

$V_{w, std}$  = Volume of water vapor collected in silica gel corrected to standard conditions, scm (scf).

$V_f$  = Final volume of condenser water, ml.

$V_i$  = Initial volume, if any, of condenser water, ml.

$W_f$  = Final weight of silica gel or silica gel plus impinger, g.

$W_i$  = Initial weight of silica gel or silica gel plus impinger, g.

$Y$  = Dry gas meter calibration factor.

$\rho_w$  = Density of water, 0.9982 g/ml (0.002201 lb/ml).

### 2.3.2 Volume of water vapor condensed.

$$V_{w, std} = \frac{(V_f - V_i) \rho_w RT_{std}}{P_{std} M_w}$$

$$= K_1 (V_f - V_i)$$

Equation 4-1

where:

$K_1 = 0.001333 \text{ m}^3/\text{ml}$  for metric units  
 $= 0.04707 \text{ ft}^3/\text{ml}$  for English units

### 2.3.3 Volume of water vapor collected in silica gel.

$$V_{w, std} = \frac{(W_f - W_i) RT_{std}}{P_{std} M_w}$$

$$= K_2 (W_f - W_i)$$

Equation 4-2

where:

$K_2 = 0.001335 \text{ m}^3/\text{g}$  for metric units  
 $= 0.04715 \text{ ft}^3/\text{g}$  for English units

### 2.3.4 Sample gas volume.

$$V_{x, std} = V_x Y \frac{(P_a)(T_{std})}{(P_{std})(T_a)}$$

$$= K_3 Y \frac{V_x P_a}{T_a}$$

Equation 4-3

where:

$K_3 = 0.3858 \text{ } ^\circ\text{K}/\text{mm Hg}$  for metric units  
 $= 17.84 \text{ } ^\circ\text{R}/\text{in. Hg}$  for English units

Note: If the post-test leak rate (Section 2.2.6) exceeds the allowable rate, correct the value of  $V_x$  in Equation 4-3, as described in Section 6.3 of Method 5.

### 2.3.5 Moisture Content.

$$B_w = \frac{V_{w, std} - V_{w, std}}{V_{x, std} - V_{w, std} + V_{w, std}}$$

Equation 4-4

Note: In saturated or moisture droplet-laden gas streams, two calculations of the moisture content of the stack gas shall be made, one using a value based upon the saturated conditions (see Section 1.2), and

another based upon the results of the impinger analysis. The lower of these two values of  $B_w$  shall be considered correct.

2.3.6 Verification of constant sampling rate. For each time increment, determine the  $\Delta V_x$ . Calculate the average. If the value for any time increment differs from the average by more than 10 percent, reject the results and repeat the run.

### 3. Approximation Method

The approximation method described below is presented only as a suggested method (see Section 1.2).

#### 3.1 Apparatus.

3.1.1 Probe. Stainless steel glass tubing, sufficiently heated to prevent water condensation and equipped with a filter (either in-stack or heated out-stack) to remove particulate matter. A plug of glass wool, inserted into the end of the probe, is a satisfactory filter.

3.1.2 Impingers. Two midjet impingers, each with 30 ml capacity, or equivalent.

3.1.3 Ice Bath. Container and ice, to aid in condensing moisture in impingers.

3.1.4 Drying Tube. Tube packed with new or regenerated 6- to 16-mesh indicating-type silica gel (or equivalent desiccant), to dry the sample gas and to protect the meter and pump.

3.1.5 Valve. Needle valve, to regulate the sample gas flow rate.

3.1.6 Pump. Leak-free, diaphragm type, or equivalent, to pull the gas sample through the train.

3.1.7 Volume Meter. Dry gas meter, sufficiently accurate to measure the sample volume within 2%, and calibrated over the range of flow rates and conditions actually encountered during sampling.

3.1.8 Rate Meter. Rotameter, to measure the flow range from 0 to 3 lpm (0 to 0.11 cfm).

3.1.9 Graduated Cylinder. 25 ml.

3.1.10 Barometer. Mercury, aneroid, or other barometer, as described in Section 2.1.5 above.

3.1.11 Vacuum Gauge. At least 760 mm Hg (30 in. Hg) gauge, to be used for the sampling leak check.

#### 3.2 Procedure.

3.2.1 Place exactly 5 ml distilled water in each impinger.

Leak check the sampling train as follows: Temporarily insert a vacuum gauge at or near the probe inlet; then, plug the probe inlet and pull a vacuum of at least 250 mm Hg (10 in. Hg). Note, the time rate of change of the dry gas meter dial; alternatively, a rotameter (0-40 cc/min) may be temporarily attached to the dry gas meter outlet to determine the leakage rate. A leak rate not in excess of 2 percent of the average sampling rate is acceptable.

Note: Carefully release the probe inlet plug before turning off the pump.

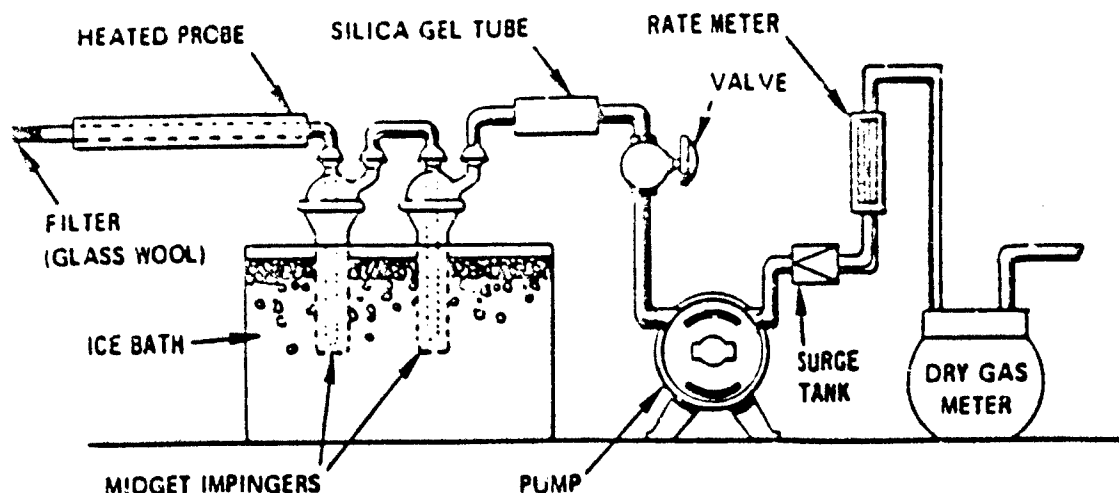


Figure 4-4. Moisture-sampling train - approximation method.

FIGURE 4-5—FIELD MOISTURE DETERMINATION—APPROXIMATION METHOD

Location \_\_\_\_\_  
 Date \_\_\_\_\_  
 Operator \_\_\_\_\_  
 Barometric pressure \_\_\_\_\_

Check time	Gas volume through meter, (V <sub>sc</sub> ), ml (cc)	Rate meter reading, (R), ml (cc) / min	Water temperature, C (°F)

3.2.2 Connect the probe, insert it into the stack, and sample at a constant rate of 2 lpm (0.071 cfm). Continue sampling until the dry gas meter registers about 30 liters (1.1 ft<sup>3</sup>) or until visible liquid droplets are carried over from the first impinger to the second. Record temperature, pressure, and dry gas meter readings as required by Figure 4-5.

3.2.3 After collecting the sample, combine the contents of the two impingers and measure the volume to the nearest 0.5 ml.

3.3 Calculations. The calculation method presented is designed to estimate the moisture in the stack gas; therefore, other data, which are only necessary for accurate moisture determinations, are not collected. The following equations adequately estimate the moisture content, for the purpose of determining isokinetic sampling rate settings.

#### 3.3.1 Nomenclature.

$B_w$  = Approximate proportion, by volume, of water vapor in the gas stream leaving the second impinger, 0.025.

$B_m$  = Water vapor in the gas stream, proportion by volume.

$M_w$  = Molecular weight of water, 18.0 g/g-mole (18.0 lb/lb-mole).

$P_a$  = Absolute pressure (for this method, same as barometric pressure) at the dry gas meter.

$P_{std}$  = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).

$R$  = Ideal gas constant, 0.06236 (mm Hg) (m<sup>3</sup>)/(g-mole) (°K) for metric units and 21.85 (in. Hg) (ft<sup>3</sup>)/lb-mole (°R) for English units.

$T_a$  = Absolute temperature at meter, °K (°R).

$T_{std}$  = Standard absolute temperature, 293° K (528° R).

$V_a$  = Final volume of impinger contents, ml.

$V_i$  = Initial volume of impinger contents, ml.

$V_d$  = Dry gas volume measured by dry gas meter, dcm (def).

$V_{dsc}$  = Dry gas volume measured by dry gas meter, corrected to standard conditions, dcm (dscf).

$V_{wsc}$  = Volume of water vapor condensed, corrected to standard conditions, scm (scf).

$\rho_w$  = Density of water, 0.9982 g/ml (0.002201 lb/ml).

$Y$  = Dry gas meter calibration factor.

3.3.2 Volume of water vapor collected.

where:

$$V_{wsc} = \frac{(V_i - V_a) B_w RT_{std}}{P_{std} M_w}$$

$$= K_1 (V_i - V_a)$$

#### Equation 4-5

$K_1 = 0.001333$  m<sup>3</sup>/ml for metric units  
 $= 0.04707$  ft<sup>3</sup>/ml for English units.

3.3.3 Gas volume.

$$V'_{sc} = V'_{sc} \left( \frac{P_a}{P_{std}} \right) \left( \frac{T_{std}}{T_a} \right)$$

$$= K_2 \frac{V'_{sc} P_a}{T_a}$$

Equation 4-6

where:

$K_2 = 0.3858$  °K/mm Hg for metric unit  
 $= 17.64$  °R/in. Hg for English units

3.3.4 Approximate moisture content

$$B_w = \frac{V_{wsc}}{V_{dsc} + V_{wsc}} + B_m$$

$$= \frac{V'_{sc}}{V'_{sc} + V_{wsc}} + B_m$$

Equation 4-7

#### 4. Calibration

4.1 For the reference method, use equipment as specified in the following: Method 3: Section 5.3 (meter system); Section 5.5 (temperature and Section 5.7 (barometer). The intended leak check of the metering (Section 5.6 of Method 3) also applies reference method. For the approximation method, use the procedures outlined in Section 3.3.1 of Method 6 to calibrate the metering system, and the procedure of Method 3, Section 5.7 to calibrate the barometer.

#### 5. Bibliography

1. Air Pollution Engineering & (Second Edition). Danielson, J. A. (ed). Environmental Protection Agency, Office of Air Quality Planning and Standard Research Triangle Park, N.C. Publication AP-46, 1973.

2. Devorkin, Howard, et al. Air Poll Source Testing Manual. Air Pollution Control District, Los Angeles, Calif. Nov 1963.

3. Methods for Determination of Volume Dust and Mist Content of Western Precipitation Division of Joy Manufacturing Co., Los Angeles, Calif. BP-WP-50, 1949.

July 1990  
Revision: Final

## **EPA WIPE SAMPLING TECHNIQUE**



## SECTION 13

### SPECIALIZED SAMPLING TECHNIQUES

#### 13.0 GENERAL

This section discusses several specialized sampling techniques that have been used by contractors on hazardous waste sites. The reader may develop other techniques for specific site needs. In those cases and in cases where the techniques listed here are modified for use on a specific site, careful documentation of the exact procedures used should be provided. This section does not discuss analytical techniques, since analytical methods would vary depending on the data quality objectives, the compounds of concern, the media, and the exact sampling technique. The Contract Laboratory Program plans to issue a "Field Methodology Catalog" in the summer of 1987 that will contain field analytical techniques suitable for analyses of the samples collected by using the techniques in this section.

#### 13.1 WIPE SAMPLING

##### 13.1.1 Scope and Purpose

This guideline discusses the steps required for obtaining a wipe sample. Wipe samples may be used to document the presence of carcinogenic substances or other toxic materials. In addition, wipe sampling is commonly used to ascertain that site or equipment decontamination has been acceptably effective.

##### 13.1.2 Definitions

###### Site Manager (SM)

The individual responsible for the successful completion of a work assignment within budget and schedule. This person is also referred to as the Site Project Manager or the Project Manager and is typically a contractor's employee (see Subsection 1.1).

###### Wipe Sample

A sample used to assess surface contamination. The terms "wipe sample," "swipe sample," and "smear sample" have all been used synonymously. For purposes of this section, the sample will be termed "wipe sample."

##### 13.1.3 Applicability

This guideline is applicable when a sample of the substances on a surface is needed. Surfaces may include walls, floors, ceilings, desk tops, equipment, or other large objects that are potentially contaminated.

##### 13.1.4 Responsibilities

The SM or designee is responsible for deciding when wipe sampling is needed.

Field personnel are responsible for performing the actual sampling, maintaining sample integrity, and preparing the proper chain-of-custody forms.

### 13.1.5 Records

Records of wipe sampling include completed chain-of-custody forms and appropriate entries in the field logbook. If the sample collected is to be analyzed using the National Contract Laboratory Program (CLP), then CLP forms must be completed as discussed in Section 5.

### 13.1.6 Procedures

Wipe sampling can be an integral part of the overall sampling program. Wipe sampling can help to provide a picture of contaminants that exist on the surface of drums, tanks, equipment, or buildings on a hazardous waste site or that exist in the homes of a populace at risk.

Wipe sampling consists of rubbing a moistened filter paper over a measured area of 100 cm<sup>2</sup> to 1 m<sup>2</sup>. The paper is then sent to the laboratory for analysis. The results are related back to the known area of the sample. A proper sampling procedure is essential to ensure a representative, uncontaminated sample.

#### 13.1.6.1 Equipment Required

The following equipment is needed for wipe sampling:

- Whatman 541 filter paper or equivalent, 15 cm
- Disposable, chemical-protective gloves
- Solvent to wet filter paper

#### 13.1.6.2 Wipe Sampling Steps

The steps involved in obtaining a wipe sample are listed below:

- Using a clean, impervious disposable glove, such as a surgeon's glove, remove a filter paper from the box. (Note: Although it is necessary to change the glove if it touches the surface being wiped, a new glove should be used for each sample to avoid cross contamination of samples. A new glove should always be used when collecting a new sample.)
- Moisten the filter with a collection medium selected to dissolve the contaminants of concern as specified in the sampling plan. Typically, organic-free water or the solvent used in analysis is used. The filter should be wet but not dripping.
- Thoroughly wipe approximately 1 m<sup>2</sup> of the area with the moistened filter. Using a 1 m<sup>2</sup> stencil will help in judging the size of the wipe area. If a different size area is wiped, record the change in the field logbook. If the surface is not flat, be sure to wipe any crevices or depressions.

- Without allowing the filter to contact any other surface, fold it with the exposed side in, and then fold it over to form a 90-degree angle in the center of the filter.
- Place the filter (angle first) into a clean glass jar, replace the top, seal the jar according to quality assurance requirements, and send the sample to the appropriate laboratory.
- Prepare a blank by moistening a filter with the collection medium. Place the blank in a separate jar, and submit it with the other samples.
- Document the sample collection in the field logbook and on appropriate forms, and ship samples per procedures listed in Section 6.

### 13.1.7 Region-Specific Variances

No region-specific variances have been identified; however, all future variances will be incorporated in subsequent revision to this compendium. Information on variances may become dated rapidly. Thus, users should contact the regional EPA RPM for full details on current regional practices and requirements.

### 13.1.8 Information Sources

EBASCO. "Dioxin Sampling." *REM III Program Guidelines*. Prepared for U.S. Environmental Protection Agency. 28 February 1986.

NUS Corporation. "Site-Specific Site Operations Plans." REM/FIT Contract.

## 13.2 HUMAN HABITATION SAMPLING

### 13.2.1 Scope and Purpose

This subsection provides general guidance for the planning, method selection, and implementation of sampling activities used to determine the potential for human exposure to contaminants that are present in residential environment.

### 13.2.2 Definitions

#### Human Habitation Areas

Any place people may spend extended periods of time, such as their homes or offices.

### 13.2.3 Applicability

This subsection discusses sampling techniques that are similar in collection methodology to other types of samples, such as environmental soil and water, but are biased to emphasize potential human exposure to contaminants moving into the residential environment.

July 1990  
Revision: Final

**MODIFIED METHOD I.W02**  
**ANALYSIS OF EXPLOSIVES IN SOIL, WIPE, AND**  
**RINSATE SAMPLES**

1311R2

## ANALYSIS OF EXPLOSIVES IN SOIL, WIPE, AND RINSATE SAMPLES

### I. SUMMARY

#### A. Analytes:

HMX	Octahydro-1,3,5,7-tetranitro-1,3,5,7-tetrazocine
RDX	Hexahydro-1,3,5-trinitro-s-triazine
NB	Nitrobenzene
1,3-DNB	1,3-Dinitrobenzene
1,3,5-TNB	1,3,5-Trinitrobenzene
2,4-DNT	2,4-Dinitrotoluene
2,6-DNT	2,6-Dinitrotoluene
2,4,6-TNT	2,4,6-Trinitrotoluene
Tetryl	2,4,6-Trinitrophenylmethylnitramine

B. Matrix: Extracts from soil, wipe, or rinsate samples.

C. General Method: Sample matrix is extracted with acetonitrile. The extract is diluted with methanol and water, and the resultant solution is injected onto the HPLC for analysis.

D. This method is based on USATHAMA Method LW02, Explosives in Soil.

### II. SAFETY INFORMATION

Work in well ventilated areas. Wear adequate protective clothing to avoid skin contact. Wash skin with soap and water thoroughly immediately after contact.

TNB, HMX, RDX, Tetryl, and TNTs are classified as Explosives A by DOT. Avoid extreme temperatures and pressures.

### III. APPARATUS AND CHEMICALS

#### A. Glassware/Hardware

1. Syringes: 10 uL, 50 uL, 100 uL, 1 mL syringe (Hamilton 1005 TEFL).
2. Vials with teflon-lined caps or septa. Nominal volume of 1.8 mL, 4.0 mL, and 12 mL.
3. B-D Glaspak disposable syringes, 5 mL, with frosted tip.
4. 0.2 micron fluorocarbon filters.

5. Micropipettes, 200 uL.
6. Hypo needles.
7. 2 mL and 20 mL pipette.
8. Whatman #42 ashless 9 cm filter paper.

B. Instrumentation

1. Perkin-Elmer Series 4 High Performance Liquid Chromatograph (HPLC) equipped with a Perkin-Elmer ISS100 Auto-Injector and Micromeritics Model 786 UV/VIS variable wavelength detector. Hewlett-Packard 3390 recording integrator in peak height mode was used to record data output. Equivalent instrumentation may be substituted.

2. Analytical Balance

Capable of weighing 0.01 gram for sample preparation and 0.1 mg for standard preparation. Mettler AE 163 or equivalent.

3. Parameters

- a. Columns:

- 1) DuPont Zorbax<sup>R</sup> ODS 4.6 mm i.d. x 25 cm HPLC column with a particle size of 5 to 6 microns.
- 2) DuPont Permaphase<sup>R</sup> ODS guard column (optional).

- b. Mobile Phase:

50% water  
34% methanol  
16% acetonitrile

- c. Flow: 1.6 mL/min with a pressure of approximately 2860 psig.

- d. Detector: 250 nm

- e. Injection Volume: 50 uL

C. Reagents and SARMS:

1. Acetonitrile, distilled in glass for HPLC use.

2. Methanol, distilled in glass for HPLC use.
3. Water, distilled in glass for HPLC use.
4. USATHAMA Standard Soil.
5. SARMS

HMX SARM No. 1217 (PA 1303)  
RDX SARM No. 1130 (PA 1302)  
NB SARM No. (PA 1306)  
1,3-DNB SARM No. 2250 (PA 1305)  
1,3,5-TNB SARM No. 1154 (PA 1300)  
2,4-DNT SARM No. 1147 (PA 1298)  
2,6-DNT SARM No. 1148 (PA 1299)  
2,4,6-TNT SARM No. 1129 (PA 1297)  
Tetryl SARM No. 1149 (PA 1301)

#### IV. CALIBRATION

##### A. Initial Calibration

##### 1. Preparation of Standards

- a. Stock calibration solutions containing approximately 10,000 mg/L of a nitro-compound are prepared by accurately weighing ca. 50 mg of a SARM into a 5-mL serum bottle and dissolving the nitro-compound in 5 mL of acetonitrile pipetted into the bottle. All stock solutions prepared in this manner and stored in a freezer (0°C to -4°C) have remained stable for a period of 6 months.
- b. Intermediate Calibration Standards: All compounds appear to be stable for at least 3 months.
  - 1) Intermediate Calibration Standard A (high level): Combine the appropriate volumes of stock calibration standard as shown below. Dilute to 10 mL with acetonitrile and seal with a teflon-lined cap. Store in the dark at 4°C. The resulting solution will have the concentrations indicated in the following table.

1248E

<u>Nitro-compound</u>	<u>uL of Stock Cal Std.</u>	<u>Resulting Concentration (ug/mL)</u>
HMX	127	127
RDX	98	98
NB	42	42
1,3-DNB	59	59
1,3,5-TNB	209	209
2,4-DNT	42	42
2,6-DNT	40	40
2,4,6-TNT	192	192
Tetryl	500	500

- 2) Intermediate Calibration Standard B (low level): 1:10 dilution of the Intermediate Calibration Standard A is made in acetonitrile. Seal with a teflon-lined cap and store in the dark at 4°C. The resulting solution will have the following concentrations:

<u>Nitro-compound</u>	<u>Resulting conc. (ug/mL)</u>
HMX	12.7
RDX	9.80
NB	4.20
1,3-DNB	5.90
1,3,5-TNB	20.9
2,4-DNT	4.20
2,6-DNT	4.00
2,4,6-INT	19.2
Tetryl	50.0

- c. Working Calibration Standards: Using the following table, prepare a series of nine calibration standards. Place the mobile phase into a 1-mL serum vial. Inject the indicated volumes of Intermediate Calibration Standard A or B into the acetonitrile with a microliter syringe. Seal the vial with a teflon-lined septum and cap. Mix well. These solutions are prepared fresh daily and kept in the dark.



## WORKING CALIBRATION STANDARDS

<u>Concentration</u>	<u>Intermediate Cal Std A (uL)</u>	<u>Intermediate Cal Std B (uL)</u>	<u>Mobile Phase (uL)</u>
0X	0	0	1,000
0.5X	-	6.25	994
1X	-	12.5	988
2X	-	25	975
5X	-	62.5	938
10X	12.5	-	988
20X	25	-	975
50X	62.5	-	938
100X	125	-	875

### 2. Daily Calibration

- a. Set up the instrument according to Section IV, Instrumental Analysis.
- b. Analyze mobile phase as a blank to verify a stable baseline.
- c. Analyze the medium calibration standard (10X) to verify peak separation and retention times.
- d. Analyze the calibration standards prepared in Section IV-A-1.

### 3. Analysis of Calibration Data

- a. Tabulate the calibration standard concentration versus the peak height response for each calibration standard.
- b. Perform a linear regression analysis on the calibration data plotting peak height vs. concentration in ug/mL.
- c. Use the liner regression to obtain analyte concentration for sample response.

### 4. Calibration Checks

- a. After completion of analyses of samples, a calibration standard at the 10X concentration is analyzed. The response must agree within 25 percent with the daily calibration 10X standard.

- b. No certified calibration check standards are available for these compounds.

V. SAMPLE HANDLING STORAGE FOR SOIL, WIPE, AND RINSATE SAMPLES

- A. Sampling Procedure: The stability of explosives in soil is not truly known. Precautions should be taken to avoid prolonged exposure to light and heat.
- B. Containers: Wide-mouth amber glass bottles with teflon-lined lids.
- C. Storage Conditions: Samples should be maintained at 4°C from the time of collection to the time of analysis. No chemical preservatives are necessary.
- D. Holding Time Limits: 7 days to extraction; 40 days to analysis from the time of extraction.
- E. Solution Verification: No certified check standards are available.

VI PROCEDURE

A. Soil Analysis

1. Method

- a. Accurately weigh 1 gm of soil into a 5-mL serum vial and pipet 2 mL of acetonitrile onto the soil.
- b. Place a septum and cap on the vial and shake the vial thoroughly by hand for 2 to 3 minutes.
- c. The extract is then filtered using the following technique. A 5-mL syringe is fitted with a needle. After the extract is drawn into the syringe barrel, a fluoro-carbon 0.2 micron disposable filter is attached in place of the needle. The sample is then slowly forced through the filter into a 4-mL teflon-capped vial and stored until the extract is diluted and analyzed by HPLC.
- d. Preparation of sample extracts and spikes for injection is performed the day of analysis.

- i. Using a disposable micropipette, accurately measure 200 uL of filtered extract into a 1-mL vial. Accurately measure 600 uL of a 33 percent methanol/67 percent water solution onto the filtered sample. This will produce 800 uL of extracted sample in mobile phase.
- ii. Place a septum cap on the vial. Shake the vial well to thoroughly mix. Store in the dark at 4°C until ready to analyze.

## 2. Daily Quality Control

- a. Perform a spike at 10X the detection limit daily as follows.
  - i. Accurately weight approximately 1 gm of USATHAMA standard soil into a 5-mL serum vial.
  - ii. Spike with 100 uL Standard A.
  - iii. Proceed as in VI-A-1, above.

## 3. Instrumental Analysis

- a. Proceed to Section VII, Instrumental Analysis. The working range for soil samples is listed below.

### Calibration Range for Soil Analysis (1X - 100X)

HMX	1.27 - 127	ug
RDX	0.98 - 98.0	ug
NB	0.42 - 42.0	ug
1,3-DNB	0.59 - 59.0	ug
1,3,5-TNB	2.09 - 209	ug
2,4-DNT	0.42 - 42.0	ug
2,6-DNT	0.40 - 40.0	ug
2,4,6-TNT	1.92 - 192	ug
Tetryl	5.00 - 500	ug

- b. Samples with analyte concentration exceeding the calibration range will require dilution as necessary.

## B. Wipe Analysis

### 1. Method

- a. Add the filter to a 40-mL vial and pipet 20 mL acetonitrile into the vial.
- b. Place a cap on the vial and shake the vial thoroughly by hand for 2 to 3 minutes.
- c. The extract is then filtered using the following technique. A 5-mL syringe is fitted with a needle. After the extract is drawn into the syringe barrel, a fluoro carbon 0.2 micron disposable filter is attached in place of the needle. The sample is then slowly forced through the filter into a 4-mL teflon-capped vial and stored until the extract is diluted and analyzed by HPLC. The remaining extract is disposed as waste.
- d. Preparation of sample extracts and spikes for injection is performed the day of analysis.
  - i. Using a disposable micropipette, accurately measure 200 uL of filtered extract into a 1-mL vial. Accurately measure 600 uL of a 33 percent methanol/67 percent water solution onto the filtered sample. This will produce 800 uL of extracted sample in mobile phase.
  - ii. Place a septum cap on the vial. Shake the vial well to thoroughly mix. Store in the dark at 4°C until ready to analyze.

### 2. Daily Quality Control

- a. Perform a spike at 10X the detection limit daily as follows.
  - i. Place 1/10 of a filter paper into a 5-mL serum vial.
  - ii. Add 2 mL acetonitrile.
  - iii. Spike with 100 uL Standard A.
  - iv. Proceed as in VI-B-1-b, above.

### 3. Instrumental Analysis

- a. Proceed to Section VII, Instrumental Analysis. The working range for wipe samples is listed below.

#### Calibration Range for Wipe Samples

HMX	12.7 - 1270	total ug/wipe
RDX	9.8 - 980	total ug/wipe
NB	4.2 - 420	total ug/wipe
1,3-DNB	5.9 - 590	total ug/wipe
1,3,5-TNB	20.9 - 2090	total ug/wipe
2,4-DNT	4.2 - 420	total ug/wipe
2,6-DNT	4.0 - 400	total ug/wipe
2,4,6-TNT	19.2 - 1920	total ug/wipe
Tetryl	50.0 - 5000	total ug/wipe

- b. Samples with analyte concentration exceeding the calibration range will require dilution as necessary.

### C. Rinsate Analysis

#### 1. Method

- a. Acetonitrile rinsate is collected from equipment.
- b. Measure volume of rinsate.
- c. The rinsate is then filtered using the following technique. A 5-mL syringe is fitted with a needle. After the extract is drawn into the syringe barrel, a fluoro-carbon 0.2 micron disposable filter is attached in place of the needle. The sample is then slowly forced through the filter into a 4-mL teflon-capped vial and stored until the extract is diluted and analyzed by HPLC. The remaining rinsate is disposed as waste.
- d. Preparation of sample extracts for injection is performed the day of analysis.
  - i. Using a disposable micropipette, accurately measure 200 uL of filtered extract into a 1-mL vial. Accurately measure 600 uL of a 33 percent methanol/67 percent water solution onto the filtered sample. This will produce 800 uL of extracted sample in mobile phase.

- ii. Place a septum cap on the vial. Shake the vial well to thoroughly mix. Store in the dark at 4°C until ready to analyze.

2. Daily Quality Control

- a. Perform a spike at 10X the detection limit daily as follows:
  - i. Add 2 mL acetonitrile to a 5-mL serum bottle.
  - ii. Spike with 100 uL of Standard A.
  - iii. Proceed as in VI-C-1-c.

3. Instrumental Analysis

- a. Proceed to Section VII, Instrumental Analysis. The working range for rinsate samples is described below.

Calibration Range for Rinsate Samples

HMX	0.635 - 63.5	total mg/sample
RDX	0.49 - 49.0	total mg/sample
NB	0.21 - 21.0	total mg/sample
1,3-DNB	0.295 - 29.5	total mg/sample
1,3,5-TNB	1.05 - 105	total mg/sample
2,4-DNT	0.21 - 21.0	total mg/sample
2,6-DNT	0.20 - 20.0	total mg/sample
2,4,6-TNT	0.96 - 96.0	total mg/sample
Tetryl	2.50 - 250	total mg/sample

- b. Samples with analyte concentration exceeding the calibration range will require dilution as necessary.

VII. INSTRUMENTAL ANALYSIS

- A. Set the chromatographic conditions as follows:

	Time (minutes)	Flow (mL/min.)	Acetonitrile (percent)	Methanol (percent)	Water (Percent)
Equilibrium	3	1.6	16	34	50
Analysis Run	15	1.6	16	34	50

- B. Using the auto-injector manufacturer's recommended procedure, introduce 50 uL of the medium level calibration standard into the chromatographic system.

Check the chromatogram to ensure separation of the nitrated toluenes and separation of the nitrobenzene and tetryl. If necessary, adjust the water/methanol ratio of the mobile phase until separate peaks are distinguished. As the column ages, less methanol is required. Generally, the column ages rapidly the first 24 hours, after which it is fairly stable.

- C. Once good peak separation is obtained, introduce 50 uL of each working calibration standard and sample into the chromatographic system using the auto-injector manufacturer's recommended procedure.

#### VIII. CALCULATIONS

##### A. Soil Samples

1. The diluted extract concentration is read or calculated from the instrument calibration curve.

$$2. \text{ Sample concentration (ug/g)} = \frac{B \times D}{A \times C}$$

$$\frac{\text{extract conc (ug/mL)} \times 4 \times B}{A}$$

where:

A = sample weight (dry weight)  
B = mL acetonitrile

##### B. Wipe Samples

$$\text{Sample Concentration (total ug)} = \text{extract conc (ug/mL)} \times 20 \text{ mL} \times 4$$

where:

20 mL = total volume  
4 = dilution in method

##### C. Rinse

$$\text{Sample concentration (total ug)} = \text{extract conc (ug/mL)} \times V \times 4$$

where:

V = total volume  
4 = dilution in method

July 1990  
Revision: Final

**MODIFIED METHOD FOR NITROCELLULOSE,  
NITROGLYCERIN, AND PETN IN WATER**



MODIFIED METHOD OF NITROCELLULOSE, NITROGLYCERIN, AND PETN IN WATER

1. APPLICATION

This method is used to qualitatively determine the concentration of nitrocellulose (NC), nitroglycerine (NG), and PETN in water samples.

- A. Tested Concentration Range - Response is linear from 5 to 100 mg/liter in water.
- B. Sensitivity Limits - Response for 5 ug of compound is: NC = 0.89, NG = 0.17, PETN = 0.15 absorbance units.
- C. Detection Limits -

<u>Compound</u>	<u>Water (ug/L)</u>
NC	9000
NG	5000
PETN	5000

- D. Interferences - Nitrite ion will interfere, NC, NG, and PETN cannot be distinguished from each other.
- E. Analysis Rate - Approximately 20 samples can be analyzed by one worker in an eight hour day.

2. CHEMISTRY:

Nitrite ion is cleaved from the nitrate ester in basic solution, which diazotizes procaine, in acidic solution, which in turn couples with N, N-dimethyl-1-naphthylamine to produce an azo-dye. This dye is determined from its absorbance at 510 um.

$C_3N_3O_9$  - Trinitroglycerine; glyceryl trinitrate;  
CAS RN-55-63-0 mp - 13°C, decomposition pt = 145°C;

$C_5N_8O_{12}$  - Pentaerythritol tetranitrate CAS  
RN-78-11-5 mp - 140°C; explosive decomposition pt.  
210°C;

$(C_6N_{12}O_{16})_x$  - nitrocellulose, soluble gun cotton,  
CAS RN-9004-70-0 mp - decomposes on heating.

Handling Hazards: Explosives hazard, avoid heat, shock or open flame. Toxic inhalation and skin absorption hazards exist. Do not handle NG except as a dilute solution.

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### 3. APPARATUS:

A. Instrumentation - Absorbance measurements are made at 510 nm on a Perkin Elmer Lambda 3 UV/UVS spectrometer equipped with a super sipper.

B. Parameters - N/A

#### C. Hardware/Glassware

- 1) 0.1-, 1-, and 2-mL
- 2) 13 x 100 mm glass test tubes
- 3) 10-mL volumetric flasks
- 4) 100-mL volumetric flasks
- 5) 1-cm spectrometer cell (glass)
- 6) water bath
- 7) hot plate
- 8) 25-uL graduated syringe
- 9) 8-ounce glass bottle
- 10) 2 dram glass vials

#### D. Chemicals

- 1) KOH, Analytical reagent grade
- 2) Glacial acetic acid, ACS grade
- 3) Acetone, ACS grade
- 4) N,N-dimethyl-1-naphthylamine
- 5) Procaine

#### E. Reagents

- 1) 10 percent KOH: Weigh 10.0 g of reagent grade potassium hydroxide into a 100-mL volumetric flask and dilute slowly with deionized water (nitrite free).
- 2) 20 percent KOH: Same as above except use 20.0 g of KOH.
- 3) 10 percent acetic acid: Pipette 10.0 mL of glacial acetic acid into a 100-mL volumetric flask that is partially filled with deionized water (nitrite free). Dilute to volume with deionized water.
- 4) 50 percent acetic acid: Same as above except use 50 mL of glacial acetic acid.
- 5) Color Developing Reagent: Weigh 0.35 g each of procaine and N,N-dimethyl-1-naphthylamine into a 100-mL volumetric flask and dilute to volume with 50 percent acetic acid-water.

- 6) Working Solution of Color Reagent: Pipette 20 mL of the color developing reagent into a 100-mL volumetric flask. Dilute to volume with deionized water (nitrite free).

#### 4. STANDARDS

##### A. Calibration Standards

- 1) Stock - Weigh 10.0 mg of NC, PETN, or 1 mL of a 1 percent NC in acetone SARM into a 10.0-mL volumetric flask and dilute to volume with acetone to obtain a 1 ug/uL solution. This solution is refrigerated when not in use.
- 2) Working - Prepare standard curve daily by adding 0.0, 2.5, 5, 10, 25, and 50 uL of 1 ug/uL stock solution, in duplicate, into 13 mm by 100 mm test tubes, using a 25-uL syringe. Add 0.5 mL of deionized water to each tube and mix thoroughly. This yields concentrations of 0, 5, 10, 20, 50, and 100 ug/mL.

- B. Control Spikes - For water samples spike as indicated for the working standards.

#### 5. PROCEDURE:

- A. Water Sample Handling/Preparation - Refrigerate the samples until ready for analysis. Prior to analysis, filter through a 0.45 micron Millipore filter and store refrigerated in a 2 dram glass vial.

##### B. Analysis of Samples

- 1a) Water - Pipette 0.50 mL of water into a 13 x 100 mm test tube and add 0.50 mL of 20 percent potassium hydroxide solution.
- b) Soil - 5 g of air-dried soil is shaken with 5 mL of acetone. The acetone is separated by filtration through a 0.45 u membrane filter (teflon). A 0.5-mL portion of the acetone solution is mixed with 0.5 mL of water and 0.5 mL of 20 percent potassium hydroxide solution.
- 2) Mix sample well and place in boiling water bath for 30 minutes.
- 3) Cool the sample; add 2.0 mL of 10 percent acetic acid, and mix.
- 4) Add 1.0 mL of color developing reagent working solution and mix well.

5) Allow color to develop for 1.5 hours; transfer the solution to a clean, dry spectrophotometer cell and read the absorbance at 510 nm.

6. CALCULATIONS:

Construct a calibration curve of absorbance vs. concentration (ug/L) of the compound of interest (differing response will be observed for NC, FETN, and NG). Determine concentration of compound in samples by interpolating from the calibration curve.

7. REFERENCE:

None.

July 1990  
Revision: Final

**AMMONIUM PICRATE IN WATER AND WIPE SAMPLES BY  
HIGH PERFORMANCE LIQUID CHROMATOGRAPHY**

AMMONIUM PICRATE IN WATER AND WIPE SAMPLES  
BY HIGH PERFORMANCE LIQUID CHROMATOGRAPHY

1. Application

This method is suitable for the determination of ammonium picrate in water and wipe samples. Ammonium picrate is converted to picric acid and quantified in that form.

2. Summary of method

Ammonium picrate is extracted from water or wipe samples with solvent. The extract is concentrated and subjected to high performance liquid chromatography (HPLC) analysis using a reverse phase column and a dual channel ultraviolet detector.

3. Interferences

Any compounds that exhibit chemical and/or physical properties similar to the compounds of interest can interfere.

4. Apparatus

4.1 Concentrator apparatus, a Kuderna-Danish (K-D) concentrator, 500-mL capacity with a 3-ball Snyder column and a 10-mL graduated receiver tube and a 500-mL flask fitted with a 1-ball Snyder column.

4.2 Erlenmeyer flask, 500-mL with a ground glass stopper.

4.3 Evaporative concentrator, Organomation N-Evap, or equivalent.

4.4 Liquid chromatograph, Waters Associates ALC/GPC 204 liquid chromatograph equipped with a dual channel, variable wavelength detector, a model 6000A solvent-delivery system, a model 660 solvent flow programmer, model WISP 710A microprocessor and data module, or equivalents.

4.5 Liquid chromatographic column, a 3.9 mm i.d. by 300 mm long stainless steel column packed with 10  $\mu$ m particle size reverse phase material. Waters Associates  $\mu$ -Bonapak C<sub>18</sub> column packing or equivalent.

4.6 Separatory funnels, Squibb form, 1-L capacity, or equivalent.

4.7 Solvent clarification kit, Waters Associates 85113, or equivalent.  
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4.8 Shaker, a mechanical wrist action shaker.

4.9 Steam bath, a constant temperature steam bath set at 85°C.

## 5. Reagents

5.1 Acetonitrile, HPLC quality.

5.2 Hydrochloric acid, ACS reagent grade.

5.3 Mobile phase solutions: Prepare the ion pairing, tetrabutylammonium-phosphate solutions for the mobile phase using Waters Associates PIC Reagent A, or equivalent.

5.3.1 Solution A: Add one bottle of PIC reagent A to 1,000 mL of Milli-Q water. Stir for 5 min and then filter through a 0.45-micron filter, type HAWP for aqueous solvents.

5.3.2 Solution B: Add one bottle of PIC reagent A to 1,000 mL acetonitrile. Stir for 5 min and then filter through a 0.45-micron filter type FHUP for organic solvents.

5.4 Picric acid standards, analytical reference grade or highest purity available. These may be obtained from chemical specialty suppliers or from military sources. Prepare standards at concentrations sufficient to cover the analytical range.

5.5 Separatory funnels, Squibb form, 1-L capacity, or equivalent.

5.6 Solvents, acetone, diethylether, methylene chloride, acetonitrile, pesticide residue quality, distilled in glass, Burdick and Jackson, or equivalent.

5.7 Water, organic-free, HPLC-grade, or water from a Millipore Milli-Q system or equivalent.

## 6. Procedure

6.1 Procedure for water (rinstate) samples: Samples should be collected according to the recommended practice for the collection of samples for organic analysis (Goerlitz and Brown, 1972). Mercuric chloride (40 ppm) is added as a preservative.

6.1.1 Pour 500 mL water into a 1-L separatory funnel.

6.1.2 Add 3 mL concentrated HCl to the sample contained in the separatory funnel. Check pH to ensure acidity.

6.1.3 Add 75 mL methylene chloride to the sample in the separatory funnel. Stopper and shake for 1 minute. Vent the pressure often. Allow the layers to separate and draw off the methylene chloride layer into a 250-mL Erlenmeyer flask.

6.1.4 Repeat the extraction of the water sample two more times, using 50-mL methylene chloride volumes each time. Combine all the organic extracts in the 250-mL Erlenmeyer, which contains the first extract.

6.1.5 Quantitatively transfer the extract to a 500-mL K-D apparatus fitted with a 3-ball Snyder column and a 20-mL receiver. Add a micro boiling chip and 4 mL of acetonitrile.

6.1.6 Place the apparatus on a hot-water bath (approximately 85°C). Reduce the volume of the extract to about 4 mL. Remove the K-D from the heat and allow it to cool.

6.1.7 Use the evaporative concentrator to reduce the volume of solvent to 0.8 to 0.9 mL by directing a stream of nitrogen onto the surface of the liquid while gently warming the receiver in a water bath.

6.1.8 Perform one method blank and three sample spikes at 40 ppb, 200 ppb, and 200 ppb with each batch of 20 samples.

6.1.9 Proceed to HPLC analysis (6.3).

## 6.2 Procedure for wipe samples

6.2.1 Add wipe sample to 40-mL vial.

6.2.2 Add 20 mL distilled water.

6.2.3 Shake 15 minutes using wrist-action shaker.

6.2.4 Decant water into 500-mL separatory funnel.

6.2.5 Repeat extraction twice, using 20 mL distilled water each time.

6.2.6 Add 440 mL distilled water to separator funnel.

6.2.7 Perform one method blank and three sample spikes of 20 ug, 100 ug, and 100 ug with each batch.

6.2.8 Proceed as in 6.1.2 under "Procedure for Water (Rinsate) Samples."

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### 6.3 Analysis by high pressure liquid chromatography.

6.3.1 The following chromatographic conditions have been found to be suitable for this analysis:

Mobile Phase: The separation is made under isocratic conditions. Combine 36 percent solution A with 64 percent solution B by using the solvent programmer.

Isocratic 36 percent acetonitrile + PIC reagent A + PICA/64 percent H<sub>2</sub>O + PIC reagent A.

Flow Rate: 1.10 mL/min

Detector Sensitivity:

UV 254 nm 0.005 A units full scale

6.3.3 Daily calibration is performed over the following range of concentrations using picric acid as the standard material.

Standard Concentration (ng/uL)	Corresponding Ammonium Picrate in Water (ug/L)	Corresponding Ammonium Picrate in Wipe (total ug)
10	20	10
20	40	20
50	100	50
100	200	100
200	400	200
500	1000	500
1000	2000	1000

6.3.4 Add 0.1 mL of PIC reagent A to the samples, mix and make up to a volume of 1.0 mL; allow samples to stand 10 minutes and inject 10 uL into the liquid chromatographic system. Record the volume injected. Identify the peaks by retention time. Dilute any extract containing an identifiable component above the calibration range to bring it within that range.

## 7. Calculations

7.1 Determine sample concentration from daily calibration curve using Least Squares Fit (LSF).  
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7.2 Water sample concentration is calculated as follows:

$$\frac{\text{ng/uL} \times \text{EV} \times 1 \text{ ug}}{1000 \text{ ng}} + \text{SV} = \text{ug/L}$$

where:

ng/uL = picric acid concentration in extract, from LSF.

EV = extract volume, in uL.

SV = sample volume, in Liters.

Note that picric acid concentration must be converted to ammonium picrate concentration by using the ratios of molecular weights.

7.3 Wipe sample concentration (total ug) is calculated as follows:

$$\frac{\text{ng/uL} \times \text{EV} \times 1 \text{ ug}}{1000 \text{ ng}} = \text{total ug}$$

where:

ng/uL = picric acid concentration in extract, from LSF.

EV = extract volume.

Note that picric acid concentration must be converted to ammonium picrate concentration by using the ratios of molecular weights.

### References

Goerlitz, D.F. and Law, L.M., Gas chromatographic method for the analysis of TNT and RDX explosives contaminating water and soil-core material, U.S. Geological Survey open file report 75-182.

Goerlitz, D.F., 1978, Direct analysis of RDX and TNT in water by high-pressure liquid chromatography, U.S. Geological Survey open file report 79--.

Goerlitz, D.F., 1978, High-performance liquid chromatography method for the analysis of picric acid in water, U.S. Geological Survey open file report.

July 1990  
Revision: Final

**EPA MODIFIED METHOD 5**  
**MODIFIED METHOD 5 SAMPLING TRAIN**

## METHOD 0010

### MODIFIED METHOD 5 SAMPLING TRAIN

#### 1.0 SCOPE AND APPLICATION

1.1 This method is applicable to the determination of Destruction and Removal Efficiency (DRE) of semivolatile Principal Organic Hazardous Compounds (POHCs) from incineration systems (PHS, 1967). This method also may be used to determine particulate emission rates from stationary sources as per EPA Method 5 (see References at end of this method).

#### 2.0 SUMMARY OF METHOD

2.1 Gaseous and particulate pollutants are withdrawn from an emission source at an isokinetic sampling rate and are collected in a multicomponent sampling train. Principal components of the train include a high-efficiency glass- or quartz-fiber filter and a packed bed of porous polymeric adsorbent resin. The filter is used to collect organic-laden particulate materials and the porous polymeric resin to adsorb semivolatile organic species. Semivolatile species are defined as compounds with boiling points  $>100^{\circ}\text{C}$ .

2.2 Comprehensive chemical analyses of the collected sample are conducted to determine the concentration and identity of the organic materials.

#### 3.0 INTERFERENCES

3.1 Oxides of nitrogen ( $\text{NO}_x$ ) are possible interferents in the determination of certain water-soluble compounds such as dioxane, phenol, and urethane; reaction of these compounds with  $\text{NO}_x$  in the presence of moisture will reduce their concentration. Other possibilities that could result in positive or negative bias are (1) stability of the compounds in methylene chloride, (2) the formation of water-soluble organic salts on the resin in the presence of moisture, and (3) the solvent extraction efficiency of water-soluble compounds from aqueous media. Use of two or more ions per compound for qualitative and quantitative analysis can overcome interference at one mass. These concerns should be addressed on a compound-by-compound basis before using this method.

#### 4.0 APPARATUS AND MATERIALS

##### 4.1 Sampling train:

4.1.1 A schematic of the sampling train used in this method is shown in Figure 1. This sampling train configuration is adapted from EPA Method 5 procedures, and, as such, the majority of the required equipment

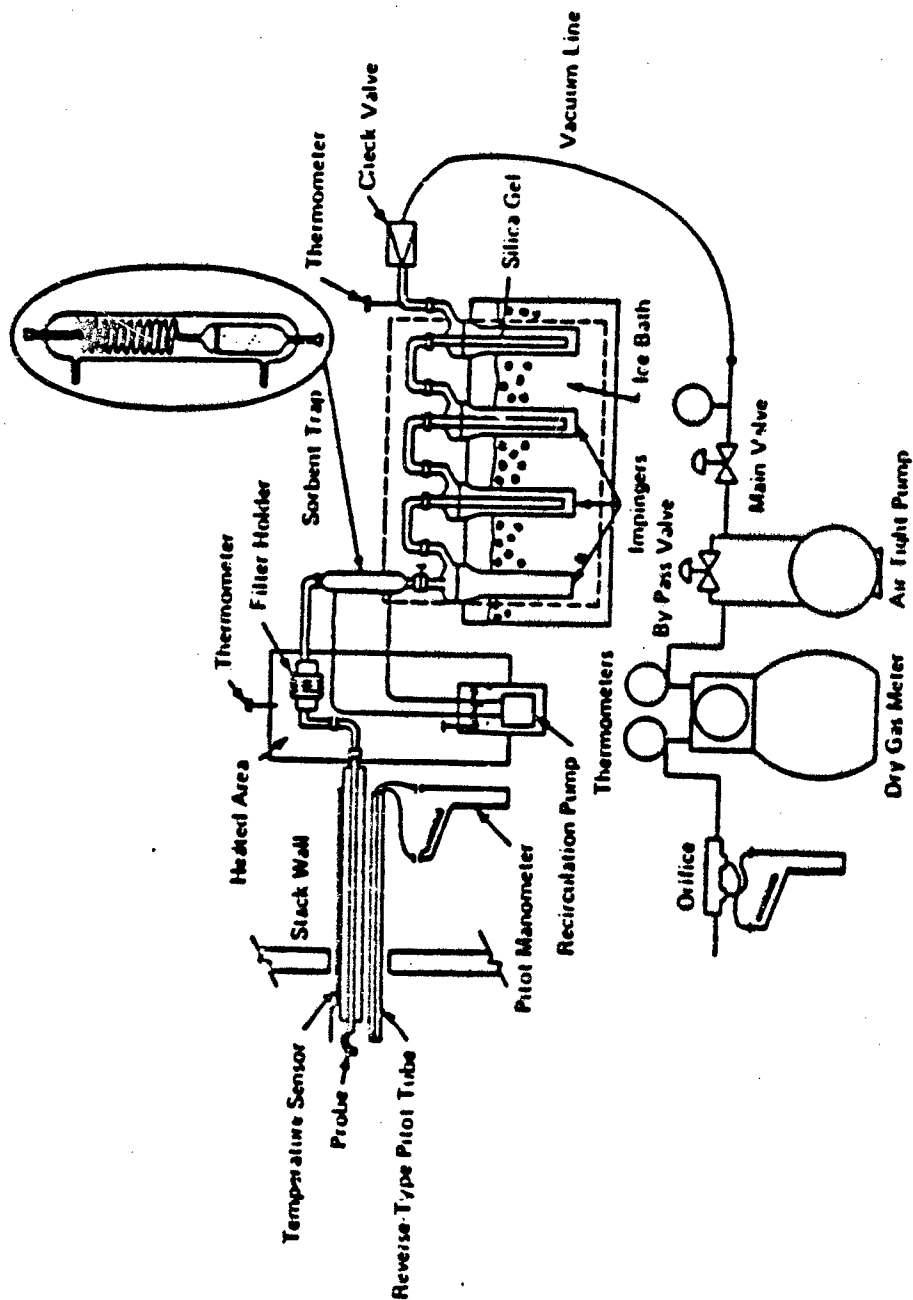


Figure 1. Modified Method 5 Sampling Train.

complete organic module are not currently available, but may be assembled from commercially available laboratory glassware and a custom-fabricated sorbent trap. Details of two acceptable designs are shown in Figures 2 and 3 (the thermocouple well is shown in Figure 2).

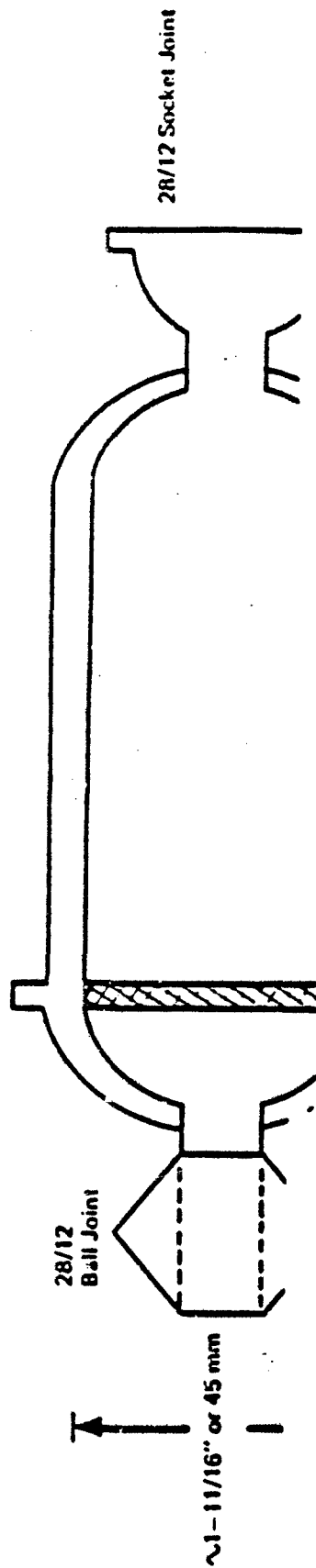
**4.1.3.8 Impinger train:** To determine the stack-gas moisture content, four 500-mL impingers, connected in series with leak-free ground-glass joints, follow the knockout trap. The first, third, and fourth impingers shall be of the Greenburg-Smith design, modified by replacing the tip with a 1.3-cm (1/2-in.) I.D. glass tube extending about 1.3 cm (1/2 in.) from the bottom of the outer cylinder. The second impinger shall be of the Greenburg-Smith design with the standard tip. The first and second impingers shall contain known quantities of water or appropriate trapping solution. The third shall be empty or charged with a caustic solution, should the stack gas contain hydrochloric acid (HCl). The fourth shall contain a known weight of silica gel or equivalent desiccant.

**4.1.3.9 Metering system:** The necessary components are a vacuum gauge, leak-free pump, thermometers capable of measuring temperature to within 3°C (5.4°F), dry-gas meter capable of measuring volume to within 1%, and related equipment, as shown in Figure 1. At a minimum, the pump should be capable of 4 cfm free flow, and the dry-gas meter should have a recording capacity of 0-999.9 cu ft with a resolution of 0.005 cu ft. Other metering systems capable of maintaining sampling rates within 10% of isokineticity and of determining sample volumes to within 2% may be used. The metering system must be used in conjunction with a pitot tube to enable checks of isokinetic sampling rates. Sampling trains using metering systems designed for flow rates higher than those described in APTD-0581 and APTD-0576 may be used, provided that the specifications of this method are met.

**4.1.3.10 Barometer:** Mercury, aneroid, or other barometer capable of measuring atmospheric pressure to within 2.5 mm Hg (0.1 in. Hg). In many cases the barometric reading may be obtained from a nearby National Weather Service station, in which case the station value (which is the absolute barometric pressure) is requested and an adjustment for elevation differences between the weather station and sampling point is applied at a rate of minus 2.5 mm Hg (0.1 in. Hg) per 30-m (100 ft) elevation increase (vice versa for elevation decrease).

**4.1.3.11 Gas density determination equipment:** Temperature sensor and pressure gauge (as described in Sections 2.3 and 2.4 of EPA Method 2), and gas analyzer, if necessary (as described in EPA Method 3). The temperature sensor ideally should be permanently attached to the pitot tube or sampling probe in a fixed configuration such that the tip of the sensor extends beyond the leading edge of the probe sheath and does not touch any metal.

~6.5 in.  
or  
168 mm





is identical to that used in EPA Method 5 determinations. The new components required are a condenser coil, and a sorbent module, which are used to collect semivolatile organic materials that pass through the glass- or quartz-fiber filter in the gas phase.

4.1.2 Construction details for the basic train components are given in APTD-0581 (see Martin, 1971, in Section 13.0, References); commercial models of this equipment are also available. Specifications for the sorbent module are provided in the following subsections. Additionally, the following subsections list changes to APTD-0581 and identify allowable train configuration modifications.

4.1.3 Basic operating and maintenance procedures for the sampling train are described in APTD-0576 (see Rom, 1972, in Section 13.0, References). As correct usage is important in obtaining valid results, all users should refer to APTD-0576 and adopt the operating and maintenance procedures outlined therein unless otherwise specified. The sampling train consists of the components detailed below.

4.1.3.1 Probe nozzle: Stainless steel (316) or glass with sharp, tapered (30° angle) leading edge. The taper shall be on the outside to preserve a constant I.D. The nozzle shall be buttonhook or elbow design and constructed from seamless tubing (if made of stainless steel). Other construction materials may be considered for particular applications. A range of nozzle sizes suitable for isokinetic sampling should be available in increments of 0.16 cm (1/16 in.), e.g., 0.32-1.27 cm (1/8-1/2 in.), or larger if higher volume sampling trains are used. Each nozzle shall be calibrated according to the procedures outlined in Paragraph 9.1.

4.1.3.2 Probe liner: Borosilicate or quartz-glass tubing with a heating system capable of maintaining a gas temperature of  $120 \pm 14^{\circ}\text{C}$  ( $248 \pm 25^{\circ}\text{F}$ ) at the exit end during sampling. (The tester may opt to operate the equipment at a temperature lower than that specified.) Because the actual temperature at the outlet of the probe is not usually monitored during sampling, probes constructed according to APTD-0581 and utilizing the calibration curves of APTD-0576 (or calibrated according to the procedure outlined in APTD-0576) are considered acceptable. Either borosilicate or quartz-glass probe liners may be used for stack temperatures up to about  $480^{\circ}\text{C}$  ( $900^{\circ}\text{F}$ ). Quartz liners shall be used for temperatures between 480 and  $900^{\circ}\text{C}$  (900 and  $1650^{\circ}\text{F}$ ). (The softening temperature for borosilicate is  $820^{\circ}\text{C}$  ( $1508^{\circ}\text{F}$ ), and for quartz  $1500^{\circ}\text{C}$  ( $2732^{\circ}\text{F}$ ).) Water-cooling of the stainless steel sheath will be necessary at temperatures approaching and exceeding  $500^{\circ}\text{C}$ .

4.1.3.3 Pitot tube: Type S, as described in Section 2.1 of EPA Method 2, or other appropriate devices (Vollaro, 1976). The pitot tube shall be attached to the probe to allow constant monitoring of the stack-gas velocity. The impact (high-pressure) opening plane of the pitot tube shall be even with or above the nozzle entry plane (see EPA Method 2, Figure 2-6b) during sampling. The Type S pitot tube assembly shall have a known coefficient, determined as outlined in Section 4 of EPA Method 2.

4.1.3.4 Differential pressure gauge: Inclined manometer or equivalent device as described in Section 2.2 of EPA Method 2. One manometer shall be used for velocity-head ( $\Delta P$ ) readings and the other for orifice differential pressure ( $\Delta H$ ) readings.

4.1.3.5 Filter holder: Borosilicate glass, with a glass frit filter support and a sealing gasket. The sealing gasket should be made of materials that will not introduce organic material into the gas stream at the temperature at which the filter holder will be maintained. The gasket shall be constructed of Teflon or materials of equal or better characteristics. The holder design shall provide a positive seal against leakage at any point along the filter circumference. The holder shall be attached immediately to the outlet of the cyclone or cyclone bypass.

4.1.3.6 Filter heating system: Any heating system capable of maintaining a temperature of  $120 \pm 14^\circ\text{C}$  ( $248 \pm 25^\circ\text{F}$ ) around the filter holder during sampling. Other temperatures may be appropriate for particular applications. Alternatively, the tester may opt to operate the equipment at temperatures other than that specified. A temperature gauge capable of measuring temperature to within  $3^\circ\text{C}$  ( $5.4^\circ\text{F}$ ) shall be installed so that the temperature around the filter holder can be regulated and monitored during sampling. Heating systems other than the one shown in APTD-0581 may be used.

4.1.3.7 Organic sampling module: This unit consists of three sections, including a gas-conditioning section, a sorbent trap, and a condensate knockout trap. The gas-conditioning system shall be capable of conditioning the gas leaving the back half of the filter holder to a temperature not exceeding  $20^\circ\text{C}$  ( $68^\circ\text{F}$ ). The sorbent trap shall be sized to contain approximately 20 g of porous polymeric resin (Rohm and Haas XAD-2 or equivalent) and shall be jacketed to maintain the internal gas temperature at  $17 \pm 3^\circ\text{C}$  ( $62.5 \pm 5.4^\circ\text{F}$ ). The most commonly used coolant is ice water from the impinger ice-water bath, constantly circulated through the outer jacket, using rubber or plastic tubing and a peristaltic pump. The sorbent trap should be outfitted with a glass well or depression, appropriately sized to accommodate a small thermocouple in the trap for monitoring the gas entry temperature. The condensate knockout trap shall be of sufficient size to collect the condensate following gas conditioning. The organic module components shall be oriented to direct the flow of condensate formed vertically downward from the conditioning section, through the adsorbent media, and into the condensate knockout trap. The knockout trap is usually similar in appearance to an empty impinger directly underneath the sorbent module; it may be oversized but should have a shortened center stem (at a minimum, one-half the length of the normal impinger stems) to collect a large volume of condensate without bubbling and overflowing into the impinger train. All surfaces of the organic module wetted by the gas sample shall be fabricated of borosilicate glass, Teflon, or other inert materials. Commercial versions of the

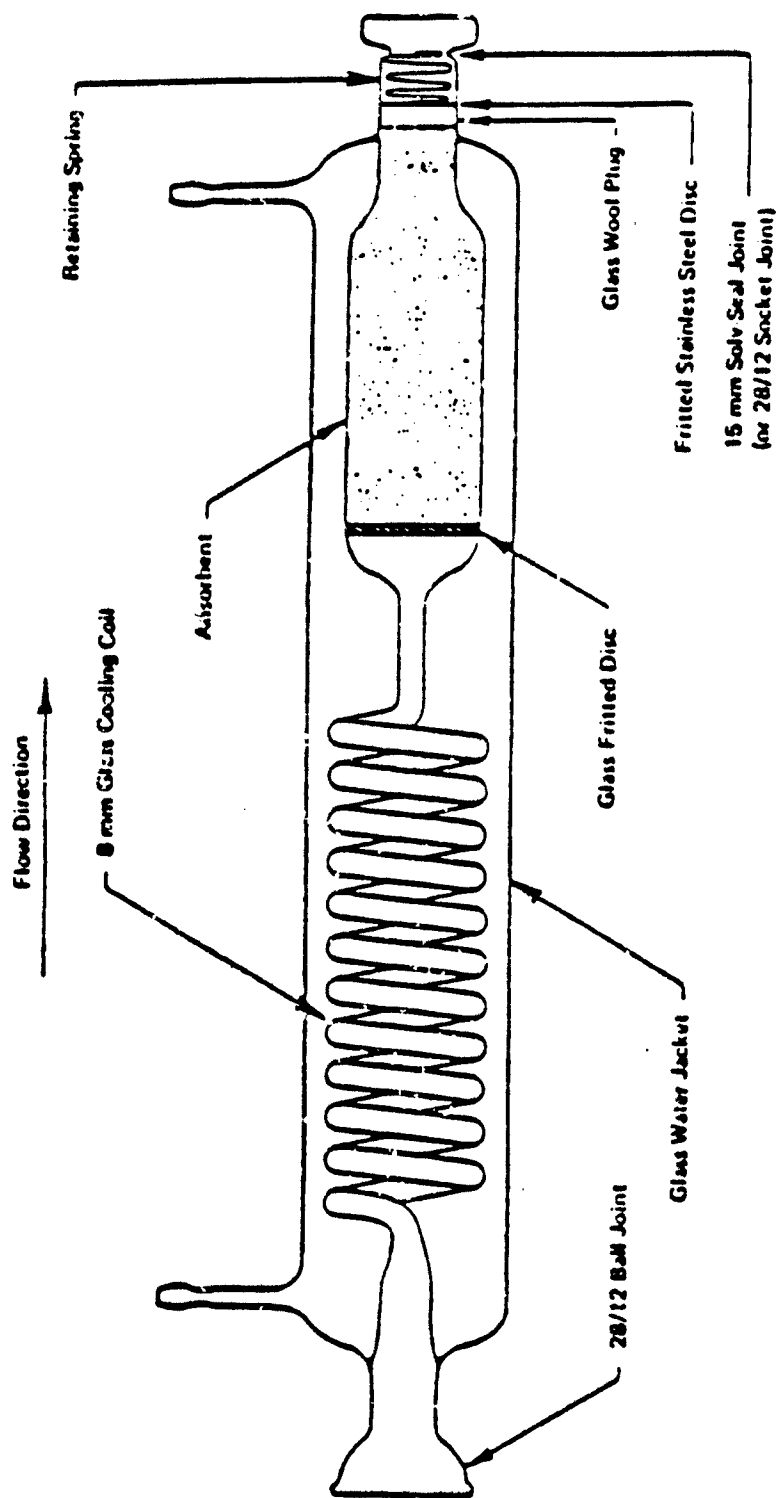


Figure 3. Adsorbent Sampling System.

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Alternatively, the sensor may be attached just prior to use in the field. Note, however, that if the temperature sensor is attached in the field, the sensor must be placed in an interference-free arrangement with respect to the Type S pitot tube openings (see EPA Method 2, Figure 2-7). As a second alternative, if a difference of no more than 1% in the average velocity measurement is to be introduced, the temperature gauge need not be attached to the probe or pitot tube.

4.1.3.12 Calibration/field-preparation record: A permanently bound laboratory notebook, in which duplicate copies of data may be made as they are being recorded, is required for documenting and recording calibrations and preparation procedures (i.e., filter and silica gel tare weights, clean XAD-2, quality assurance/quality control check results, dry-gas meter, and thermocouple calibrations, etc.). The duplicate copies should be detachable and should be stored separately in the test program archives.

#### 4.2 Sample Recovery:

4.2.1 Probe liner: Probe nozzle and organic module conditioning section brushes; nylon bristle brushes with stainless steel wire handles are required. The probe brush shall have extensions of stainless steel, Teflon, or inert material at least as long as the probe. The brushes shall be properly sized and shaped to brush out the probe liner, the probe nozzle, and the organic module conditioning section.

4.2.2 Wash bottles: Three. Teflon or glass wash bottles are recommended; polyethylene wash bottles should not be used because organic contaminants may be extracted by exposure to organic solvents used for sample recovery.

4.2.3 Glass sample storage containers: Chemically resistant, borosilicate amber and clear glass bottles, 500-mL or 1,000-mL. Bottles should be tinted to prevent action of light on sample. Screw-cap liners shall be either Teflon or constructed so as to be leak-free and resistant to chemical attack by organic recovery solvents. Narrow-mouth glass bottles have been found to exhibit less tendency toward leakage.

4.2.4 Petri dishes: Glass, sealed around the circumference with wide (1-in.) Teflon tape, for storage and transport of filter samples.

4.2.5 Graduated cylinder and/or balances: To measure condensed water to the nearest 1 mL or 1 g. Graduated cylinders shall have subdivisions not  $>2$  mL. Laboratory triple-beam balances capable of weighing to  $\pm 0.5$  g or better are required.

4.2.6 Plastic storage containers: Screw-cap polypropylene or polyethylene containers to store silica gel.

4.2.7 Funnel and rubber policeman: To aid in transfer of silica gel to container (not necessary if silica gel is weighed in field).

4.2.8 Funnels: Glass, to aid in sample recovery.

4.3 Filters: Glass- or quartz-fiber filters, without organic binder, exhibiting at least 99.95% efficiency (<0.05% penetration) on 0.3-um dioctyl phthalate smoke particles. The filter efficiency test shall be conducted in accordance with ASTM standard method D2986-71. Test data from the supplier's quality control program are sufficient for this purpose. In sources containing SO<sub>2</sub> or SO<sub>3</sub>, the filter material must be of a type that is unreactive to SO<sub>2</sub> or SO<sub>3</sub>. Reeve Angel 934 AH or Schleicher and Schuell #3 filters work well under these conditions.

4.4 Crushed ice: Quantities ranging from 10-50 lb may be necessary during a sampling run, depending on ambient air temperature.

4.5 Stopcock grease: Solvent-insoluble, heat-stable silicone grease. Use of silicone grease upstream of the module is not permitted, and amounts used on components located downstream of the organic module shall be minimized. Silicone grease usage is not necessary if screw-on connectors and Teflon sleeves or ground-glass joints are used.

4.6 Glass wool: Used to plug the unfitted end of the sorbent module. The glass-wool fiber should be solvent-extracted with methylene chloride in a Soxhlet extractor for 12 hr and air-dried prior to use.

## 5.0 REAGENTS

5.1 Adsorbent resin: Porous polymeric resin (XAD-2 or equivalent) is recommended. These resins shall be cleaned prior to their use for sample collection. Appendix A of this method should be consulted to determine appropriate precleaning procedure. For best results, resin used should not exhibit a blank of higher than 4 mg/kg of total chromatographable organics (TCO) (see Appendix B) prior to use. Once cleaned, resin should be stored in an airtight, wide-mouth amber glass container with a Teflon-lined cap or placed in one of the glass sorbent modules tightly sealed with Teflon film and elastic bands. The resin should be used within 4 wk of the preparation.

5.2 Silica gel: Indicating type, 6-16 mesh. If previously used, dry at 175°C (350°F) for 2 hr before using. New silica gel may be used as received. Alternatively, other types of desiccants (equivalent or better) may be used, subject to the approval of the Administrator.

5.3 Impinger solutions: Distilled organic-free water (Type II) shall be used, unless sampling is intended to quantify a particular inorganic gaseous species. If sampling is intended to quantify the concentration of additional species, the impinger solution of choice shall be subject to Administrator approval. This water should be prescreened for any compounds of interest. One hundred mL will be added to the specified impinger; the third impinger in the train may be charged with a basic solution (1 N sodium hydroxide or sodium acetate) to protect the sampling pump from acidic gases. Sodium acetate should be used when large sample volumes are anticipated because sodium hydroxide will react with carbon dioxide in aqueous media to form sodium carbonate, which may possibly plug the impinger.

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#### 5.4 Sample recovery reagents:

5.4.1 Methylene chloride: Distilled-in-glass grade is required for sample recovery and cleanup (see Note to 5.4.2 below).

5.4.2 Methyl alcohol: Distilled-in-glass grade is required for sample recovery and cleanup.

NOTE: Organic solvents from metal containers may have a high residue blank and should not be used. Sometimes suppliers transfer solvents from metal to glass bottles; thus blanks shall be run prior to field use and only solvents with low blank value ( $<0.001\%$ ) shall be used.

5.4.3 Water: Water (Type II) shall be used for rinsing the organic module and condenser component.

#### 6.0 SAMPLE COLLECTION, PRESERVATION, AND HANDLING

6.1 Because of complexity of this method, field personnel should be trained in and experienced with the test procedures in order to obtain reliable results.

##### 6.2 Laboratory preparation:

6.2.1 All the components shall be maintained and calibrated according to the procedure described in APTD-0576, unless otherwise specified.

6.2.2 Weigh several 200- to 300-g portions of silica gel in airtight containers to the nearest 0.5 g. Record on each container the total weight of the silica gel plus containers. As an alternative to preweighing the silica gel, it may instead be weighed directly in the impinger or sampling holder just prior to train assembly.

6.2.3 Check filters visually against light for irregularities and flaws or pinhole leaks. Label the shipping containers (glass Petri dishes) and keep the filters in these containers at all times except during sampling and weighing.

6.2.4 Desiccate the filters at  $20 \pm 5.6^{\circ}\text{C}$  ( $68 \pm 10^{\circ}\text{F}$ ) and ambient pressure for at least 24 hr, and weigh at intervals of at least 6 hr to a constant weight (i.e.,  $<0.5\text{-mg}$  change from previous weighing), recording results to the nearest 0.1 mg. During each weighing the filter must not be exposed for more than a 2-min period to the laboratory atmosphere and relative humidity above 50%. Alternatively (unless otherwise specified by the Administrator), the filters may be oven-dried at  $105^{\circ}\text{C}$  ( $220^{\circ}\text{F}$ ) for 2-3 hr, desiccated for 2 hr, and weighed.

### 6.3 Preliminary field determinations:

6.3.1 Select the sampling site and the minimum number of sampling points according to EPA Method 1 or as specified by the Administrator. Determine the stack pressure, temperature, and range of velocity heads using EPA Method 2. It is recommended that a leak-check of the pitot lines (see EPA Method 2, Section 3.1) be performed. Determine the stack-gas moisture content using EPA Approximation Method 4 or its alternatives to establish estimates of isokinetic sampling-rate settings. Determine the stack-gas dry molecular weight, as described in EPA Method 2, Section 3.6. If integrated EPA Method 3 sampling is used for molecular weight determination, the integrated bag sample shall be taken simultaneously with, and for the same total length of time as, the sample run.

6.3.2 Select a nozzle size based on the range of velocity heads so that it is not necessary to change the nozzle size in order to maintain isokinetic sampling rates. During the run, do not change the nozzle. Ensure that the proper differential pressure gauge is chosen for the range of velocity heads encountered (see Section 2.2 of EPA Method 2).

6.3.3 Select a suitable probe liner and probe length so that all traverse points can be sampled. For large stacks, to reduce the length of the probe, consider sampling from opposite sides of the stack.

6.3.4 A minimum of 3 dscm (105.9 dscf) of sample volume is required for the determination of the Destruction and Removal Efficiency (DRE) of POHCs from incineration systems. Additional sample volume shall be collected as necessitated by analytical detection limit constraints. To determine the minimum sample volume required, refer to sample calculations in Section 10.0.

6.3.5 Determine the total length of sampling time needed to obtain the identified minimum volume by comparing the anticipated average sampling rate with the volume requirement. Allocate the same time to all traverse points defined by EPA Method 1. To avoid timekeeping errors, the length of time sampled at each traverse point should be an integer or an integer plus one-half min.

6.3.6 In some circumstances (e.g., batch cycles) it may be necessary to sample for shorter times at the traverse points and to obtain smaller gas-sample volumes. In these cases, the Administrator's approval must first be obtained.

### 6.4 Preparation of collection train:

6.4.1 During preparation and assembly of the sampling train, keep all openings where contamination can occur covered with Teflon film or aluminum foil until just prior to assembly or until sampling is about to begin.

6.4.2 Fill the sorbent trap section of the organic module with approximately 20 g of clean adsorbent resin. While filling, ensure that the trap packs uniformly, to eliminate the possibility of channeling. When freshly cleaned, many adsorbent resins carry a static charge, which will cause clinging to trap walls. This may be minimized by filling the trap in the presence of an antistatic device. Commercial antistatic devices include Model-204 and Model-210 manufactured by the 3M Company, St. Paul, Minnesota.

6.4.3 If an impinger train is used to collect moisture, place 100 mL of water in each of the first two impingers, leave the third impinger empty (or charge with caustic solution, as necessary), and transfer approximately 200-300 g of preweighed silica gel from its container to the fourth impinger. More silica gel may be used, but care should be taken to ensure that it is not entrained and carried out from the impinger during sampling. Place the container in a clean place for later use in the sample recovery. Alternatively, the weight of the silica gel plus impinger may be determined to the nearest 0.5 g and recorded.

6.4.4 Using a tweezer or clean disposable surgical gloves, place a labeled (identified) and weighed filter in the filter holder. Be sure that the filter is properly centered and the gasket properly placed to prevent the sample gas stream from circumventing the filter. Check the filter for tears after assembly is completed.

6.4.5 When glass liners are used, install the selected nozzle using a Viton-A O-ring when stack temperatures are  $<260^{\circ}\text{C}$  ( $500^{\circ}\text{F}$ ) and a woven glass-fiber gasket when temperatures are higher. See APTD-0576 (Rom, 1972) for details. Other connecting systems utilizing either 316 stainless steel or Teflon ferrules may be used. When metal liners are used, install the nozzle as above, or by a leak-free direct mechanical connection. Mark the probe with heat-resistant tape or by some other method to denote the proper distance into the stack or duct for each sampling point.

6.4.6 Set up the train as in Figure 1. During assembly, do not use any silicone grease on ground-glass joints that are located upstream of the organic module. A very light coating of silicone grease may be used on all ground-glass joints that are located downstream of the organic module, but it should be limited to the outer portion (see APTD-0576) of the ground-glass joints to minimize silicone-grease contamination. Subject to the approval of the Administrator, a glass cyclone may be used between the probe and the filter holder when the total particulate catch is expected to exceed 100 mg or when water droplets are present in the stack. The organic module condenser must be maintained at a temperature of  $17 \pm 3^{\circ}\text{C}$ . Connect all temperature sensors to an appropriate potentiometer/display unit. Check all temperature sensors at ambient temperature.

6.4.7 Place crushed ice around the impingers and the organic module condensate knockout.



6.4.8 Turn on the sorbent module and condenser coil coolant recirculating pump and begin monitoring the sorbent module gas entry temperature. Ensure proper sorbent module gas entry temperature before proceeding and again before any sampling is initiated. It is extremely important that the XAD-2 resin temperature never exceed 50°C (122°F), because thermal decomposition will occur. During testing, the XAD-2 temperature must not exceed 20°C (68°F) for efficient capture of the semivolatile species of interest.

6.4.9 Turn on and set the filter and probe heating systems at the desired operating temperatures. Allow time for the temperatures to stabilize.

## 6.5 Leak-check procedures

### 6.5.1 Pre-test leak-check:

6.5.1.1 Because the number of additional intercomponent connections in the Semi-VOST train (over the M5 Train) increases the possibility of leakage, a pre-test leak-check is required.

6.5.1.2 After the sampling train has been assembled, turn on and set the filter and probe heating systems at the desired operating temperatures. Allow time for the temperatures to stabilize. If a Viton A O-ring or other leak-free connection is used in assembling the probe nozzle to the probe liner, leak-check the train at the sampling site by plugging the nozzle and pulling a 381-mm Hg (15-in. Hg) vacuum.

(NOTE: A lower vacuum may be used, provided that it is not exceeded during the test.)

6.5.1.3 If an asbestos string is used, do not connect the probe to the train during the leak-check. Instead, leak-check the train by first attaching a carbon-filled leak-check impinger (shown in Figure 4) to the inlet of the filter holder (cyclone, if applicable) and then plugging the inlet and pulling a 381-mm Hg (15-in. Hg) vacuum. (Again, a lower vacuum may be used, provided that it is not exceeded during the test.) Then, connect the probe to the train and leak-check at about 25-mm Hg (1-in. Hg) vacuum; alternatively, leak-check the probe with the rest of the sampling train in one step at 381-mm Hg (15-in. Hg) vacuum. Leakage rates in excess of 4% of the average sampling rate or  $>0.00057 \text{ m}^3/\text{min}$  (0.02 cfm), whichever is less, are unacceptable.

6.5.1.4 The following leak-check instructions for the sampling train described in APTD-0576 and APTD-0581 may be helpful. Start the pump with fine-adjust valve fully open and coarse-adjust valve completely closed. Partially open the coarse-adjust valve and slowly close the fine-adjust valve until the desired vacuum is reached. Do not reverse direction of the fine-adjust valve; this will cause water to back up into the organic module. If the desired vacuum is exceeded, either leak-check at this higher vacuum or end the leak-check, as shown below, and start over.

CROSS SECTIONAL VIEW  
Leak Testing Apparatus

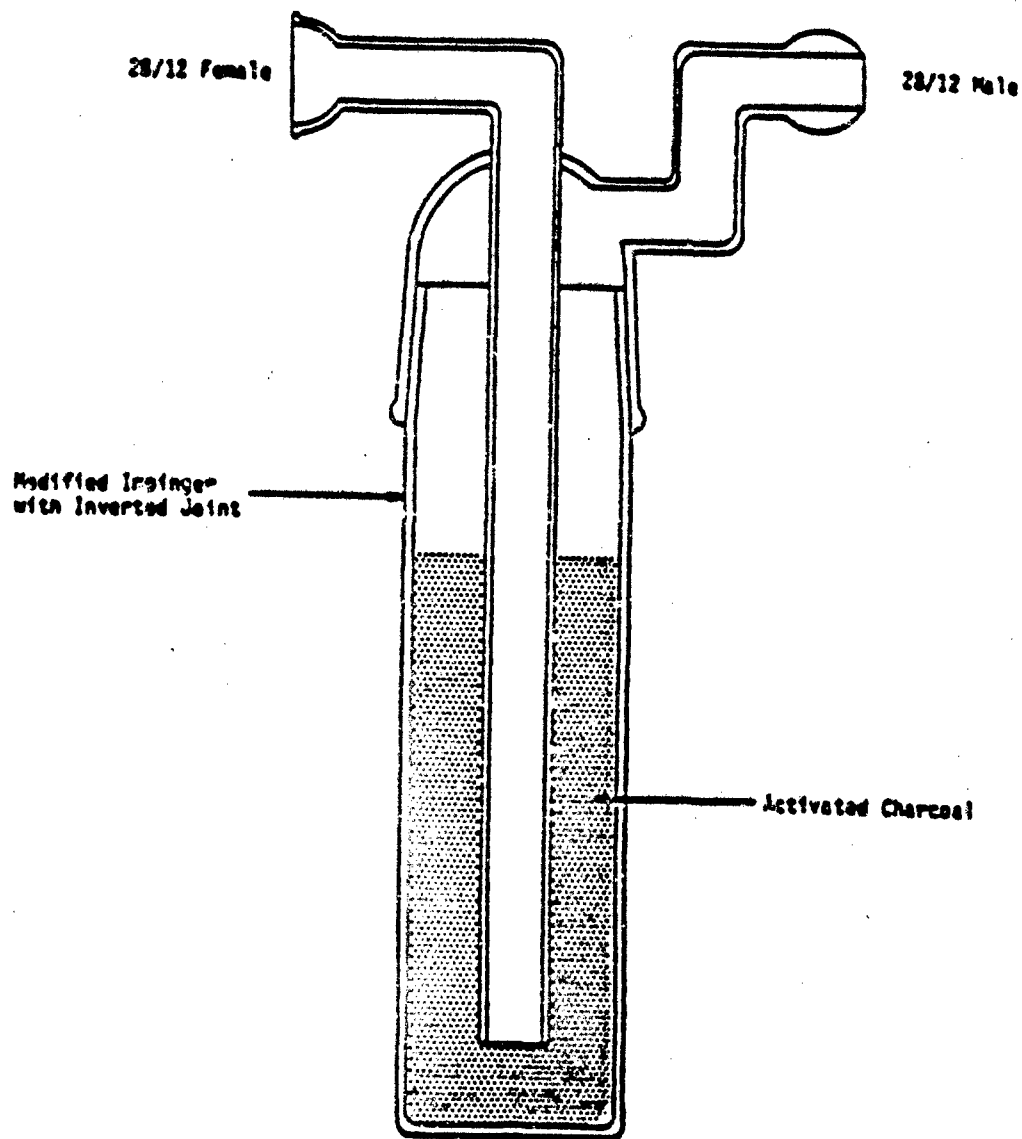


Figure 4. Leak-check impinger.

6.5.1.5 When the leak-check is completed, first slowly remove the plug from the inlet to the probe, filter holder, or cyclone (if applicable). When the vacuum drops to 127 mm (5 in.) Hg or less, immediately close the coarse-adjust valve. Switch off the pumping system and reopen the fine-adjust valve. Do not reopen the fine-adjust valve until the coarse-adjust valve has been closed. This prevents the water in the impingers from being forced backward into the organic module and silica gel from being entrained backward into the third impinger.

#### 6.5.2 Leak-checks during sampling run:

6.5.2.1 If, during the sampling run, a component (e.g., filter assembly, impinger, or sorbent trap) change becomes necessary, a leak-check shall be conducted immediately after the interruption of sampling and before the change is made. The leak-check shall be done according to the procedure outlined in Paragraph 6.5.1, except that it shall be done at a vacuum greater than or equal to the maximum value recorded up to that point in the test. If the leakage rate is found to be no greater than  $0.00057 \text{ m}^3/\text{min}$  (0.02 cfm) or 4% of the average sampling rate (whichever is less), the results are acceptable, and no correction will need to be applied to the total volume of dry gas metered. If a higher leakage rate is obtained, the tester shall void the sampling run. (It should be noted that any "correction" of the sample volume by calculation by calculation reduces the integrity of the pollutant concentrations data generated and must be avoided.)

6.5.2.2 Immediately after a component change, and before sampling is reinitiated, a leak-check similar to a pre-test leak-check must also be conducted.

#### 6.5.3 Post-test leak-check:

6.5.3.1 A leak-check is mandatory at the conclusion of each sampling run. The leak-check shall be done with the same procedures as those with the pre-test leak-check, except that it shall be conducted at a vacuum greater than or equal to the maximum value reached during the sampling run. If the leakage rate is found to be no greater than  $0.00057 \text{ m}^3/\text{min}$  (0.02 cfm) or 4% of the average sampling rate (whichever is less), the results are acceptable, and no correction need be applied to the total volume of dry gas metered. If, however, a higher leakage rate is obtained, the tester shall either record the leakage rate, correct the sample volume (as shown in the calculation section of this method), and consider the data obtained of questionable reliability, or void the sampling run.

#### 6.6 Sampling-train operation:

6.6.1 During the sampling run, maintain an isokinetic sampling rate to within 10% of true isokinetic, unless otherwise specified by the Administrator. Maintain a temperature around the filter of  $120 \pm 14^\circ\text{C}$  ( $248 \pm 25^\circ\text{F}$ ) and a gas temperature entering the sorbent trap at a maximum of  $20^\circ\text{C}$  ( $68^\circ\text{F}$ ).

6.6.2 For each run, record the data required on a data sheet such as the one shown in Figure 5. Be sure to record the initial dry-gas meter reading. Record the dry-gas meter readings at the beginning and end of each sampling time increment, when changes in flow rates are made before and after each leak-check, and when sampling is halted. Take other readings required by Figure 5 at least once at each sample point during each time increment and additional readings when significant changes (20% variation in velocity-head readings) necessitate additional adjustments in flow rate. Level and zero the manometer. Because the manometer level and zero may drift due to vibrations and temperature changes, make periodic checks during the traverse.

6.6.3 Clean the stack access ports prior to the test run to eliminate the chance of sampling deposited material. To begin sampling, remove the nozzle cap, verify that the filter and probe heating systems are at the specified temperature, and verify that the pitot tube and probe are properly positioned. Position the nozzle at the first traverse point, with the tip pointing directly into the gas stream. Immediately start the pump and adjust the flow to isokinetic conditions. Nomographs, which aid in the rapid adjustment of the isokinetic sampling rate without excessive computations, are available. These nomographs are designed for use when the Type S pitot-tube coefficient is  $0.84 \pm 0.02$  and the stack-gas equivalent density (dry molecular weight) is equal to  $29 \pm 4$ . APTD-0576 details the procedure for using the nomographs. If the stack-gas molecular weight and the pitot-tube coefficient are outside the above ranges, do not use the nomographs unless appropriate steps (Shigehara, 1974) are taken to compensate for the deviations.

6.6.4 When the stack is under significant negative pressure (equivalent to the height of the impinger stem), take care to close the coarse-adjust valve before inserting the probe into the stack, to prevent water from backing into the organic module. If necessary, the pump may be turned on with the coarse-adjust valve closed.

6.6.5 When the probe is in position, block off the openings around the probe and stack access port to prevent unrepresentative dilution of the gas stream.

6.6.6 Traverse the stack cross section, as required by EPA Method 1 or as specified by the Administrator, being careful not to bump the probe nozzle into the stack walls when sampling near the walls or when removing or inserting the probe through the access port, in order to minimize the chance of extracting deposited material.

6.6.7 During the test run, make periodic adjustments to keep the temperature around the filter holder and the organic module at the proper levels; add more ice and, if necessary, salt to maintain a temperature of  $<20^{\circ}\text{C}$  ( $68^{\circ}\text{F}$ ) at the condenser/silica gel outlet. Also, periodically check the level and zero of the manometer.

Ambient Temperature \_\_\_\_\_  
Barometric Pressure \_\_\_\_\_  
Assumed Moisture % \_\_\_\_\_  
Probe Length, m (ft) \_\_\_\_\_  
Nozzle Identification No. \_\_\_\_\_  
Average Calibrated Nozzle Diameter, cm (in) \_\_\_\_\_  
Probe Heater Setting \_\_\_\_\_  
Leak Rate, m<sup>3</sup>/min. (cfm) \_\_\_\_\_  
Probe Liner Material \_\_\_\_\_  
Static Pressure, mm Hg (in. Hg) \_\_\_\_\_  
Filter No. \_\_\_\_\_

### Schematic of Stack Cross Section

Traverse Point Number	Sampling Time (s) min.	Vacuum mm Hg (in. Hg)	Stack Temperature ( $t_s$ ) °C( $f$ )	Velocity Head { $P_v$ } mm (in.) H <sub>2</sub> O	Pressure Differential Across Orifice Meter mm (H <sub>2</sub> O) (in H <sub>2</sub> O)	Gas Sample Volume m <sup>3</sup> (ft. <sup>3</sup> )	Gas Sample Temp. at Dry Gas Meter Inlet ( $T_i$ ) Outlet ( $T_o$ ) °C( $F$ )	Filter Holder Temperature °C( $F$ )	Temperature of Gas Entering Sorbel Trap °C( $F$ )	Temperature of Gas Leaving Condenser or Last Impinger
Total Average							Avg. Avg.			

**Figure 5. Particulate field data.**

6.6.8 If the pressure drop across the filter or sorbent trap becomes too high, making isokinetic sampling difficult to maintain, the filter/sorbent trap may be replaced in the midst of a sample run. Using another complete filter holder/sorbent trap assembly is recommended, rather than attempting to change the filter and resin themselves. After a new filter/sorbent trap assembly is installed, conduct a leak-check. The total particulate weight shall include the summation of all filter assembly catches.

6.6.9 A single train shall be used for the entire sample run, except in cases where simultaneous sampling is required in two or more separate ducts or at two or more different locations within the same duct, or in cases where equipment failure necessitates a change of trains. In all other situations, the use of two or more trains will be subject to the approval of the Administrator.

6.6.10 Note that when two or more trains are used, separate analysis of the front-half (if applicable) organic-module and impinger (if applicable) catches from each train shall be performed, unless identical nozzle sizes were used on all trains. In that case, the front-half catches from the individual trains may be combined (as may the impinger catches), and one analysis of front-half catch and one analysis of impinger catch may be performed.

6.6.11 At the end of the sample run, turn off the coarse-adjust valve, remove the probe and nozzle from the stack, turn off the pump, record the final dry-gas meter reading, and conduct a post-test leak-check. Also, leak-check the pitot lines as described in EPA Method 2. The lines must pass this leak-check in order to validate the velocity-head data.

6.6.12 Calculate percent isokineticity (see Section 10.8) to determine whether the run was valid or another test run should be made.

## 7.0 SAMPLE RECOVERY

### 7.1 Preparation:

7.1.1 Proper cleanup procedure begins as soon as the probe is removed from the stack at the end of the sampling period. Allow the probe to cool. When the probe can be safely handled, wipe off all external particulate matter near the tip of the probe nozzle and place a cap over the tip to prevent losing or gaining particulate matter. Do not cap the probe tip tightly while the sampling train is cooling down because this will create a vacuum in the filter holder, drawing water from the impingers into the sorbent module.

7.1.2 Before moving the sample train to the cleanup site, remove the probe from the sample train and cap the open outlet, being careful not to lose any condensate that might be present. Cap the filter inlet.

Remove the umbilical cord from the last impinger and cap the impinger. If a flexible line is used between the organic module and the filter holder, disconnect the line at the filter holder and let any condensed water or liquid drain into the organic module.

7.1.3 Cap the filter-holder outlet and the inlet to the organic module. Separate the sorbent trap section of the organic module from the condensate knockout trap and the gas-conditioning section. Cap all organic module openings. Disconnect the organic-module knockout trap from the impinger train inlet and cap both of these openings. Ground-glass stoppers, Teflon caps, or caps of other inert materials may be used to seal all openings.

7.1.4 Transfer the probe, the filter, the organic-module components, and the impinger/condenser assembly to the cleanup area. This area should be clean and protected from the weather to minimize sample contamination or loss.

7.1.5 Save a portion of all washing solutions (methanol/methylene chloride, Type II water) used for cleanup as a blank. Transfer 200 mL of each solution directly from the wash bottle being used and place each in a separate, prelabeled glass sample container.

7.1.6 Inspect the train prior to and during disassembly and note any abnormal conditions.

## 7.2 Sample containers:

7.2.1 Container no. 1: Carefully remove the filter from the filter holder and place it in its identified Petri dish container. Use a pair or pairs of tweezers to handle the filter. If it is necessary to fold the filter, ensure that the particulate cake is inside the fold. Carefully transfer to the Petri dish any particulate matter or filter fibers that adhere to the filter-holder gasket, using a dry nylon bristle brush or sharp-edged blade, or both. Label the container and seal with 1-in.-wide Teflon tape around the circumference of the lid.

7.2.2 Container no. 2: Taking care that dust on the outside of the probe or other exterior surfaces does not get into the sample, quantitatively recover particulate matter or any condensate from the probe nozzle, probe fitting, probe liner, and front half of the filter holder by washing these components first with methanol/methylene chloride (1:1 v/v) into a glass container. Distilled water may also be used. Retain a water and solvent blank and analyze in the same manner as with the samples. Perform rinses as follows:

7.2.2.1 Carefully remove the probe nozzle and clean the inside surface by rinsing with the solvent mixture (1:1 v/v methanol/methylene chloride) from a wash bottle and brushing with a nylon bristle brush. Brush until the rinse shows no visible particles; then make a final rinse of the inside surface with the solvent mix. Brush and rinse the inside parts of the Swagelok fitting with the solvent mix in a similar way until no visible particles remain.

7.2.2.2 Have two people rinse the probe liner with the solvent mix by tilting and rotating the probe while squirting solvent into its upper end so that all inside surfaces will be wetted with solvent. Let the solvent drain from the lower end into the sample container. A glass funnel may be used to aid in transferring liquid washes to the container.

7.2.2.3 Follow the solvent rinse with a probe brush. Hold the probe in an inclined position and squirt solvent into the upper end while pushing the probe brush through the probe with a twisting action; place a sample container underneath the lower end of the probe and catch any solvent and particulate matter that is brushed from the probe. Run the brush through the probe three times or more until no visible particulate matter is carried out with the solvent or until none remains in the probe liner on visual inspection. With stainless steel or other metal probes, run the brush through in the above-prescribed manner at least six times (metal probes have small crevices in which particulate matter can be entrapped). Rinse the brush with solvent and quantitatively collect these washings in the sample container. After the brushing, make a final solvent rinse of the probe as described above.

7.2.2.4 It is recommended that two people work together to clean the probe to minimize sample losses. Between sampling runs, keep brushes clean and protected from contamination.

7.2.2.5 Clean the inside of the front half of the filter holder and cyclone/cyclone flask, if used, by rubbing the surfaces with a nylon bristle brush and rinsing with methanol/methylene chloride (1:1 v/v) mixture. Rinse each surface three times or more if needed to remove visible particulate. Make a final rinse of the brush and filter holder. Carefully rinse out the glass cyclone and cyclone flask (if applicable). Brush and rinse any particulate material adhering to the inner surfaces of these components into the front-half rinse sample. After all solvent washings and particulate matter have been collected in the sample container, tighten the lid on the sample container so that solvent will not leak out when it is shipped to the laboratory. Mark the height of the fluid level to determine whether leakage occurs during transport. Label the container to identify its contents.

7.2.3 Container no. 3: The sorbent trap section of the organic module may be used as a sample transport container, or the spent resin may be transferred to a separate glass bottle for shipment. If the sorbent trap itself is used as the transport container, both ends should be sealed with tightly fitting caps or plugs. Ground-glass stoppers or Teflon caps may be used. The sorbent trap should then be labeled, covered with aluminum foil, and packaged on ice for transport to the laboratory. If a separate bottle is used, the spent resin should be quantitatively transferred from the trap into the clean bottle. Resin that adheres to the walls of the trap should be recovered using a rubber policeman or spatula and added to this bottle.



7.2.4 Container no. 4: Measure the volume of condensate collected in the condensate knockout section of the organic module to within  $\pm 1$  mL by using a graduated cylinder or by weighing to within  $\pm 0.5$  g using a triple-beam balance. Record the volume or weight of liquid present and note any discoloration or film in the liquid catch. Transfer this liquid to a prelabeled glass sample container. Inspect the back half of the filter housing and the gas-conditioning section of the organic module. If condensate is observed, transfer it to a graduated or weighing bottle and measure the volume, as described above. Add this material to the condensate knockout-trap catch.

7.2.5 Container no. 5: All sampling train components located between the high-efficiency glass- or quartz-fiber filter and the first wet impinger or the final condenser system (including the heated Teflon line connecting the filter outlet to the condenser) should be thoroughly rinsed with methanol/methylene chloride (1:1 v/v) and the rinsings combined. This rinse shall be separated from the condensate. If the spent resin is transferred from the sorbent trap to a separate sample container for transport, the sorbent trap shall be thoroughly rinsed until all sample-wetted surfaces appear clean. Visible films should be removed by brushing. Whenever train components are brushed, the brush should be subsequently rinsed with solvent mixture and the rinsings added to this container.

7.2.6 Container no. 6: Note the color of the indicating silica gel to determine if it has been completely spent and make a notation of its condition. Transfer the silica gel from the fourth impinger to its original container and seal. A funnel may make it easier to pour the silica gel without spilling. A rubber policeman may be used as an aid in removing the silica gel from the impinger. It is not necessary to remove the small amount of dust particles that may adhere strongly to the impinger wall. Because the gain in weight is to be used for moisture calculations, do not use any water or other liquids to transfer the silica gel. If a balance is available in the field, weigh the container and its contents to 0.5 g or better.

### 7.3 Impinger water:

7.3.1 Make a notation of any color or film in the liquid catch. Measure the liquid in the first three impingers to within  $\pm 1$  mL by using a graduated cylinder or by weighing it to within  $\pm 0.5$  g by using a balance (if one is available). Record the volume or weight of liquid present. This information is required to calculate the moisture content of the effluent gas.

7.3.2 Discard the liquid after measuring and recording the volume or weight, unless analysis of the impinger catch is required (see Paragraph 4.1.3.7). Amber glass containers should be used for storage of impinger catch, if required.

7.3.3 If a different type of condenser is used, measure the amount of moisture condensed either volumetrically or gravimetrically.

**7.4 Sample preparation for shipment:** Prior to shipment, recheck all sample containers to ensure that the caps are well secured. Seal the lids of all containers around the circumference with Teflon tape. Ship all liquid samples upright on ice and all particulate filters with the particulate catch facing upward. The particulate filters should be shipped unrefrigerated.

## **8.0 ANALYSIS**

### **8.1 Sample preparation:**

**8.1.1 General:** The preparation steps for all samples will result in a finite volume of concentrated solvent. The final sample volume (usually in the 1- to 10-mL range) is then subjected to analysis by GC/MS. All samples should be inspected and the appearance documented. All samples are to be spiked with surrogate standards as received from the field prior to any sample manipulations. The spike should be at a level equivalent to 10 times the MDL when the solvent is reduced in volume to the desired level (i.e., 10 mL). The spiking compounds should be the stable isotopically labeled analog of the compounds of interest or a compound that would exhibit properties similar to the compounds of interest, be easily chromatographed, and not interfere with the analysis of the compounds of interest. Suggested surrogate spiking compounds are: deuterated naphthalene, chrysene, phenol, nitrobenzene, chlorobenzene, toluene, and carbon-13-labeled pentachlorophenol.

**8.1.2 Condensate:** The "condensate" is the moisture collected in the first impinger following the XAD-2 module. Spike the condensate with the surrogate standards. The volume is measured and recorded and then transferred to a separatory funnel. The pH is to be adjusted to pH 2 with 6 N sulfuric acid, if necessary. The sample container and graduated cylinder are sequentially rinsed with three successive 10-mL aliquots of the extraction solvent and added to the separatory funnel. The ratio of solvent to aqueous sample should be maintained at 1:3. Extract the sample by vigorously shaking the separatory funnel for 5 min. After complete separation of the phases, remove the solvent and transfer to a Kuderna-Danish concentrator (K-D), filtering through a bed of pre-cleaned, dry sodium sulfate. Repeat the extraction step two additional times. Adjust the pH to 11 with 6 N sodium hydroxide and reextract combining the acid and base extracts. Rinse the sodium sulfate into the K-D with fresh solvent and discard the desiccant. Add Teflon boiling chips and concentrate to 10 mL by reducing the volume to slightly less than 10 mL and then bringing to volume with fresh solvent. In order to achieve the necessary detection limit, the sample volume can be further reduced to 1 mL by using a micro column K-D or nitrogen blow-down. Should the sample start to exhibit precipitation, the concentration step should be stopped and the sample redissolved with fresh solvent taking the volume to some finite amount. After adding a standard (for the purpose of quantitation by GC/MS), the sample is ready for analysis, as discussed in Paragraph 8.2.

8.1.3 Impinger: Spike the sample with the surrogate standards; measure and record the volume and transfer to a separatory funnel. Proceed as described in Paragraph 8.1.2.

8.1.4 XAD-2: Spike the resin directly with the surrogate standards. Transfer the resin to the all-glass thimbles by the following procedure (care should be taken so as not to contaminate the thimble by touching it with anything other than tweezers or other solvent-rinsed mechanical holding devices). Suspend the XAD-2 module directly over the thimble. The glass frit of the module (see Figure 2) should be in the up position. The thimble is contained in a clean beaker, which will serve to catch the solvent rinses. Using a Teflon squeeze bottle, flush the XAD-2 into the thimble. Thoroughly rinse the glass module with solvent into the beaker containing the thimble. Add the XAD-2 glass-wool plug to the thimble. Cover the XAD-2 in the thimble with a precleaned glass-wool plug sufficient to prevent the resin from floating into the solvent reservoir of the extractor. If the resin is wet, effective extraction can be accomplished by loosely packing the resin in the thimble. If a question arises concerning the completeness of the extraction, a second extraction, without a spike, is advised. The thimble is placed in the extractor and the rinse solvent contained in the beaker is added to the solvent reservoir. Additional solvent is added to make the reservoir approximately two-thirds full. Add Teflon boiling chips and assemble the apparatus. Adjust the heat source to cause the extractor to cycle 5-6 times per hr. Extract the resin for 16 hr. Transfer the solvent and three 10-ml rinses of the reservoir to a K-D and concentrate as described in Paragraph 8.1.2.

8.1.5 Particulate filter (and cyclone catch): If particulate loading is to be determined, weigh the filter (and cyclone catch, if applicable). The particulate filter (and cyclone catch, if applicable) is transferred to the glass thimble and extracted simultaneously with the XAD-2 resin.

8.1.6 Train solvent rinses: All train rinses (i.e., probe, impinger, filter housing) using the extraction solvent and methanol are returned to the laboratory as a single sample. If the rinses are contained in more than one container, the intended spike is divided equally among the containers proportioned from a single syringe volume. Transfer the rinse to a separatory funnel and add a sufficient amount of organic-free water so that the methylene chloride becomes immiscible and its volume no longer increases with the addition of more water. The extraction and concentration steps are then performed as described in Paragraph 8.1.2.

## 8.2 Sample analysis:

8.2.1 The primary analytical tool for the measurement of emissions from hazardous waste incinerators is GC/MS using fused-silica capillary GC columns, as described in Method 8270 in Chapter Four of this manual. Because of the nature of GC/MS instrumentation and the cost associated

with sample analysis, prescreening of the sample extracts by chromatography/flame ionization detection (GC/FID) or with electron capture (GC/ECD) is encouraged. Information regarding the complexity and concentration level of a sample prior to GC/MS analysis can be enormous help. This information can be obtained by using either capillary columns or less expensive packed columns. However, the prescreen should be performed with a column similar to that used with GC/MS. Keep in mind that GC/FID has a slightly lower detection limit than GC/MS and, therefore, that the concentration of the sample can be adjusted either up or down prior to analysis by GC/MS.

8.2.2 The mass spectrometer will be operated in a full scan (4-450) mode for most of the analyses. The range for which data is acquired in a GC/MS run will be sufficiently broad to encompass the major ions, as listed in Chapter Four, Method 8270, for each of the designated POHCs in an incinerator effluent analysis.

8.2.3 For most purposes, electron ionization (EI) spectra will be collected because a majority of the POHCs give reasonable EI spectra. Also, EI spectra are compatible with the NBS Library of Mass Spectra and other mass spectral references, which aid in the identification process for other components in the incinerator process streams.

8.2.4 To clarify some identifications, chemical ionization (CI) spectra using either positive ions or negative ions will be used to elucidate molecular-weight information and simplify the fragmentation patterns of some compounds. In no case, however, should CI spectra alone be used for compound identification. Refer to Chapter Four, Method 8270 for complete descriptions of GC conditions, MS conditions, and quantitative and qualitative identification.

## 9.0 CALIBRATION

9.1 Probe nozzle: Probe nozzles shall be calibrated before their initial use in the field. Using a micrometer, measure the inside diameter of the nozzle to the nearest 0.025 mm (0.001 in.). Make measurements at three separate places across the diameter and obtain the average of the three measurements. The difference between the high and low numbers shall not exceed 0.1 mm (0.004 in.). When nozzles become nicked, dented, or corroded they shall be reshaped, sharpened, and recalibrated before use. Each nozzle shall be permanently and uniquely identified.

9.2 Pitot tube: The Type S pitot tube assembly shall be calibrated according to the procedure outlined in Section 4 of EPA Method 2, or assigned a nominal coefficient of 0.84 if it is not visibly nicked, dented, or corroded and if it meets design and intercomponent spacing specifications.

### 9.3 Metering system:

9.3.1 Before its initial use in the field, the metering system shall be calibrated according to the procedure outlined in APTD-0576. Instead of physically adjusting the dry-gas meter dial readings to correspond to the wet-test meter readings, calibration factors may be used to correct the gas meter dial readings mathematically to the proper values. Before calibrating the metering system, it is suggested that a leak-check be conducted. For metering systems having diaphragm pumps, the normal leak-check procedure will not detect leakages within the pump. For these cases the following leak-check procedure is suggested: Make a 10-min calibration run at  $0.00057 \text{ m}^3/\text{min}$  (0.02 cfm); at the end of the run, take the difference of the measured wet-test and dry-gas meter volumes and divide the difference by 10 to get the leak rate. The leak rate should not exceed  $0.00057 \text{ m}^3/\text{min}$  (0.02 cfm).

9.3.2 After each field use, the calibration of the metering system shall be checked by performing three calibration runs at a single intermediate orifice setting (based on the previous field test). The vacuum shall be set at the maximum value reached during the test series. To adjust the vacuum, insert a valve between the wet-test meter and the inlet of the metering system. Calculate the average value of the calibration factor. If the calibration has changed by more than 5%, recalibrate the meter over the full range of orifice settings, as outlined in APTD-0576.

9.3.3 Leak-check of metering system: That portion of the sampling train from the pump to the orifice meter (see Figure 1) should be leak-checked prior to initial use and after each shipment. Leakage after the pump will result in less volume being recorded than is actually sampled. The following procedure is suggested (see Figure 6): Close the main valve on the meter box. Insert a one-hole rubber stopper with rubber tubing attached into the orifice exhaust pipe. Disconnect and vent the low side of the orifice manometer. Close off the low side orifice tap. Pressurize the system to 13-18 cm (5-7 in.) water column by blowing into the rubber tubing. Pinch off the tubing and observe the manometer for 1 min. A loss of pressure on the manometer indicates a leak in the meter box. Leaks, if present, must be corrected.

NOTE: If the dry-gas-meter coefficient values obtained before and after a test series differ by >5%, either the test series shall be voided or calculations for test series shall be performed using whichever meter coefficient value (i.e., before or after) gives the lower value of total sample volume.

9.4 Probe heater: The probe-heating system shall be calibrated before its initial use in the field according to the procedure outlined in APTD-0576. Probes constructed according to APTD-0581 need not be calibrated if the calibration curves in APTD-0576 are used.

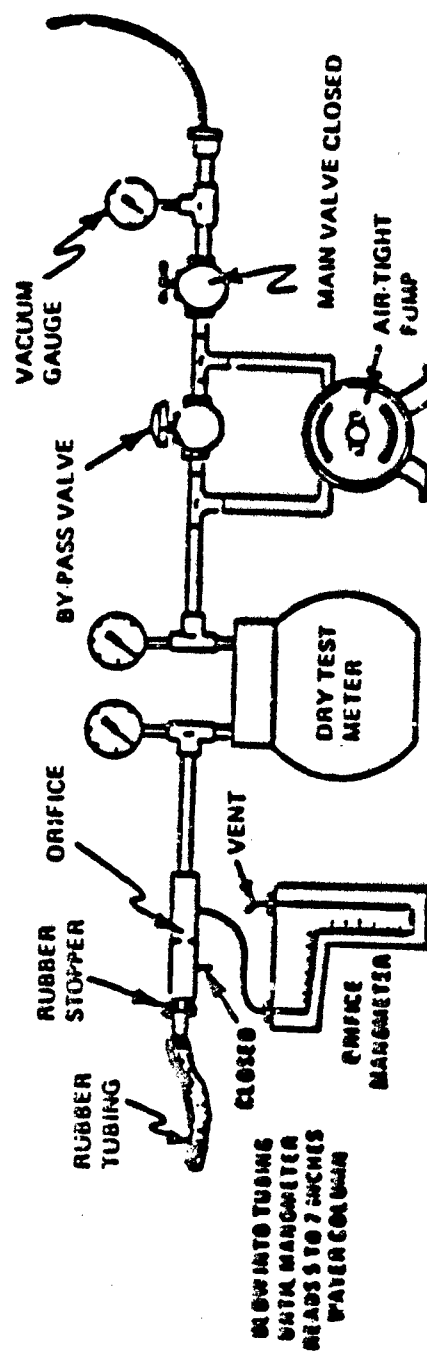


Figure 6. Leak check of meter box.

9.5 Temperature gauges: Each thermocouple must be permanently and uniquely marked on the casting; all mercury-in-glass reference thermometers must conform to ASTM E-1 63C or 63F specifications. Thermocouples should be calibrated in the laboratory with and without the use of extension leads. If extension leads are used in the field, the thermocouple readings at ambient air temperatures, with and without the extension lead, must be noted and recorded. Correction is necessary if the use of an extension lead produces a change  $>1.5\%$ .

9.5.1 Impinger, organic module, and dry-gas meter thermocouples: For the thermocouples used to measure the temperature of the gas leaving the impinger train and the XAD-2 resin bed, three-point calibration at ice-water, room-air, and boiling-water temperatures is necessary. Accept the thermocouples only if the readings at all three temperatures agree to  $\pm 2^{\circ}\text{C}$  ( $3.6^{\circ}\text{F}$ ) with those of the absolute value of the reference thermometer.

9.5.2 Probe and stack thermocouple: For the thermocouples used to indicate the probe and stack temperatures, a three-point calibration at ice-water, boiling-water, and hot-oil-bath temperatures must be performed; it is recommended that room-air temperature be added, and that the thermometer and the thermocouple agree to within 1.5% at each of the calibration points. A calibration curve (equation) may be constructed (calculated) and the data extrapolated to cover the entire temperature range suggested by the manufacturer.

9.6 Barometer: Adjust the barometer initially and before each test series to agree to within  $\pm 25$  mm Hg (0.1 in. Hg) of the mercury barometer or the corrected barometric pressure value reported by a nearby National Weather Service Station (same altitude above sea level).

9.7 Triple-beam balance: Calibrate the triple-beam balance before each test series, using Class-S standard weights; the weights must be within  $\pm 0.5\%$  of the standards, or the balance must be adjusted to meet these limits.

## 10.0 CALCULATIONS

10.1 Carry out calculations. Round off figures after the final calculation to the correct number of significant figures.

### 10.2 Nomenclature:

$A_n$  = Cross-sectional area of nozzle,  $\text{m}^2$  ( $\text{ft}^2$ ).

$\beta_{ws}$  = Water vapor in the gas stream, proportion by volume.

$C_d$  = type S pitot tube coefficient (nominally  $0.84 \pm 0.02$ ), dimensionless.

$I$  = Percent of isokinetic sampling.

- $L_a$  = Maximum acceptable leakage rate for a leak-check, either pre-test or following a component change; equal to 0.00057 m<sup>3</sup>/min (0.0 cfm) or 4% of the average sampling rate, whichever is less.
- $L_i$  = Individual leakage rate observed during the leak-check conducted prior to the "i<sup>th</sup>" component change (i = 1, 2, 3...n) m<sup>3</sup>/min (cfm).
- $L_p$  = Leakage rate observed during the post-test leak-check, m<sup>3</sup>/min (cfm).
- $M_d$  = Stack-gas dry molecular weight, g/g-mole (lb/lb-mole).
- $M_w$  = Molecular weight of water, 18.0 g/g-mole (18.0 lb/lb-mole).
- $P_{bar}$  = Barometric pressure at the sampling site, mm Hg (in. Hg).
- $P_s$  = Absolute stack-gas pressure, mm Hg (in. Hg).
- $P_{std}$  = Standard absolute pressure, 760 mm Hg (29.92 in. Hg).
- $R$  = Ideal gas constant, 0.06236 mm Hg-m<sup>3</sup>/K-g-mole (21.85 in. Hg-ft<sup>3</sup>/°R-lb-mole).
- $T_m$  = Absolute average dry-gas meter temperature (see Figure 6), K (°R).
- $T_s$  = Absolute average stack-gas temperature (see Figure 6), K (°R).
- $T_{std}$  = Standard absolute temperature, 293K (528°R).
- $V_{lc}$  = Total volume of liquid collected in the organic module condensate knockout trap, the impingers, and silica gel, mL.
- $V_m$  = Volume of gas sample as measured by dry-gas meter, dscm (dscf).
- $V_m(std)$  = Volume of gas sample measured by the dry-gas meter, corrected to standard conditions, dscm (dscf).
- $V_w(std)$  = Volume of water vapor in the gas sample, corrected to standard conditions, scm (scf).
- $v_s$  = Stack-gas velocity, calculated by Method 2, Equation 2-9, using data obtained from Method 5, m/sec (ft/sec).
- $W_a$  = Weight of residue in acetone wash, mg.
- $\gamma$  = Dry-gas-meter calibration factor, dimensionless.
- $\Delta H$  = Average pressure differential across the orifice meter (see Figure 2), mm H<sub>2</sub>O (in. H<sub>2</sub>O).



$\rho_w$  = Density of water, 0.9982 g/mL (0.002101 lb/L).

$t$  = Total sampling time, min.

$t_1$  = Sampling time interval from the beginning of a run until the first component change, min.

$t_i$  = Sampling time interval between two successive component changes, beginning with the interval between the first and second changes, min.

$t_p$  = Sampling time interval from the final (nth) component change until the end of the sampling run, min.

13.6 = Specific gravity of mercury.

60 = sec/min.

100 = Conversion to percent.

10.3 Average dry-gas-meter temperature and average orifice pressure drop: See data sheet (Figure 5, above).

10.4 Dry-gas volume: Correct the sample measured by the dry-gas meter to standard conditions (20°C, 760 mm Hg [68°F, 29.92 in. Hg]) by using Equation 1:

$$V_{m(std)} = V_m \frac{T_{std}}{T_m} \frac{P_{bar} + \Delta H/13.6}{P_{std}} = K_1 V_m \frac{P_{bar} + \Delta H/13.6}{T_m} \quad (1)$$

where:

$K_1$  = 0.3858 K/mm Hg for metric units, or  
 $K_1$  = 17.64°R/in. Hg for English units.

It should be noted that Equation 1 can be used as written, unless the leakage rate observed during any of the mandatory leak-checks (i.e., the post-test leak-check or leak-checks conducted prior to component changes) exceeds  $L_a$ . If  $L_p$  or  $L_i$  exceeds  $L_a$ , Equation 1 must be modified as follows:

- a. Case 1 (no component changes made during sampling run): Replace  $V_m$  in Equation 1 with the expression:

$$V_m = (L_p - L_a)$$

- d. Case II (one or more component changes made during the sampling run): Replace  $V_m$  in Equation 1 by the expression:

$$V_m = (L_1 - L_2) V_1 - \sum_{i=2}^n (L_1 - L_i) V_1 - (L_p - L_2) V_p$$

and substitute only for those leakage rates ( $L_1$  or  $L_p$ ) that exceed  $L_a$ .

#### 10.5 Volume of water vapor:

$$V_{w(std)} = V_{1c} \frac{P_w}{P_{std}} \frac{RT_{std}}{P_{std}} = K_2 V_{1c} \quad (2)$$

where:

$K_2 = 0.001333 \text{ m}^3/\text{mL}$  for metric units, or  
 $K_2 = 0.04707 \text{ ft}^3/\text{mL}$  for English units.

#### 10.6 Moisture content:

$$B_{ws} = \frac{V_{w(std)}}{V_m(std) + V_{w(std)}} \quad (3)$$

NOTE: In saturated or water-droplet-laden gas streams, two calculations of the moisture content of the stack gas shall be made, one from the impinger analysis (Equation 3) and a second from the assumption of saturated conditions. The lower of the two values of  $B_w$  shall be considered correct. The procedure for determining the moisture content based upon assumption of saturated conditions is given in the Note to Section 1.2 of Method 4. For the purposes of this method, the average stack-gas temperature from Figure 6 may be used to make this determination, provided that the accuracy of the in-stack temperature sensor is  $\pm 1^\circ\text{C}$  ( $2^\circ\text{F}$ ).

#### 10.7 Conversion factors:

From	To	Multiply by
scf	$\text{m}^3$	0.02832
g/ft <sup>3</sup>	gr/ft <sup>3</sup>	15.43
g/ft <sup>3</sup>	lb/ft <sup>3</sup>	$2.205 \times 10^{-3}$
g/ft <sup>3</sup>	g/m <sup>3</sup>	35.31

### 10.3 Isokinetic variation:

#### 10.3.1 Calculation from raw data:

$$I = \frac{100 T_s [K_3 F_{lc} + (V_s/T_m) (P_{bar} + 3H/13.6)]}{503 V_s P_s A_n} \quad (4)$$

where:

$K_3 = 0.003454 \text{ mm Hg-m}^3/\text{mL-K}$  for metric units, or  
 $K_3 = 0.002569 \text{ in. Hg-ft}^3/\text{mL-}^\circ\text{R}$  for English units.

#### 10.3.2 Calculation for intermediate values:

$$I = \frac{T_s V_m(\text{std}) P_{\text{std}} 100}{T_{\text{std}} V_s A_n P_s 60 (1 - \theta_{ws})} \quad (5)$$

$$= K_4 \frac{T_s V_m(\text{std})}{P_s V_s A_n (1 - \theta_{ws})}$$

where:

$K_4 = 4.320$  for metric units, or  
 $K_4 = 0.09450$  for English units.

10.3.3 Acceptable results: If  $90\% \leq I \leq 110\%$ , the results are acceptable. If the results are low in comparison with the standard and  $I$  is beyond the acceptable range, or if  $I$  is less than 90%, the Administrator may opt to accept the results.

10.9 To determine the minimum sample volume that shall be collected, the following sequence of calculations shall be used.

10.9.1 From prior analysis of the waste feed, the concentration of POHCs introduced into the combustion system can be calculated. The degree of destruction and removal efficiency that is required is used to determine the maximum amount of POHC allowed to be present in the effluent. This may be expressed as:

$$\frac{(WF) (\text{POHC}_i \text{ conc}) (100 - \text{DRE})}{100} = \text{Max POHC}_i \text{ Mass} \quad (6)$$

where:

$WF$  = mass flow rate of waste feed per hr, g/hr (lb/hr).

$\text{POHC}_i$  = concentration of Principal Organic Hazardous Compound (wt %) introduced into the combustion process.

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DRE = percent Destruction and Removal Efficiency required.

Max POHC = mass flow rate (g/hr [lb/hr]) of POHC emitted from the combustion source.

10.9.2 The average discharge concentration of the POHC in the effluent gas is determined by comparing the Max POHC with the volumetric flow rate being exhausted from the source. Volumetric flow rate data are available as a result of preliminary Method 1-4 determinations:

$$\frac{\text{Max POHC}_i \text{ Mass}}{DV_{\text{eff}}(\text{std})} = \text{Max POHC}_i \text{ conc} \quad (7)$$

where:

$DV_{\text{eff}}(\text{std})$  = volumetric flow rate of exhaust gas, dscm (dscf).

$\text{POHC}_i \text{ conc}$  = anticipated concentration of the POHC in the exhaust gas stream, g/dscm (lb/dscf).

10.9.3 In making this calculation, it is recommended that a safety margin of at least ten be included:

$$\frac{LDL_{\text{POHC}} \times 10}{\text{POHC}_i \text{ conc}} = V_{\text{TBC}} \quad (8)$$

where:

$LDL_{\text{POHC}}$  = detectable amount of POHC in entire sampling train.

NOTE: The whole extract from an XAD-2 cartridge is seldom if ever, injected at once. Therefore, if aliquoting factors are involved, the  $LDL_{\text{POHC}}$  is not the same as the analytical (or column) detection limit.

$V_{\text{TBC}}$  = minimum dry standard volume to be collected at dry-gas meter.

10.10 Concentration of any given POHC in the gaseous emissions of a combustion process:

1) Multiply the concentration of the POHC as determined in Method 8270 by the final concentration volume, typically 10 mL.

$$C_{\text{POHC}} (\text{ug/mL}) \times \text{sample volume (mL)} = \text{amount (ug) of POHC in sample} \quad (9)$$

Notes:

$C_{POHC}$  = concentration of POHC as analyzed by Method 8270.

2) Sum the amount of POHC found in all samples associated with a single train.

$$\text{Total (ug)} = \text{XAD-2 (ug)} + \text{condensate (ug)} + \text{rinses (ug)} + \text{impinger (ug)} \quad (10)$$

3) Divide the total ug found by the volume of stack gas sampled ( $m^3$ ).

$$(\text{Total ug})/(\text{train sample volume}) = \text{concentration of POHC (ug}/m^3) \quad (11)$$

## 11.0 QUALITY CONTROL

11.1 Sampling: See EPA Manual 600/4-77-027b for Method 5 quality control.

11.2 Analysis: The quality assurance program required for this study includes the analysis of field and method blanks, procedure validations, incorporation of stable labeled surrogate compounds, quantitation versus stable labeled internal standards, capillary column performance checks, and external performance tests. The surrogate spiking compounds selected for a particular analysis are used as primary indicators of the quality of the analytical data for a wide range of compounds and a variety of sample matrices. The assessment of combustion data, positive identification, and quantitation of the selected compounds are dependent on the integrity of the samples received and the precision and accuracy of the analytical methods employed. The quality assurance procedures for this method are designed to monitor the performance of the analytical method and to provide the required information to take corrective action if problems are observed in laboratory operations or in field sampling activities.

11.2.1 Field Blanks: Field blanks must be submitted with the samples collected at each sampling site. The field blanks include the sample bottles containing aliquots of sample recovery solvents, unused filters, and resin cartridges. At a minimum, one complete sampling train will be assembled in the field staging area, taken to the sampling area, and leak-checked at the beginning and end of the testing (or for the same total number of times as the actual test train). The filter housing and probe of the blank train will be heated during the sample test. The train will be recovered as if it were an actual test sample. No gaseous sample will be passed through the sampling train.

11.2.2 Method blanks: A method blank must be prepared for each set of analytical operations, to evaluate contamination and artifacts that can be derived from glassware, reagents, and sample handling in the laboratory.

11.2.3 Refer to Method 8270 for additional quality control considerations.

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## 12.0 METHOD PERFORMANCE

12.1 Method performance evaluation: Evaluation of analytical procedure for a selected series of compounds must include the sample-preparation procedures and each associated analytical determination. The analytical procedures should be challenged by the test compounds spiked at appropriate levels and carried through the procedures.

12.2 Method detection limit: The overall method detection limits (lower and upper) must be determined on a compound-by-compound basis because different compounds may exhibit different collection, retention, and extraction efficiencies as well as instrumental minimum detection limit (MDL). The method detection limit must be quoted relative to a given sample volume. The upper limits for the method must be determined relative to compound retention volumes (breakthrough).

12.3 Method precision and bias: The overall method precision and bias must be determined on a compound-by-compound basis at a given concentration level. The method precision value would include a combined variability due to sampling, sample preparation, and instrumental analysis. The method bias would be dependent upon the collection, retention, and extraction efficiency of the train components. From evaluation studies to date using a dynamic spiking system, method biases of -13% and -16% have been determined for toluene and 1,1,2,2-tetrachloroethane, respectively. A precision of 19.9% was calculated from a field test data set representing seven degrees of freedom which resulted from a series of paired, unspiked Semivolatile Organic Sampling trains (Semi-VOST) sampling emissions from a hazardous waste incinerator.

## 13.0 REFERENCES

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## METHOD 0010, APPENDIX A

### PREPARATION OF XAD-2 SORBENT RESIN

#### 1.0 SCOPE AND APPLICATION

1.1 XAD-2 resin as supplied by the manufacturer is impregnated with a bicarbonate solution to inhibit microbial growth during storage. Both the salt solution and any residual extractable monomer and polymer species must be removed before use. The resin is prepared by a series of water and organic extractions, followed by careful drying.

#### 2.0 EXTRACTION

2.1 Method 1: The procedure may be carried out in a giant Soxhlet extractor. An all-glass thimble containing an extra-coarse frit is used for extraction of XAD-2. The frit is recessed 10-15 mm above a crenellated ring at the bottom of the thimble to facilitate drainage. The resin must be carefully retained in the extractor cup with a glass-wool plug and stainless steel screen because it floats on methylene chloride. This process involves sequential extraction in the following order.

<u>Solvent</u>	<u>Procedure</u>
Water	Initial rinse: Place resin in a beaker, rinse once with Type II water, and discard. Fill with water a second time, let stand overnight, and discard.
Water	Extract with H <sub>2</sub> O for 8 hr.
Methyl alcohol	Extract for 22 hr.
Methylene chloride	Extract for 22 hr.
Methylene chloride (fresh)	Extract for 22 hr.

#### 2.2 Method 2:

2.2.1 As an alternative to Soxhlet extraction, a continuous extractor has been fabricated for the extraction sequence. This extractor has been found to be acceptable. The particular canister used for the apparatus shown in Figure A-1 contains about 500 g of finished XAD-2. Any size may be constructed; the choice is dependent on the needs of the sampling programs. The XAD-2 is held under light spring tension between a pair of coarse and fine screens. Spacers under the bottom screen allow for even distribution of clean solvent. The three-necked flask should be of sufficient size (3-liter in this case) to hold solvent



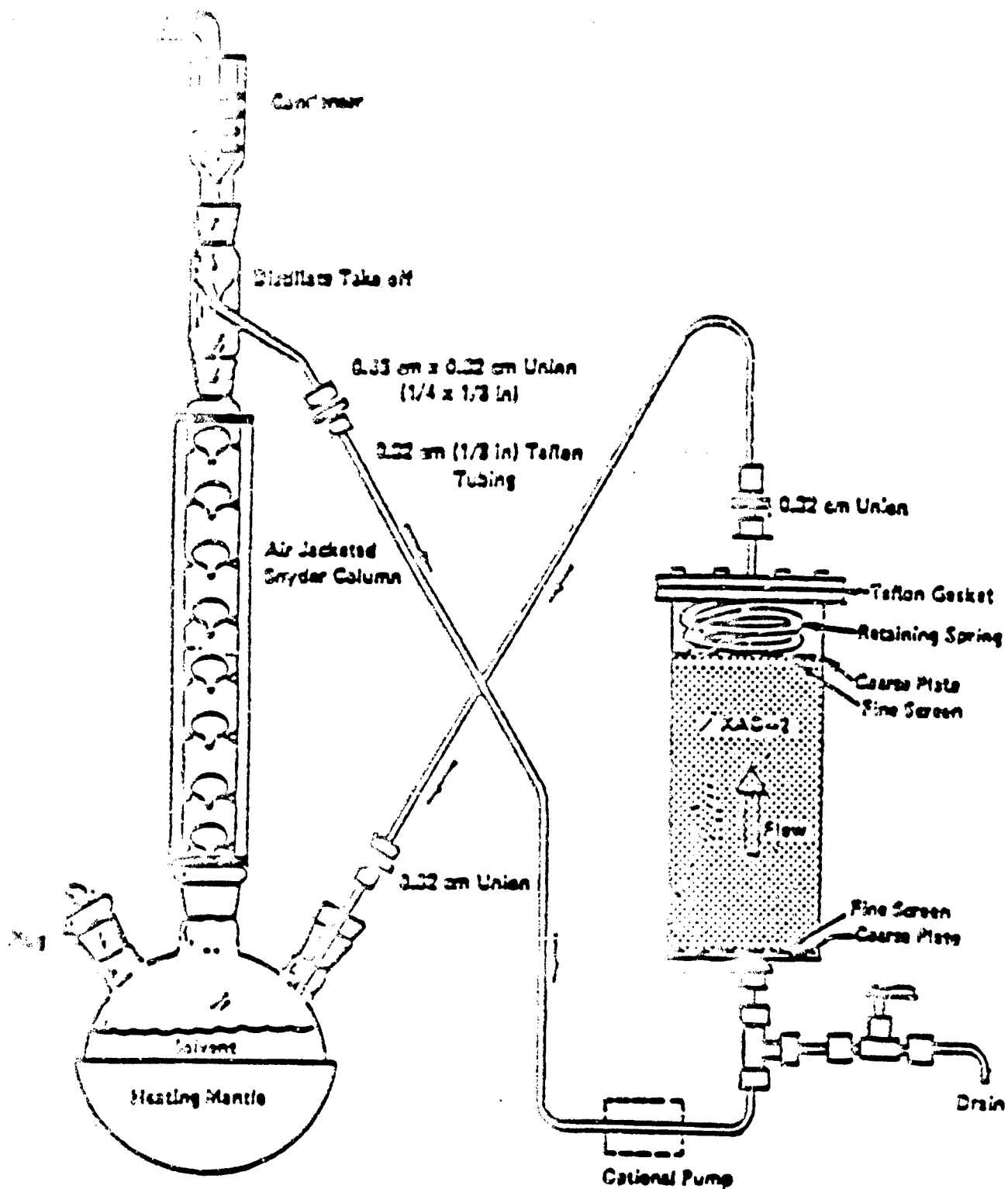


Figure A-1. XAD-2 cleanup extraction apparatus.

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equal to twice the dead volume of the XAD-2 canister. Solvent is refluxed through the Snyder column, and the distillate is continuously cycled up through the XAD-2 for extraction and returned to the flask. The flow is maintained upward through the XAD-2 to allow maximum solvent contact and prevent channeling. A valve at the bottom of the canister allows removal of solvent from the canister between changes.

2.2.2 Experience has shown that it is very difficult to cycle sufficient water in this mode. Therefore the aqueous rinse is accomplished by simply flushing the canister with about 20 liters of distilled water. A small pump may be useful for pumping the water through the canister. The water extraction should be carried out at the rate of about 20-40 mL/min.

2.2.3 After draining the water, subsequent methyl alcohol and methylene chloride extractions are carried out using the refluxing apparatus. An overnight or 10- to 20-hr period is normally sufficient for each extraction.

2.2.4 All materials of construction are glass, Teflon, or stainless steel. Pumps, if used, should not contain extractable materials. Pumps are not used with methanol and methylene chloride.

### 3.0 DRYING

3.1 After evaluation of several methods of removing residual solvent, a fluidized-bed technique has proved to be the fastest and most reliable drying method.

3.2 A simple column with suitable retainers, as shown in Figure A-2, will serve as a satisfactory column. A 10.2-cm (4-in.) Pyrex pipe 0.6 m (2 ft) long will hold all of the XAD-2 from the extractor shown in Figure A-1 or the Soxhlet extractor, with sufficient space for fluidizing the bed while generating a minimum resin load at the exit of the column.

3.3 Method 1: The gas used to remove the solvent is the key to preserving the cleanliness of the XAD-2. Liquid nitrogen from a standard commercial liquid nitrogen cylinder has routinely proved to be a reliable source of large volumes of gas free from organic contaminants. The liquid nitrogen cylinder is connected to the column by a length of precleaned 0.95-cm (3/8-in.) copper tubing, coiled to pass through a heat source. As nitrogen is bled from the cylinder, it is vaporized in the heat source and passes through the column. A convenient heat source is a water bath heated from a steam line. The final nitrogen temperature should only be warm to the touch and not over 40°C. Experience has shown that about 500 g of XAD-2 may be dried overnight by consuming a full 160-liter cylinder of liquid nitrogen.

3.4 Method 2: As a second choice, high-purity tank nitrogen may be used to dry the XAD-2. The high-purity nitrogen must first be passed through a bed

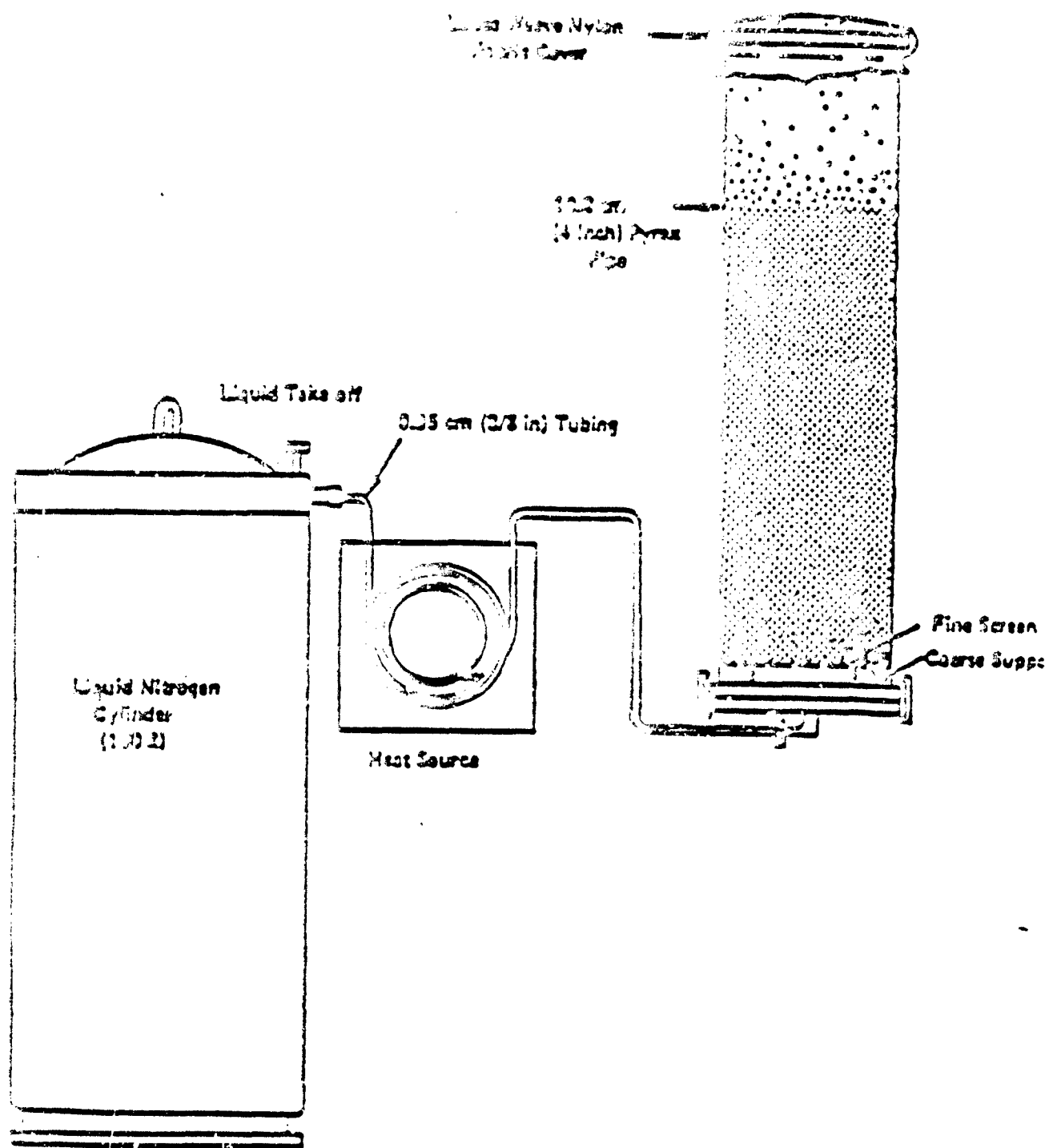


Figure A-2. XAD-2 fluidized-bed drying apparatus.

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of activated charcoal approximately 150 mL in volume. With either type of drying method, the rate of flow should gently agitate the bed. Excessive fluidization may cause the particles to break up.

### 3.0 QUALITY CONTROL PROCEDURES

4.1 For both Methods 1 and 2, the quality control results must be reported for the batch. The batch must be reextracted if the residual extractable organics are  $>20$  ug/mL by TCO analysis or the gravimetric residue is  $>0.5$  mg/20 g XAD-2 extracted. (See also section 5.1, Method 0010.)

4.2 Four control procedures are used with the final XAD-2 to check for (1) residual methylene chloride, (2) extractable organics (TCO), (3) specific compounds of interest as determined by GC/MS, as described in Section 4.5 below, and (4) residue (GRAV).

#### 4.3 Procedure for residual methylene chloride:

4.3.1 Description: A  $1\pm0.1$ -g sample of dried resin is weighed into a small vial, 3 mL of toluene are added, and the vial is capped and well shaken. Five uL of toluene (now containing extracted methylene chloride) are injected into a gas chromatograph, and the resulting integrated area is compared with a reference standard. The reference solution consists of 2.5 uL of methylene chloride in 100 mL of toluene, simulating 100 ug of residual methylene chloride on the resin. The acceptable maximum content is 1,000 ug/g resin.

4.3.2 Experimental: The gas chromatograph conditions are as follows:

6-ft x 1/8-in. stainless steel column containing 10% OV-101 on 100/120 Supelcoport;

Helium carrier at 30 mL/min;

FID operated on  $4 \times 10^{-11}$  A/mV;

Injection port temperature: 250°C;

Detector temperature: 305°C;

Program: 30°C(4 min) 40°C/min 250°C (hold); and

Program terminated at 1,000 sec.

#### 4.4 Procedure for residual extractable organics:

4.4.1 Description: A  $20\pm0.1$ -g sample of cleaned, dried resin is weighed into a precleaned alundum or cellulose thimble which is plugged with cleaned glass wool. (Note that 20 g of resin will fill a thimble, and the

resin will float out unless well plugged.) The thimble containing the resin is extracted for 24 hr with 200-mL of pesticide-grade methylene chloride (Burdick and Jackson pesticide-grade or equivalent purity). The 200-mL extract is reduced in volume to 10-mL using a Kuderna-Danish concentrator and/or a nitrogen evaporation stream. Five  $\mu$ L of that solution are analyzed by gas chromatography using the TCO analysis procedure. The concentrated solution should not contain  $>20$   $\mu$ g/mL of TCO extracted from the XAD-2. This is equivalent to 10  $\mu$ g/g of TCO in the XAD-2 and would correspond to 1.3 mg of TCO in the extract of the 130-g XAD-2 module. Care should be taken to correct the TCO data for a solvent blank prepared (200 mL reduced to 10 mL) in a similar manner.

4.4.2 Experimental: Use the TCO analysis conditions described in the revised Level 1 manual (EPA 600/7-78-201).

4.5 GC/MS Screen: The extract, as prepared in paragraph 4.4.1, is subjected to GC/MS analysis for each of the individual compounds of interest. The GC/MS procedure is described in Chapter Four, Method 8270. The extract is screened at the MDL of each compound. The presence of any compound at a concentration  $>25$   $\mu$ g/mL in the concentrated extract will require the XAD-2 to be recleaned by repeating the methylene chloride step.

4.5 Methodology for residual gravimetric determination: After the TCO value and GC/MS data are obtained for the resin batch by the above procedures, dry the remainder of the extract in a tared vessel. There must be  $<0.5$  mg residue registered or the batch of resin will have to be extracted with fresh methylene chloride again until it meets this criterion. This level corresponds to 25  $\mu$ g/g in the XAD-2, or about 3.25 mg in a resin charge of 130 g.

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TOTAL CHROMATOGRAPHABLE ORGANIC MATERIAL ANALYSIS

## 1.0 SCOPE AND APPLICATION

1.1 In this procedure, gas chromatography is used to determine the quantity of lower boiling hydrocarbons (boiling points between 90° and 300°C) in the concentrates of all organic solvent rinses, XAD-2 resin and LC fractions - when Method 1 is used (see References, Method 0010) - encountered in Level 1 environmental sample analyses. Data obtained using this procedure serve a twofold purpose. First, the total quantity of the lower boiling hydrocarbons in the sample is determined. Then whenever the hydrocarbon concentrations in the original concentrates exceed 75 ug/m<sup>3</sup>, the chromatography results are reexamined to determine the amounts of individual species.

The extent of compound identification is limited to representing all materials as normal alkanes based upon comparison of boiling points. Thus the method is not qualitative. In a similar manner, the analysis is semiquantitative; calibrations are prepared using only one hydrocarbon. They are replicated but samples routinely are not.

1.2 Application: This procedure applies solely to the Level 1 C7-C16 gas chromatographic analysis of concentrates of organic extracts, neat liquids, and of LC fractions. Throughout the procedure, it is assumed the analyst has been given a properly prepared sample.

1.3 Sensitivity: The sensitivity of this procedure, defined as the slope of a plot of response versus concentration, is dependent on the instrument and must be verified regularly. TRW experience indicates the nominal range is of the order of 77 uV-V-sec-uL/ng of n-heptane and 79 uV-sec-uL/ng of n-hexadecane. The instrument is capable of perhaps one hundredfold greater sensitivity. The level specified here is sufficient for Level 1 analysis.

1.4 Detection limit: The detection limit of this procedure as written is 1.3 ng/uL for a 1 uL injection of n-decane. This limit is arbitrarily based on defining the minimum detectable response as 100 uV-sec. This is an easier operational definition than defining the minimum detection limit to be that amount of material which yields a signal twice the noise level.

1.5 Range: The range of the procedure will be concentrations of 1.3 ng/uL and greater.

1.6 Limitations

1.6.1 Reporting limitations: It should be noted that a typical environmental sample will contain compounds which: (a) will not elute in the specified boiling ranges and thus will not be reported, and/or (b)

will not elute from the column at all and thus will not be reported. Consequently, the organic content of the sample as reported is a lower bound and should be regarded as such.

1.6.2 Calibration limitations: Quantitation is based on calibration with n-decane. Data should therefore be reported as, e.g., mg C<sub>8</sub>/m<sup>3</sup> as n-decane. Since response varies linearly with carbon number (over a wide range the assumption may involve a 20% error), it is clear that heptane (C<sub>7</sub>) detected in a sample and quantitated as decane will be overestimated. Likewise, hexadecane (C<sub>16</sub>) quantitated as decane will be underestimated. From previous data, it is estimated the error involved is on the order of 6-7%.

1.6.3 Detection limitations: The sensitivity of the flame ionization detector varies from compound to compound. However, n-alkanes have a greater response than other classes. Consequently, using an n-alkane as a calibrant and assuming equal responses of all other compounds tends to give low reported values.

## 2.0 SUMMARY OF METHOD

2.1 A  $\mu$ L aliquot of all 10-mL concentrates is disbursed for GC-TCO analysis. With boiling point-retention time and response-amount calibration curves, the data (peak retention times and peak areas) are interpreted by first summing peak areas in the ranges obtained from the boiling point-retention time calibration. Then, with the response-amount calibration curve, the area sums are converted to amounts of material in the reported boiling point ranges.

2.2 After the instrument is set up, the boiling point-retention time calibration is effected by injecting a mixture of n-C<sub>7</sub> through n-C<sub>16</sub> hydrocarbons and operating the standard temperature program. Response-quantity calibrations are accomplished by injecting n-decane in n-pentane standards and performing the standard temperature program.

### 2.3 Definitions

2.3.1 GC: Gas chromatography or gas chromatograph.

2.3.2 C<sub>7</sub>-C<sub>16</sub> n-alkanes: Heptane through hexadecane.

2.3.3 SCA temperature program: 4 min isothermal at 60°C, 10°C/min from 60° to 220°C.

2.3.4 TRV temperature program: 5 min isothermal at room temperature, then program from 30°C to 250°C at 15°C/min.

## 3.0 INTERFERENCES

Not applicable.

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#### 4.0 APPARATUS AND MATERIALS

4.1 Gas chromatograph: This procedure is intended for use on a Varian 1360 gas chromatograph, equipped with dual flame ionization detectors and a linear temperature programmer. Any equivalent instrument can be used provided that electrometer settings, etc., be changed appropriately.

##### 4.2 Gases:

4.2.1 Helium: Minimum quality is reactor grade. A 4A or 13X molecular sieve drying tube is required. A filter must be placed between the trap and the instrument. The trap should be recharged after every third tank of helium.

4.2.2 Air: Zero grade is satisfactory.

4.2.3 Hydrogen: Zero grade.

4.3 Syringe: Syringes are Hamilton 701N, 10 uL, or equivalent.

4.4 Septa: Septa will be of such quality as to produce very low bleed during the temperature program. An appropriate septum is Supelco Microsep 133, which is teflon-backed. If septum bleed cannot be reduced to a negligible level, it will be necessary to install septum swingers on the instrument.

4.5 Recorder: The recorder of this procedure must be capable of not less than 1 mV full-scale display, a 1-sec time constant and 0.5 in. per min chart rate.

4.6 Integrator: An integrator is required. Peak area measurement by hand is satisfactory but too time-consuming. If manual integration is required, the method of "height times width at half height" is used.

##### 4.7 Columns:

4.7.1 Preferred column: 6 ft x 1/8 in. O.D. stainless steel column of 10% OV-101 on 100/120 mesh Supelcoport.

4.7.2 Alternate column: 6 ft x 1/8 in. O.D. stainless steel column of 10% OV-1 (or other silicon phase) on 100/120 mesh Supelcoport.

4.8 Syringe cleaner: Hamilton syringe cleaner or equivalent connected to a suitable vacuum source.

#### 5.0 REAGENTS

5.1 Pentane: "Distilled-in-Glass" (reg. trademark) or "Nanograde" (reg. trademark) for standards and for syringe cleaning.



5.2 Methylene chloride: "Distilled-in-Glass" (reg. trademark) or "Anagrade" (reg. trademark) for syringe cleaning.

## 6.0 SAMPLING HANDLING AND PRESERVATION

6.1 The extracts are concentrated in a Kuderna-Danish evaporator to a volume less than 10 mL. The concentrate is then quantitatively transferred to a 10-mL volumetric flask and diluted to volume. A 1-mL aliquot is taken for both this analysis and possible subsequent GC/MS analysis and set aside in the sample bank. For each GC-TCO analysis, obtain the sample sufficiently in advance to allow it to warm to room temperature. For example, after one analysis is started, return that sample to the sample bank and take the next sample.

## 7.0 PROCEDURES

7.1 Setup and checkout: Each day, the operator will verify the following:

7.1.1 That supplies of carrier gas, air and hydrogen are sufficient, i.e., that each tank contains > 100 psig.

7.1.2 That, after replacement of any gas cylinder, all connections leading to the chromatograph have been leak-checked.

7.1.3 That the carrier gas flow rate is  $30 \pm 2$  mL/min, the hydrogen flow rate is  $30 \pm 2$  mL/min, and the air flow rate is  $300 \pm 20$  mL/min.

7.1.4 That the electrometer is functioning properly.

7.1.5 That the recorder and integrator are functioning properly.

7.1.6 That the septa have been leak-checked (leak-checking is effected by placing the soap bubble flow meter inlet tube over the injection port adaptors), and that no septum will be used for more than 20 injections.

7.1.7 That the list of samples to be run is ready.

7.2 Retention time calibration:

7.2.1 To obtain the temperature ranges for reporting the results of the analyses, the chromatograph is given a normal boiling point-retention time calibration. The n-alkanes, their boiling points, and data reporting ranges are given in the table below:

	<u>OSP, °C</u>	<u>Reporting Range, °C</u>	<u>Report As</u>
n-heptane	98	90-110	C7
n-octane	126	110-140	C8
n-nonane	151	140-160	C9
n-decane	174	150-180	C10
n-undecane	194	180-200	C11
n-dodecane	214	200-220	C12
n-tridecane	234	220-240	C13
n-tetradecane	252	240-260	C14
n-pentadecane	270	260-280	C15
n-hexadecane	298	280-300	C16

7.2.2 Preparation of standards: Preparing a mixture of the C7-C16 alkanes is required. There are two approaches: (1) use of a standards kit (e.g., Polyscience Kit) containing bottles of mixtures of selected n-alkanes which may be combined to produce a C7-C16 standard; or (2) use of bottles of the individual C7-C16 alkanes from which accurately known volumes may be taken and combined to give a C7-C16 mixture.

7.2.3 Procedure for retention time calibration: This calibration is performed at the start of an analytical program; the mixture is chromatographed at the start of each day. To attain the required retention time precision, both the carrier gas flow rate and the temperature program specifications must be observed. Details of the procedure depend on the instrument being used. The general procedure is as follows:

7.2.3.1 Set the programmer upper limit at 250°C. If this setting does not produce a column temperature of 250°C, find the correct setting.

7.2.3.2 Set the programmer lower limit at 30°C.

7.2.3.3 Verify that the instrument and samples are at room temperature.

7.2.3.4 Inject 1 µL of the n-alkane mixture.

7.2.3.5 Start the integrator and recorder.

7.2.3.6 Allow the instrument to run isothermally at room temperature for five min.

7.2.3.7 Shut the oven door.

7.2.3.8 Change the mode to Automatic and start the temperature program.

7.2.3.9 Repeat Steps 1-9 a sufficient number of times so that the relative standard deviation of the retention times for each peak is <5%.

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### 7.3 Response calibration:

7.3.1 For the purposes of a Level 1 analysis, response-quantity calibration with n-decane is adequate. A 10- $\mu$ L volume of n-decane is injected into a tared 10 mL volumetric flask. The weight injected is obtained and the flask is diluted to the mark with n-pentane. This standard contains about 730 ng n-decane per  $\mu$ L n-pentane. The exact concentration depends on temperature, so that a weight is required. Two serial tenfold dilutions are made from this standard, giving standards at about 730, 73, and 7.3 ng n-decane per  $\mu$ L n-pentane, respectively.

7.3.2 Procedure for response calibration: This calibration is performed at the start of an analytical program and monthly thereafter. The most concentrated standard is injected once each day. Any change in calibration necessitates a full calibration with new standards. Standards are stored in the refrigerator locker and are made up monthly.

7.3.2.1 Verify that the instrument is set up properly.

7.3.2.2 Set electrometer at  $1 \times 10^{-10}$  A/mV.

7.3.2.3 Inject 1  $\mu$ L of the highest concentration standard.

7.3.2.4 Run standard temperature program as specified above.

7.3.2.5 Clean syringe.

7.3.2.6 Make repeated injections of all three standards until the relative standard deviations of the areas of each standard are  $\leq 5\%$ .

### 7.4 Sample analysis procedure:

7.4.1 The following apparatus is required:

7.4.1.1 Gas chromatograph set up and working.

7.4.1.2 Recorder, integrator working.

7.4.1.3 Syringe and syringe cleaning apparatus.

7.4.1.4 Parameters: Electrometer setting is  $1 \times 10^{-10}$  A/mV; recorder is set at 0.5 in./min and 1 mV full-scale.

7.4.2 Steps in the procedure are:

7.4.2.1 Label chromatogram with the data, sample number, etc.

7.4.2.2 Inject sample.

7.4.2.3 Start integrator and recorder.

7.4.2.4 After isothermal operation for 5 min, begin temperature program.

7.4.2.5 Clean syringe.

7.4.2.6 Return sample; obtain new sample.

7.4.2.7 When analysis is finished, allow instrument to cool. Turn chromatogram and integrator output and data sheet over to data analyst.

7.5 Syringe cleaning procedure:

7.5.1 Remove plunger from syringe.

7.5.2 Insert syringe into cleaner; turn on aspirator.

7.5.3 Fill pipet with pentane; run pentane through syringe.

7.5.4 Repeat with methylene chloride from a separate pipet.

7.5.5 Flush plunger with pentane followed by methylene chloride.

7.5.6 Repeat with methylene chloride.

7.6 Sample analysis decision criterion: The data from the TCO analyses of organic extract and rinse concentrates are first used to calculate the total concentration of C7-C16 hydrocarbon-equivalents (Paragraph 7.7.3) in the sample with respect to the volume of air actually sampled, i.e.,  $\mu\text{g}/\text{m}^3$ . On this basis, a decision is made both on whether to calculate the quantity of each n-alkane equivalent present and on which analytical procedural pathway will be followed. If the total organic content is great enough to warrant continuing the analysis --  $>500 \mu\text{g}/\text{m}^3$  -- a TCO of less than  $75 \mu\text{g}/\text{m}^3$  will require only LC fractionation and gravimetric determinations and IR spectra to be obtained on each fraction. If the TCO is greater than  $75 \mu\text{g}/\text{m}^3$ , then the first seven LC fractions of each sample will be reanalyzed using this same gas chromatographic technique.

7.7 Calculations:

7.7.1 Boiling Point - Retention Time Calibration: The required data for this calibration are on the chromatogram and on the data sheet. The data reduction is performed as follows:

7.7.1.1 Average the retention times and calculate relative standard deviations for each n-hydrocarbon.

7.7.1.2 Plot average retention times as abscissae versus normal boiling points as ordinates.

7.7.1.3 Draw in calibration curve.

7.7.1.4 Locate and record retention times corresponding to boiling ranges 90-100, 110-140, 140-160, 160-180, 180-200, 200-220, 220-240, 240-260, 260-280, 280-300°C.

7.7.2 Response-amount calibration: The required data for this calibration are on the chromatogram and on the data sheet. The data reduction is performed as follows:

7.7.2.1 Average the area responses of each standard and calculate relative standard deviations.

7.7.2.2 Plot response (uV-sec) as ordinate versus ng/uL as abscissa.

7.7.2.3 Draw in the curve. Perform least squares regression and obtain slope (uV-sec·uL/ng).

7.7.3 Total C7-C16 hydrocarbons analysis: The required data for this calculation are on the chromatogram and on the data sheet. The data reduction is performed as follows:

7.7.3.1 Sum the areas of all peaks within the retention time range of interest.

7.7.3.2 Convert this area (uV-sec) to ng/uL by dividing by the weight response for n-decane (uV-sec·uL/ng).

7.7.3.3 Multiply this weight by the total concentrate volume (10 mL) to get the weight of the C7-C16 hydrocarbons in the sample.

7.7.3.4 Using the volume of gas sampled or the total weight of sample acquired, convert the result of Step 7.7.3.3 above to  $\mu\text{g}/\text{m}^3$ .

7.7.3.5 If the value of total C7-C16 hydrocarbons from Step 7.7.3.4 above exceeds 75  $\mu\text{g}/\text{m}^3$ , calculate individual hydrocarbon concentrations in accordance with the instructions in Paragraph 7.7.5.5 below.

7.7.4 Individual C7-C16 n-Alkane Equivalent Analysis: The required data from the analyses are on the chromatogram and on the data sheet. The data reduction is performed as follows:

7.7.4.1 Sum the areas of peaks in the proper retention time ranges.

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7.7.4.2 Convert areas ( $\mu\text{V}\cdot\text{sec}$ ) to  $\text{ng}/\mu\text{L}$  by dividing by the proper weight response ( $\mu\text{V}\cdot\text{sec}\cdot\mu\text{L}/\text{ng}$ ).

7.7.4.3 Multiply each weight by total concentrate volume (10  $\mu\text{L}$ ) to get weight of species in each range of the sample.

7.7.4.4 Using the volume of gas sampled on the total weight of sample acquired, convert the result of Step 7.7.4.3 above to  $\mu\text{g}/\text{m}^3$ .

## 8.0 QUALITY CONTROL

8.1 Appropriate QC is found in the pertinent procedures throughout the method.

## 9.0 METHOD PERFORMANCE

9.1 Even relatively comprehensive error propagation analysis is beyond the scope of this procedure. With reasonable care, peak area reproducibility of a standard should be of the order of 1% RSD. The relative standard deviation of the sum of all peaks in a fairly complex waste might be of the order of 5-10%. Accuracy is more difficult to assess. With good analytical technique, accuracy and precision should be of the order of 10-20%.

## 10.0 REFERENCES

1. Emissions Assessment of Conventional Stationary Combustion Systems: Methods and Procedure Manual for Sampling and Analysis, Interagency Energy/Environmental R&D Program, Industrial Environmental Research Laboratory, Research Triangle Park, NC 27711, EPA-600/7-79-C29a, January 1979.

July 1980  
Revision: Final

**EPA METHOD 5**  
**DETERMINATION OF PARTICULATE EMISSIONS**  
**FROM STATIONARY SOURCES**

1311R2

### METHOD 3—DETERMINATION OF PARTICULATE EMISSIONS FROM STATIONARY SOURCES

#### 1. Principle and Applicability

1.1 Principle. Particulate matter is withdrawn isokinetically from the source and collected on a glass fiber filter maintained at a temperature in the range of  $120 \pm 14^\circ\text{C}$  ( $248 \pm 25^\circ\text{F}$ ) or such other temperature as specified by an applicable subpart of the standards or approved by Administrator, U.S. Environmental Protection Agency, for a particular application. The particulate mass, which includes any material that condenses at or above the filtration temperature, is determined gravimetrically after removal of uncombined water.

1.2 Applicability. This method is applicable for the determination of particulate emissions from stationary sources.

#### 2. Apparatus

2.1 Sampling Train. A schematic of the sampling train used in this method is shown in Figure 5-1. Complete construction details are given in APTD-0581 (Citation 2 in Bibliography); commercial models of this train are also available. For changes from APTD-0581 and for allowable modifications of the train shown in Figure 5-1, see the following subsections.

The operating and maintenance procedures for the sampling train are described in APTD-0576 (Citation 3 in Bibliography). Since correct usage is important in obtaining valid results, all users should read APTD-0576 and adopt the operating and maintenance procedures outlined in it, unless otherwise specified herein. The sampling train consists of the following components:

2.1.1 Probe Nozzle. Stainless steel (316) or glass with sharp, tapered leading edge. The angle of taper shall be  $<30^\circ$  and the taper shall be on the outside to preserve a constant internal diameter. The probe nozzle shall be of the button-hook or elbow design, unless otherwise specified by the Administrator. If made of stainless steel, the nozzle shall be constructed from seamless tubing; other materials of construction may be used, subject to the approval of the Administrator.

A range of nozzle sizes suitable for isokinetic sampling should be available, e.g., 0.32 to 1.27 cm ( $1/8$  to  $1/2$  in.)—or larger if higher volume sampling trains are used—inside diameter (ID) nozzles in increments of 0.16 cm ( $1/16$  in.). Each nozzle shall be calibrated according to the procedures outlined in Section 5.

2.1.2 Probe Liner. Borosilicate or quartz glass tubing with a heating system capable of maintaining a gas temperature at the exit end during sampling of  $120 \pm 14^\circ\text{C}$  ( $248 \pm 25^\circ\text{F}$ ) or such other temperature as specified by an applicable subpart of the standards or approved by the Administrator for a particular application. (The tester may opt to operate the equipment at a temperature lower than that specified.) Since the actual temperature at the outlet of the probe is not usually monitored during sampling, probes constructed according to APTD-0581 and utilizing the calibration curves of APTD-0576 (or calibrated according to the procedure outlined in APTD-0576) will be considered acceptable.

Either borosilicate or quartz glass probe liners may be used for stack temperatures up to about  $480^\circ\text{C}$  ( $900^\circ\text{F}$ ). Quartz liners shall be used for temperatures between  $430$  and  $900^\circ\text{C}$  ( $800$  and  $1,650^\circ\text{F}$ ). Both types of liners may be used at higher temperatures than specified for short periods of time, subject to the approval of the Administrator. The softening temperature for borosilicate is  $820^\circ\text{C}$  ( $1,508^\circ\text{F}$ ), and for quartz it is  $1,500^\circ\text{C}$  ( $2,732^\circ\text{F}$ ).

Whenever practical, every effort should be made to use borosilicate or quartz glass probe liners. Alternatively, metal liners (e.g., 316 stainless steel, Incoloy 825,<sup>1</sup> or other corrosion resistant metals) made of seamless tubing may be used, subject to the approval of the Administrator.

2.1.3 Pitot Tube. Type S, as described in Section 2.1 of Method 2, or other device approved by the Administrator. The pitot tube shall be attached to the probe (as shown in Figure 5-1) to allow constant monitoring of the stack gas velocity. The impact (high pressure) opening plane of the pitot tube shall be even with or above the nozzle entry plane (see Method 2, Figure 2-6b) during sampling. The Type S pitot tube assembly shall have a known coefficient, determined as outlined in Section 4 of Method 2.

<sup>1</sup>Mention of trade names or specific products does not constitute endorsement by the Environmental Protection Agency.

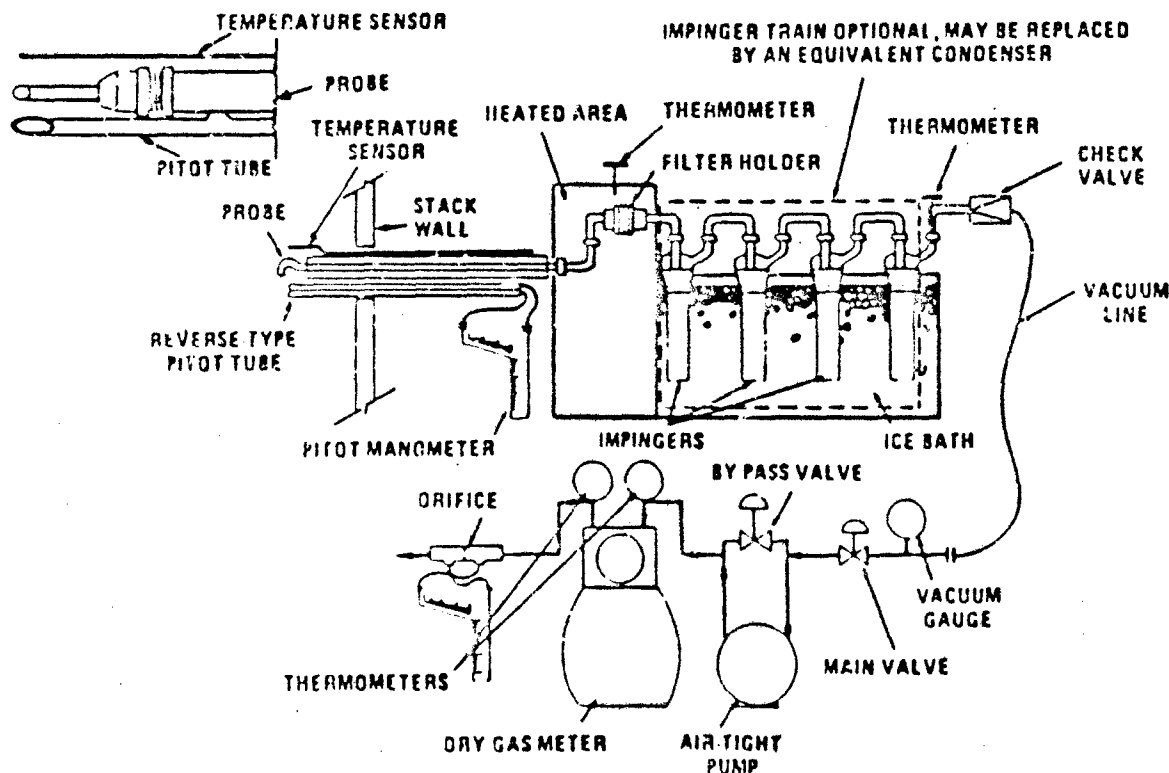


Figure 5-1. Particulate sampling train.



2.1.4 **Differential Pressure Gauge.** Inclined manometer or equivalent device (two), as described in Section 2.2 of Method 2. One manometer shall be used for velocity (30) readings, and the other, for orifice differential pressure readings.

2.1.5 **Filter Holder.** Borosilicate glass, with a glass frit filter support and a silicone rubber gasket. Other materials of construction (e.g., stainless steel, Teflon, Viton) may be used, subject to approval of the Administrator. The holder design shall provide a positive seal against leakage from the outside or around the filter. The holder shall be attached immediately at the outlet of the probe for cyclone, if used).

2.1.6 **Filter Heating System.** Any heating system capable of maintaining a temperature around the filter holder during sampling of 120±14° C (248±25° F), or such other temperature as specified by an applicable subpart of the standards or approved by the Administrator for a particular application. Alternatively, the tester may opt to operate the equipment at a temperature lower than that specified. A temperature gauge capable of measuring temperature to within 3° C (5.4° F) shall be installed so that the temperature around the filter holder can be regulated and monitored during sampling. Heating systems other than the one shown in APTD-0581 may be used.

2.1.7 **Condenser.** The following system shall be used to determine the stack gas moisture content: Four impingers connected in series with leak-free ground glass fittings or any similar leak-free non-contaminating fittings. The first, third, and fourth impingers shall be of the Greenburg-Smith design, modified by replacing the tip with .3 cm (1/8 in.) ID glass tube extending to about 1.3 cm (1/2 in.) from the bottom of the flask. The second impinger shall be of the Greenburg-Smith design with the standard tip. Modifications (e.g., using flexible connections between the impingers, using materials other than glass, or using flexible vacuum lines to connect the filter holder to the condenser) may be used, subject to the approval of the Administrator. The first and second impingers shall contain known quantities of water (Section 4.1.3), the third shall be empty, and the fourth shall contain a known weight of silica gel, or equivalent desiccant. A thermometer, capable of measuring temperature to within 1° C (2° F) shall be placed at the outlet of the fourth impinger for monitoring purposes.

Alternatively, any system that cools the sample gas stream and allows measurement of the water condensed and moisture leaving the condenser, each to within 1 ml or 1 g may be used, subject to the approval of the Administrator. Acceptable means are to measure the condensed water either gravimetrically or volumetrically and to measure the moisture leaving the condenser by: (1) monitoring the temperature and pressure at the exit of the condenser and using Dalton's law of partial pressures; or (2) passing the sample gas stream through a tared silica gel or equivalent desiccant trap with exit lines kept below 20° C (68° F) and determining the weight gain.

If means other than silica gel are used to determine the amount of moisture leaving the condenser, it is recommended that silica gel (or equivalent) still be used between the condenser system and pump to prevent moisture condensation in the pump and metering devices and to avoid the need to make corrections for moisture in the metered volume.

**NOTE:** If a determination of the particulate matter collected in the impingers is required in addition to moisture content, the impinger system described above shall be used, without modification. Individual States or control agencies requiring this information shall be contacted as to the sample recovery and analysis of the impinger contents.

2.1.8 **Metering System.** Vacuum gauge, leak-free pump, thermometers capable of measuring temperature to within 3° C (5.4° F), dry gas meter capable of measuring volume to within 2 percent, and related equipment, as shown in Figure 5-1. Other metering systems capable of maintaining sampling rates within 10 percent of isokinetic and of determining sample volumes to within 2 percent may be used, subject to the approval of the Administrator. When the metering system is used in conjunction with a pitot tube, the system shall enable checks of isokinetic rates.

Sampling trains utilizing metering systems designed for higher flow rates than that described in APTD-0581 or APDT-0578 may be used provided that the specifications of this method are met.

2.1.9 **Barometer.** Mercury aneroid, or other barometer capable of measuring atmospheric pressure to within 2.5 mm Hg (0.1 in. Hg). In many cases the barometric reading may be obtained from a nearby national weather service station, in which case the station value (which is the absolute barometric pressure) shall be requested and an adjustment for elevation differences between the weather station and sampling point shall be applied at a rate of minus 2.5 mm Hg (0.1 in. Hg) per 30 m (100 ft) elevation increase or vice versa for elevation decrease.

2.1.10 **Gas Density Determination Equipment.** Temperature sensor and pressure gauge, as described in Sections 2.3 and 2.4 of Method 2, and gas analyzer, if necessary, as described in Method 3. The temperature sensor shall, preferably, be permanently attached to the pitot tube or sampling probe in a fixed configuration, such that the tip of the sensor extends beyond the leading edge of the probe sheath and does not touch any metal. Alternatively, the sensor may be attached just prior to use in the field. Note, however, that if the temperature sensor is attached in the field, the sensor must be placed in an interference-free arrangement with respect to the Type S pitot tube openings (see Method 2, Figure 2-7). As a second alternative, if a difference of not more than 1 percent in the average velocity measurement is to be introduced, the temperature gauge need not be attached to the probe or pitot tube. (This alternative is subject to the approval of the Administrator.)

2.2 **Sample Recovery.** The following items are needed.

2.2.1 **Probe-Liner and Probe-Nozzle Brushes.** Nylon bristle brushes with stainless steel wire handles. The probe brush shall have extensions (at least as long as the probe) of stainless steel, Nylon, Teflon, or similarly inert material. The brushes shall be properly sized and shaped to brush out the probe liner and nozzle.

2.2.2 **Wash Bottles—Two.** Glass wash bottles are recommended; polyethylene wash bottles may be used at the option of the tester. It is recommended that acetone not be stored in polyethylene bottles for longer than a month.

2.2.3 **Glass Sample Storage Containers.** Chemically resistant, borosilicate glass bottles, for acetone washes, 500 ml or 1000 ml. Screw cap liners shall either be rubber-backed Teflon or shall be constructed so as to be leak-free and resistant to chemical attack by acetone. (Narrow mouth glass bottles have been found to be less prone to leakage.) Alternatively, polyethylene bottles may be used.

2.2.4 **Petri Dishes.** For filter samples, glass or polyethylene, unless otherwise specified by the Administrator.

2.2.5 **Graduated Cylinder and/or Balance.** To measure condensed water to within 1 ml or 1 g. Graduated cylinders shall have subdivisions no greater than 2 ml. Most laboratory balances are capable of weighing to the nearest 0.5 g or less. Any of these balances is suitable for use here and in Section 2.3.4.

2.2.6 **Plastic Storage Containers.** Airtight containers to store silica gel.

2.2.7 **Funnel and Rubber Policeman.** To aid in transfer of silica gel to container; not used in transfer of silica gel to container; not used in sample recovery.

2.2.8 **Funnel.** Glass or polyethylene, to aid in sample recovery.

2.3 **Analysis.** For analysis, the following equipment is needed.

2.3.1 **Glass Weighing Dishes.**

2.3.2 **Desiccator.**

2.3.3 **Analytical Balance.** To measure to within 0.1 mg.

2.3.4 **Balance.** To measure to within 0.5 g.

2.3.5 **Beakers.** 250 ml.

2.3.6 **Hygrometer.** To measure the relative humidity of the laboratory environment.

2.3.7 **Temperature Gauge.** To measure the temperature of the laboratory environment.

### 3. Reagents

3.1 **Sampling.** The reagents used in sampling are as follows:

3.1.1 **Filters.** Glass fiber filters, without organic binder, exhibiting at least 99.95 percent efficiency (<0.05 percent penetration) on 0.3-micron diethyl phthalate smoke particles. The filter efficiency test shall be conducted in accordance with ASTM standard method D2946-71 (Reapproved 1978) (Incorporated by reference—see § 60.17). Test data from the supplier's quality control program are sufficient for this purpose. In sources containing SO<sub>2</sub> or SO<sub>3</sub>, the filter material must be of a type that is unreactive to SO<sub>2</sub> or SO<sub>3</sub>. Citation 16 in Section 7 Bibliography, may be used to select the appropriate filter.

3.1.2 **Silica Gel.** Indicating type, # 16 mesh, if previously used, dry at 175° C (350° F) for 2 hours. New silica gel may be used as received. Alternatively, other types of desiccants (equivalent or better) may be used, subject to the approval of the Administrator.

3.1.3 **Water.** When analysis of the material caught in the impingers is required, distilled water shall be used. Run blanks prior to field use to eliminate a high blank on test samples.

3.1.4 **Crushed Ice.**

3.1.5 **Stopcock Grease.** Acetone-insoluble, heat-stable silicone grease. This is not necessary if screw-on connectors with Teflon sleeves, or similar, are used. Alternatively, other types of stopcock grease may be used, subject to the approval of the Administrator.

For each run, record the data required on a data sheet such as the one shown in Figure 3-2. Be sure to record the initial dry gas meter reading. Record the dry gas meter readings at the beginning and end of each sampling time increment, when changes in flow rates are made, before and after each leak-check, and when sampling is halted.

When the stack is under significant negative pressure (height of impinging steam), take care to close the coarse adjust valve before inserting the probe into the stack to prevent water from backing into the filter holder. If necessary, the pump may be turned on with the coarse adjust valve closed.

A single train shall be used for the entire sample run, except in cases where simultaneous aerosol sampling is required in two or more separate ducts or at two or more different locations within the same duct, or, in case where equipment failure necessitates change of trains. In all other situations, the use of two or more trains will be subject to the approval of the Administrator.

Plant Location Operator Date Run No. Sample test No. Inlet test No. Motor JPH C factor Plant name and location, Co.	Ambient temperature Barometric pressure Assumed moisture, % Probe length, in. (ft.) Nozzle identification No. Average calibrated nozzle diameter, mm (in.) Probe heater setting Loss rate, in./min. (cm) Probe inlet material Static pressure, mm. Hg (in. Hg) Filter No.
--	---

SOURCE: U.S. STEEL CORP. SYSTEM

[illegible]

**3.2 Sample Recovery.** Acetone-reagent grade, 0.001 percent residue, in glass bottles is required. Acetone from metal containers generally has a high residue blank and should not be used. Sometimes, suppliers transfer acetone to glass bottles from metal containers; thus, acetone blanks shall be run prior to field use and only acetone with low blank values (<0.001 percent) shall be used. In no case shall a blank value of greater than 0.001 percent of the weight of acetone used be subtracted from the sample weight.

**3.3 Analysis.** Two reagents are required for the analysis:

**3.3.1 Acetone.** Same as 3.2.

**3.3.2 Desiccant.** Anhydrous calcium sulfate, indicating type. Alternatively, other types of desiccants may be used, subject to the approval of the Administrator.

#### **4. Procedure**

**4.1 Sampling.** The complexity of this method is such that, in order to obtain reliable results, testers should be trained and experienced with the test procedures.

**4.1.1 Pretest Preparation.** It is suggested that sampling equipment be maintained according to the procedures described in APTD-0578.

Weigh several 200 to 300 g portions of silica gel in air-tight containers to the nearest 0.5 g. Record the total weight of the silica gel plus container, on each container. As an alternative, the silica gel need not be preweighed, but may be weighed directly in the impinger or sampling holder just prior to train assembly.

Check filters visually against light for irregularities and flaws or pinhole leaks. Label filters of the proper diameter on the back side near the edge using numbering machine ink. As an alternative, label the shipping containers (glass or plastic petri dishes) and keep the filters in these containers at all times except during sampling and weighing.

Desiccate the filters at  $23 \pm 5^\circ\text{C}$  ( $68 \pm 10^\circ\text{F}$ ) and ambient pressure for at least 24 hours and weigh at intervals of at least 6 hours to a constant weight, i.e., 0.5 mg change from previous weighing; record results to the nearest 0.1 mg. During each weighing the filter must not be exposed to the laboratory atmosphere for a period greater than 2 minutes and a relative humidity above 50 percent. Alternatively (unless otherwise specified by the Administrator), the filters may be oven dried at  $108^\circ\text{C}$  ( $230^\circ\text{F}$ ) for 3 to 3 hours, desiccated for 2 hours, and weighed. Procedures other than those described, which account for relative humidity effects, may be used, subject to the approval of the Administrator.

**4.1.2 Preliminary Determinations.** Select the sampling site and the minimum number of sampling points according to Method 1 or as specified by the Administrator. Determine the stack pressure, temperature, and the range of velocity heads using Method 2. It is recommended that a leak-check of the pilot lines (see Method 2, Section 3.1) be performed. Determine the moisture content using Approximation Method 4 or its alternatives for the purpose of making isokinetic sampling rate settings. Determine the stack

gas dry molecular weight, as described in Method 2, Section 3.6; if Integrated Method 3 sampling is used for molecular weight determination, the integrated bag sample shall be taken simultaneously with, and for the same total length of time as, the particulate sample run.

Select a nozzle size based on the range of velocity heads, such that it is not necessary to change the nozzle size in order to maintain isokinetic sampling rates. During the run, do not change the nozzle size. Ensure that the proper differential pressure gauge is chosen for the range of velocity heads encountered (see Section 2.2 of Method 2).

Select a suitable probe liner and probe length such that all traverse points can be sampled. For large stacks, consider sampling from opposite sides of the stack to reduce the length of probes.

Select a total sampling time greater than or equal to the minimum total sampling time specified in the test procedures for the specific industry such that (1) the sampling time per point is not less than 2 min (or some greater time interval as specified by the Administrator), and (2) the sample volume taken (corrected to standard conditions) will exceed the required minimum total gas sample volume. The latter is based on an approximate average sampling rate.

It is recommended that the number of minutes sampled at each point be an integer or an integer plus one-half minute, in order to avoid timekeeping errors. The sampling time at each point shall be the same.

In some circumstances, e.g., batch cycles, it may be necessary to sample for shorter times at the traverse points and to obtain smaller gas sample volumes. In these cases, the Administrator's approval must first be obtained.

**4.1.3 Preparation of Collection Train.** During preparation and assembly of the sampling train, keep all openings where contamination can occur covered until just prior to assembly or until sampling is about to begin.

Place 100 ml of water in each of the first two impingers, leave the third impinger empty, and transfer approximately 200 to 300 g of preweighed silica gel from its container to the fourth impinger. More silica gel may be used, but care should be taken to ensure that it is not entrained and carried out from the impinger during sampling. Place the container in a clean place for later use in the sample recovery. Alternatively, the weight of the silica gel plus impinger may be determined to the nearest 0.5 g and recorded.

Using a tweezer or clean disposable surgical gloves, place a labeled (identified) and weighed filter in the filter holder. Be sure that the filter is properly centered and the gasket properly placed so as to prevent the sample gas stream from circumventing the filter. Check the filter for tears after assembly is completed.

When glass liners are used, install the selected nozzle using a Viton A O-ring when stack temperatures are less than  $260^\circ\text{C}$  ( $500^\circ\text{F}$ ) and an asbestos string gasket when temperatures are higher. See APTD-0578 for details. Other connecting systems using either 316 stainless steel or Teflon ferrules may be used. When metal liners are used, install the nozzle as above or by a leak-free direct mechanical connection. Mark the probe with heat resistant tape or by some other method to denote the proper distance into the stack or duct for each sampling point.

Set up the train as in Figure 5-1, using (if necessary) a very light coat of silicone grease on all ground glass joints, greasing only the outer portion (see APTD-0578) to avoid possibility of contamination by the silicone grease. Subject to the approval of the Administrator, a glass cyclone may be used between the probe and filter holder when the total particulate catch is expected to exceed 100 mg or when water droplets are present in the stack gas.

Place crushed ice around the impingers.

#### **4.1.4 Leak-Check Procedures.**

**4.1.4.1 Pretest Leak-Check.** A pretest leak-check is recommended, but not required. If the tester opts to conduct the pretest leak-check, the following procedure shall be used.

After the sampling train has been assembled, turn on and set the filter and probe heating systems at the desired operating temperatures. Allow time for the temperatures to stabilize. If a Viton A O-ring or other leak-free connection is used in assembling the probe nozzle to the probe liner, leak-check the train at the sampling site by plugging the nozzle and pulling a 380 mm Hg (15 in. Hg) vacuum.

**Note:** A lower vacuum may be used, provided that it is not exceeded during the test.

If an asbestos string is used, do not connect the probe to the train during the leak-check. Instead, leak-check the train by first plugging the inlet to the filter holder (cyclone, if applicable) and pulling a 380 mm Hg (15 in. Hg) vacuum (see Note immediately above). Then connect the probe to the train and leak-check at about 25 mm Hg (1 in. Hg) vacuum; alternatively, the probe may be leak-checked with the rest of the sampling train, in one step, at 380 mm Hg (15 in. Hg) vacuum. Leakage rates in excess of 4 percent of the average sampling rate or  $0.00057\text{ m}^3/\text{min}$  ( $0.02\text{ cfm}$ ), whichever is less, are unacceptable.

The following leak-check instructions for the sampling train described in APTD-0578 and APTD-0581 may be helpful. Start the pump with bypass valve fully open and coarse adjust valve, completely closed. Partially open the coarse adjust valve and slowly close the bypass valve until the desired vacuum is reached. Do not reverse direction of bypass valve; this will cause water to back up into the filter holder. If the desired vacuum is exceeded, either leak-check at this higher vacuum or end the leak-check as shown below and start over.

When the leak-check is completed, first slowly remove the plug from the inlet to the probe, filter holder, or cyclone (if applicable) and immediately turn off the vacuum pump. This prevents the water in the impingers from being forced backward into the filter holder and silica gel from being entrained backward into the third impinger.

**4.1.4.2 Leak-Checks During Sample Run.** If, during the sampling run, a component (e.g., filter assembly or impinger) change becomes necessary, a leak-check shall be conducted immediately before the change is made. The leak-check shall be done according to the procedure outlined in Section 4.1.4.1 above, except that it shall be done at a vacuum equal to or greater than the maximum value recorded up to that point in the test. If the leakage rate is found to be no greater than  $0.00057\text{ m}^3/\text{min}$  ( $0.02\text{ cfm}$ ) or 4 percent of the average sampling rate (whichever is less), the results are acceptable, and no correction will need to be applied to the total volume of dry gas metered.

Note that when two or more trains are used, separate analyses of the front-half and (if applicable) impinger catches from each train shall be performed, unless identical nozzle sizes were used on all trains, in which case, the front-half catches from the individual trains may be combined (as may the impinger catches) and one analysis of front-half catch and one analysis of impinger catch may be performed. Consult with the Administrator for details concerning the calculation of results when two or more trains are used.

At the end of the sample run, turn off the coarse adjust valve, remove the probe and nozzle from the stack, turn off the pump, record the final dry gas meter reading, and conduct a post-test leak-check, as outlined in Section 4.1.4.3. Also, leak-check the pilot lines as described in Method 2, Section 3.1; the lines must pass this leak-check, in order to validate the velocity head data.

4.1.6 Calculation of Percent Isokinetic. Calculate percent isokinetic (see Calculations, Section 6) to determine whether the run was valid or another test run should be made. If there was difficulty in maintaining isokinetic rates due to source conditions, consult with the Administrator for possible variance on the isokinetic rates.

4.2 Sample Recovery. Proper cleanup procedure begins as soon as the probe is removed from the stack at the end of the sampling period. Allow the probe to cool.

When the probe can be safely handled, wipe off all external particulate matter near the tip of the probe nozzle and place a cap over it to prevent losing or gaining particulate matter. Do not cap off the probe tip tightly while the sampling train is cooling down as this would create a vacuum in the filter holder, thus drawing water from the impingers into the filter holder.

Before moving the sample train to the cleanup site, remove the probe from the sample train, wipe off the silicone grease, and cap the open outlet of the probe. Be careful not to lose any condensate that might be present. Wipe off the silicone grease from the filter inlet where the probe was fastened and cap it. Remove the umbilical cord from the last impinger and cap the impinger. If a flexible line is used between the first impinger or condenser and the filter holder, disconnect the line at the filter holder and let any condensed water or liquid drain into the impingers or condenser. After wiping off the silicone grease, cap off the filter holder outlet and impinger inlet. Either ground-glass stoppers, plastic caps, or serum caps may be used to close these openings.

Transfer the probe and filter-impinger assembly to the cleanup area. This area should be clean and protected from the wind so that the chances of contaminating or losing the sample will be minimized.

Save a portion of the acetone used for cleanup as a blank. Take 200 ml of this acetone directly from the wash bottle being used and place it in a glass sample container labeled "acetone blank."

Inspect the train prior to and during disassembly and note any abnormal conditions. Treat the samples as follows:

Container No. 1. Carefully remove the filter from the filter holder and place it in its identified petri dish container. Use a pair of tweezers and/or clean disposable surgical gloves to handle the filter. If it is necessary to fold the filter, do so such that the particulate cake is inside the fold. Carefully transfer to the petri dish any particulate matter and/or filter fibers which adhere to the filter holder gasket, by using a dry Nylon

bristle crush and/or a sharp-edged blade. Seal the container.

Container No. 2. Taking care to see that dust on the outside of the probe or other exterior surfaces does not get into the sample, quantitatively recover particulate matter or any condensate from the probe nozzle, probe fitting, probe liner, and front half of the filter holder by washing these components with acetone and placing the wash in a glass container. Distilled water may be used instead of acetone when approved by the Administrator and shall be used when specified by the Administrator; in these cases, save a water blank and follow the Administrator's directions on analysis. Perform the acetone rinses as follows:

Carefully remove the probe nozzle and clean the inside surface by rinsing with acetone from a wash bottle and brushing with a Nylon bristle brush. Brush until the acetone rinse shows no visible particles, after which make a final rinse of the inside surface with acetone.

Brush and rinse the inside parts of the Swagelok fitting with acetone in a similar way until no visible particles remain.

Rinse the probe liner with acetone by tilting and rotating the probe while squirting acetone into its upper end so that all inside surfaces will be wetted with acetone. Let the acetone drain from the lower end into the sample container. A funnel (glass or polyethylene) may be used to aid in transferring liquid wastes to the container. Follow the acetone rinse with a probe brush. Hold the probe in an inclined position, squirt acetone into the upper end as the probe brush is being pushed with a twisting action through the probe; hold a sample container underneath the lower end of the probe, and catch any acetone and particulate matter which is brushed from the probe. Run the brush through the probe three times or more until no visible particulate matter is carried out with the acetone or until none remains in the probe liner on visual inspection. With stainless steel or other metal probes, run the brush through in the above prescribed manner at least six times since metal probes have small crevices in which particulate matter can be entrapped. Rinse the brush with acetone, and quantitatively collect these washings in the sample container. After the brushing, make a final acetone rinse of the probe as described above.

It is recommended that two people clean the probe to minimize sample losses. Between sampling runs, keep brushes clean and protected from contamination.

After ensuring that all joints have been wiped clean of silicone grease, clean the inside of the front half of the filter holder by rubbing the surfaces with a Nylon bristle brush and rinsing with acetone. Rinse each surface three times or more if needed to remove visible particulate. Make a final rinse of the brush and filter holder. Carefully rinse out the glass cyclone, also (if applicable). After all acetone washings and particulate matter have been collected in the sample container, tighten the lid on the sample container so that acetone will not leak out when it is shipped to the laboratory. Mark the height of the fluid level to determine whether or not leakage occurred during transport. Label the container to clearly identify its contents.

Container No. 3. Note the color of the indicating silica gel to determine if it has been completely spent and make a notation of its condition. Transfer the silica gel from the fourth impinger to its original container and seal. A funnel may make it easier to pour the silica gel without spilling. A rubber policeman may be used as an aid in removing the silica gel from the impinger; it is not necessary to remove the small amount of dust particles that may adhere to the impinger wall and are difficult to remove. Since the gain in weight is to be used for moisture calculations, do not use any water or other liquids to transfer the silica gel. If a balance is available in the field, follow the procedure for container No. 3 in Section 4.3.

Impinger Water. Treat the impingers as follows: Make a notation of any color or film in the liquid catch. Measure the liquid which is in the first three impingers to within  $\pm 1$  ml by using a graduated cylinder or by weighing it to within  $\pm 0.5$  g by using a balance (if one is available). Record the volume or weight of liquid present. This information is required to calculate the moisture content of the effluent gas.

Discard the liquid after measuring and recording the volume or weight, unless analysis of the impinger catch is required (see Note, Section 2.1.7).

If a different type of condenser is used, measure the amount of moisture condensed either volumetrically or gravimetrically.

Whenever possible, containers should be shipped in such a way that they remain upright at all times.

4.3 Analysis. Record the data required on a sheet such as the one shown in Figure 3-3. Handle each sample container as follows:

FIGURE 3-3—ANALYTICAL DATA

Plant \_\_\_\_\_  
Date \_\_\_\_\_  
Run No. \_\_\_\_\_  
Filter No. \_\_\_\_\_  
Amount liquid lost during transport \_\_\_\_\_  
Acetone blank volume, ml \_\_\_\_\_  
Acetone wash volume, ml \_\_\_\_\_  
Acetone blank concentration, mg/mg (equation 3-4) \_\_\_\_\_  
Acetone wash blank, mg (equation 3-3) \_\_\_\_\_

Container number	Weight of particulate collected, mg		
	First weight	Tare weight	Weight gain
1			
2			
Total			
Loss acetone blank			
Weight of particulate matter			

	Volume of liquid water collected	
	Impinger volume, ml	Silica gel weight, g
First		
Initial		
Loss - if collected		
Total volume collected		g ml

\*Convert weight of water to volume by dividing total weight increase by density of water (1 g/ml).

Increase, g  
(1 g/ml) = Volume water, ml

Container No. 1. Leave the contents in the shipping container or transfer the filter and any loose particulate from the sample container to a tared glass weighing vial. Desiccate for 24 hours in a desiccator containing anhydrous calcium sulfate. Weigh to a constant weight and report the results to the nearest 0.1 mg. For purposes of this Section, 4.3, the term "constant weight" means a difference of no more than 0.5 mg or 1 percent of total weight less tare weight, whichever is greater, between two consecutive weighings, with no less than 8 hours of desiccation time between weighings.

Alternatively, the sample may be oven dried at 105° C (220° F) for 2 to 3 hours, cooled in the desiccator, and weighed to a constant weight, unless otherwise specified by the Administrator. The tester may also opt to oven dry the sample at 105° C (220° F) for 2 to 3 hours, weigh the sample, and use this weight as a final weight.

Container No. 2. Note the level of liquid in the container and confirm on the analysis sheet whether or not leakage occurred during transport. If a noticeable amount of leakage has occurred, either void the sample or use methods, subject to the approval of the Administrator, to correct the final results. Measure the liquid in this container either volumetrically to  $\pm 1$  ml or gravimetrically to  $\pm 0.5$  g. Transfer the contents to a tared 250-ml beaker and evaporate to dryness at ambient temperature and pressure. Desiccate for 24 hours and weigh to a constant weight. Report the results to the nearest 0.1 mg.

Container No. 3. Weigh the spent silica gel (or silica gel plus impinger) to the nearest 0.5 g using a balance. This step may be conducted in the field.

"Acetone Blank" Container. Measure acetone in this container either volumetrically or gravimetrically. Transfer the acetone to a tared 250-ml beaker and evaporate to dryness at ambient temperature and pressure. Desiccate for 24 hours and weigh to a constant weight. Report the results to the nearest 0.1 mg.

NOTE: At the option of the tester, the contents of Container No. 2 as well as the acetone blank container may be evaporated at temperatures higher than ambient. If evaporation is done at an elevated temperature, the temperature must be below the boiling point of the solvent; also, to prevent "bumping," the evaporation process must be closely supervised, and the contents of the beaker must be stirred occasionally to maintain an even temperature. Use extreme care, as acetone is highly flammable and has a low flash point.

4.4 Quality Control Procedures. The following quality control procedures are suggested to check the volume metering system calibration values at the field test site prior to sample collection. These procedures are optional for the tester.

4.4.1 Meter Orifice Check. Using the calibration data obtained during the calibration procedure described in Section 3.3, determine the  $\Delta H_0$  for the metering system orifice. The  $\Delta H_0$  is the orifice pressure differential in units of in. H<sub>2</sub>O that correlates to 0.75 cfm of air at 528°R and 29.92 in. Hg. The  $\Delta H_0$  is calculated as follows:

$$\Delta H_0 = 0.0219 \frac{T_a}{P_a} \frac{\theta^4}{YV_0}$$

Eq. 3-9

Where:

$\Delta H$  = Average pressure differential across the orifice meter, in. H<sub>2</sub>O.

$T_a$  = Absolute average dry gas meter temperature, °R.

$P_a$  = Barometric pressure, in. Hg.

$\theta$  = Total sampling time, min.

$Y$  = Dry gas meter calibration factor, dimensionless.

$V_0$  = Volume of gas sample as measured by dry gas meter, ccf.

$0.0319 = (0.0567 \text{ in. Hg}/^\circ\text{R}) \times (0.75 \text{ cfm})^4$

Before beginning the field test (a set of three runs usually constitutes a field test), operate the metering system (i.e., pump, volume meter, and orifice) at the  $\Delta H_0$  pressure differential for 10 minutes. Record the volume collected, the dry gas meter temperature, and the barometric pressure. Calculate a dry gas meter calibration check value,  $Y_c$ , as follows:

$$Y_c = \frac{10}{V_c} \left[ \frac{0.0319 T_a}{P_a} \right] \theta$$

Eq. 3-10

Where:

$Y_c$  = Dry gas meter calibration check value, dimensionless.

$10$  = 10 minutes of run time.

Compare the  $Y_c$  value with the dry gas meter calibration factor  $Y$  to determine that:

$0.97Y < Y_c < 1.03Y$

If the  $Y_c$  value is not within this range, the volume metering system should be investigated before beginning the test.

4.4.2 Calibration Critical Orifice. A

calibrated critical orifice, calibrated against a wet test meter or spirometer and designed to be inserted at the inlet of the sampling meter box, may be used as a quality control check by following the procedure of Section 7.2.

5. Calibration

Maintain a laboratory log of all calibrations.

5.1 Probe Nipple. Probe nipples shall be calibrated before their initial use in the field. Using a micrometer, measure the inside diameter of the nipple to the nearest 0.025 mm (0.001 in.). Make three separate measurements using different diameters each time, and obtain the average of the measurements. The difference between the high and low numbers shall not exceed 0.1 mm (0.004 in.). When nipples become nicked, dented, or corroded, they shall be reshaped, sharpened, and recalibrated before use. Each nipple shall be permanently and uniquely identified.

5.2 Pitot Tube. The Type S pitot tube assembly shall be calibrated according to the procedure outlined in Section 4 of Method 2.

5.3 Metering System. Before its initial use in the field, the metering system shall be calibrated according to the procedure outlined in APTD-0378. Instead of physically adjusting the dry gas meter dial readings to correspond to the wet test meter readings, calibration factors may be used to mathematically correct the gas meter dial readings to the proper values. Before calibrating the metering system, it is suggested that a leak-check be conducted. For metering systems having diaphragm pumps, the normal leak-check procedure will not detect leakages within the pump, for these cases

the following leak-check procedure is suggested: make a 10-minute calibration run at 0.0057 m<sup>3</sup>/min (0.02 cfm); at the end of the run, take the difference of the measure wet test meter and dry gas meter volume, divide the difference by 10, to get the leak rate. The leak rate should not exceed 0.00057 m<sup>3</sup>/min (0.02 cfm).

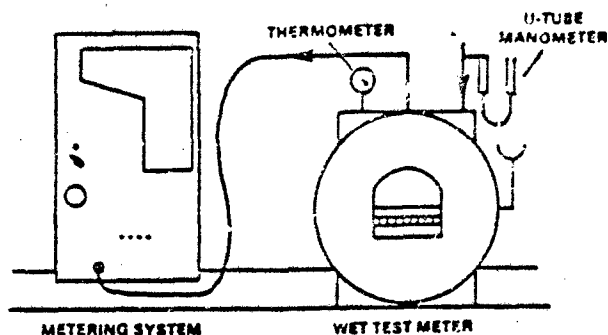
After each field use, the calibration of the metering system shall be checked by performing three calibration runs at a single intermediate orifice setting (based on the previous field test). With the vacuum set at the maximum value reached during the test series. To adjust the vacuum, insert a valve between the wet test meter and the inlet of the metering system. Calculate the average value of the calibration factor. If the calibration has changed by more than 5 percent, recalibrate the meter over the full range of orifice settings, as outlined in APTD-0378.

Alternative procedures, e.g., using the orifice meter coefficients, maybe used, subject to the approval of the Administrator.

NOTE: If the dry gas meter coefficient values obtained before and after a test series differ by more than 5 percent, the test series shall either be voided, or calculations for test series shall be performed using whichever meter coefficient value (i.e., before or after) gives the lower value of total sample volume.

5.3.1 Calibration Prior to Use. Before its initial use in the field, the metering system shall be calibrated as follows: Connect the metering system inlet to the outlet of a wet test meter that is accurate to within 1 percent. Refer to Figure 3.8. The wet test meter should have a capacity of 30 liters/rev (1 ft<sup>3</sup>/rev). A spirometer of 400 liters (14 ft<sup>3</sup>) or more capacity, or equivalent, may be used for this calibration, although a wet test meter is usually more practical. The wet test meter should be periodically calibrated with a spirometer or a liquid displacement meter to ensure the accuracy of the wet test meter. Spirometers or wet test meters of other sizes may be used, provided that the specified accuracies of the procedure are maintained. Run the metering system pump for about 15 minutes with the orifice manometer indicating a median reading as expected in field use to allow the pump to warm up and to permit the interior surface of the wet test meter to be thoroughly wetted. Then, at each of a minimum of three orifice manometer settings, pass an exact quantity of gas through the wet test meter and note the gas volume indicated by the dry gas meter. Also note the barometric pressure, and the temperatures of the wet test meter, the inlet of the dry gas meter, and the outlet of the dry gas meter. Select the highest and lowest orifice settings to bracket the expected field operating range of the orifice. Use a minimum volume of 0.15 m<sup>3</sup> (5 cf) at all orifice settings. Record all the data on a form similar to Figure 3.8, and calculate  $Y$ , the dry gas meter calibration factor, and  $\Delta H_0$ , the orifice calibration factor, at each orifice setting as shown on Figure 3.8. Allowable tolerances for individual  $Y$  and  $\Delta H_0$  values are given in Figure 3.8. Use the average of the  $Y$  values in the calculations in Section 6.

**5.6 Leak Check of Metering System** Shown in Figure 5-1. That portion of the sampling train from the pump to the orifice meter should be leak checked prior to initial use and after each shipment. Leakage after the pump will result in less volume being recorded than is actually sampled. The follow-



**Figure 5.5 Equipment arrangement for metering system calibration.**

Barometric pressure,  $P_b$  = \_\_\_\_\_ in. Hg[illegible]

### Calculations

	V	$\Delta H_g$
$\Delta H$ ft. H <sub>2</sub> O	$\frac{V_w P_2 (t_w + 460)}{\frac{\Delta H}{P_2 (t_w + 460)}}$	$\frac{9.0317 \Delta H}{P_2 (t_w + 460)} \left[ \frac{(t_w + 460)^2}{V_w} \right]^2$
Average		

Y = Ratio of reading of wet test meter to dry test meter; tolerance for individual values  $\pm 0.02$  from average.

$\Delta H_g$  = Orifice pressure differential that equates to 0.75 cm of air @ 68°F and 29.92 inches of mercury, in.  $H_2O$ ; tolerance for individual values  $\pm 0.20$  from average.

Figure 5.6. Example data sheet for calibration of metering system (English units).

ing procedure is suggested (see Figure 5-4): Close the main valve on the meter box. Insert a one-hole rubber stopper with rubber tubing attached into the orifice exhaust pipe. Disconnect and vent the low side of the orifice manometer. Close off the low side orifice tap. Pressurize the system to 13 to 18 cm (5 to 7 in.) water column by blowing into the rubber tubing. Pinch off the tubing and observe the manometer for one minute. A loss of pressure on the manometer indicates a leak in the meter box; leaks, if present, must be corrected.

5.7 Barometer. Calibrate against a mercury barometer.

#### 6. Calculations

Carry out calculations, retaining at least one extra decimal figure beyond that of the acquired data. Round off figures after the final calculation. Other forms of the equations may be used as long as they give equivalent results.

#### 6.1 Nomenclature

$A$  = Cross-sectional area of nozzle,  $m^2/(ft^2)$ .  
 $B$  = Water vapor in the gas stream, proportion by volume.  
 $C$  = Acetone blank residue concentration,  $mg/rig$ .  
 $c$  = Concentration of particulate matter in stack gas, dry basis, corrected to standard conditions,  $g/dscm$  ( $g/dscf$ ).  
 $I$  = Percent of isokinetic sampling.  
 $L$  = Maximum acceptable leakage rate for either a pretest leak check or for a leak check following a component change; equal to  $0.0037 m^3/min$  ( $0.02 cfm$ ) or 4 percent of the average sampling rate, whichever is less.  
 $L_1$  = Individual leakage rate observed during the leak check conducted prior to the "1st" component change ( $i=1, 2, 3, \dots$ ),  $m^3/min$  ( $cfm$ ).  
 $L_2$  = Leakage rate observed during the post-test leak check,  $m^3/min$  ( $cfm$ ).  
 $m_t$  = Total amount of particulate matter collected,  $mg$ .  
 $M_w$  = Molecular weight of water,  $18.0 g/g-mole$  ( $18.0 lb/lb-mole$ ).  
 $m_r$  = Mass of residue of acetone after evaporation,  $mg$ .  
 $P_m$  = Barometric pressure at the sampling site,  $mm Hg$  ( $in. Hg$ ).

$P_s$  = Absolute stack gas pressure,  $mm Hg$  ( $Hg$ ).  
 $P_{std}$  = Standard absolute pressure,  $760 mm Hg$  ( $29.92 in. Hg$ ).  
 $R$  = Ideal gas constant,  $0.08206 mm Hg \cdot m^3/g-mole \cdot K$  ( $ft^3 \cdot lb-mole \cdot R$ ).  
 $T_a$  = Absolute average dry gas meter temperature (see Figure 5-2),  $^{\circ}K$  ( $^{\circ}R$ ).  
 $T_s$  = Absolute average stack gas temperature (see Figure 5-2),  $^{\circ}K$  ( $^{\circ}R$ ).  
 $T_{std}$  = Standard absolute temperature,  $293^{\circ}K$  ( $528^{\circ}R$ ).  
 $V_b$  = Volume of acetone blank,  $ml$ .  
 $V_{wa}$  = Volume of acetone used in wash,  $ml$ .  
 $V_c$  = Total volume of liquid collected in impingers and silica gel (see Figure 5-3),  $ml$ .  
 $V_m$  = Volume of gas sample as measured dry gas meter,  $dscm$  ( $dscf$ ).  
 $V_{md}$  = Volume of gas sample measured by the dry gas meter, corrected to standard conditions,  $dscm$  ( $dscf$ ).  
 $V_{ws}$  = Volume of water vapor in the gas sample, corrected to standard conditions,  $dscm$  ( $dscf$ ).  
 $v$  = Stack gas velocity, calculated by Method 2, Equation 2-9, using data obtained from Method 3,  $m/sec$  ( $ft/sec$ ).  
 $W_r$  = Weight of residue in acetone wash,  $mg$ .  
 $Y$  = Dry gas meter calibration factor.  
 $\Delta H$  = Average pressure differential across the orifice meter (see Figure 5-2),  $mm H_2O$  ( $in. H_2O$ ).  
 $\rho_a$  = Density of acetone,  $mg/ml$  (see label on bottle).

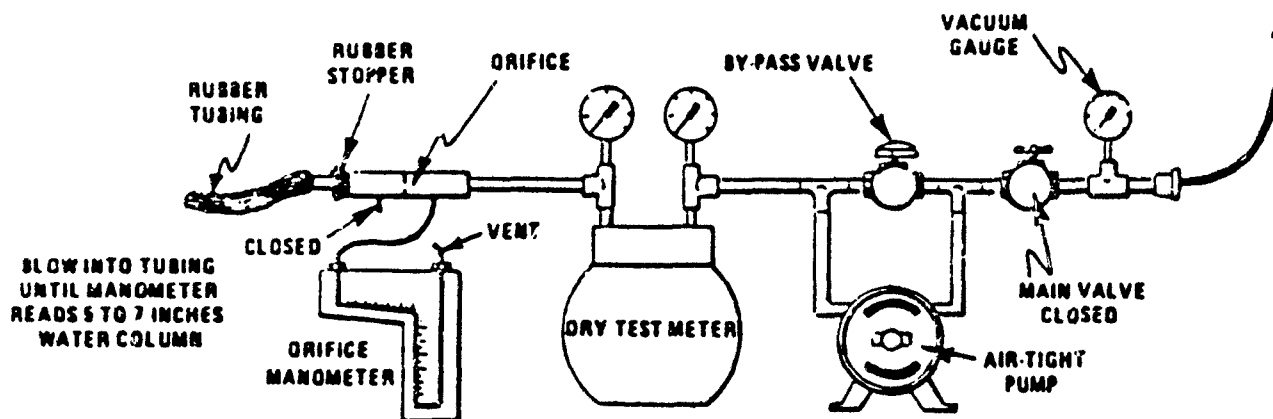


Figure 5-4. Leak check of meter box.

- $\rho_w$  = Density of water, 0.9982 g/ml (0.002201 lb/ml).  
 $\theta$  = Total sampling time, min.  
 $\theta_1$  = Sampling time interval, from the beginning of a run until the first component change, min.  
 $\theta_2$  = Sampling time interval, between two successive component changes, beginning with the interval between the first and second changes, min.  
 $\theta_n$  = Sampling time interval, from the final ( $n^{\text{th}}$ ) component change until the end of the sampling run, min.  
 $13.6$  = Specific gravity of mercury.  
 $60$  = Sec/min.  
 $100$  = Conversion to percent.

6.2 Average dry gas meter temperature and average orifice pressure drop. See data sheet (Figure 5-2).

6.3 Dry Gas Volume. Correct the sample volume measured by the dry gas meter to standard conditions (20° C; 760 mm Hg or 68° F, 29.92 in. Hg) by using Equation 5-1.

$$V_{n(tot)} = V_n Y \left( \frac{T_{std}}{T_n} \right) \left[ \frac{P_{std} + \frac{\Delta H}{13.6}}{P_{std}} \right]$$

$$= K_1 V_n Y \frac{P_{std} + (\Delta H/13.6)}{T_n}$$

Equation 5-1

where:

- $K_1$  = 0.3358 °K/mm Hg for metric units  
 = 17.34 °R/in. Hg for English units

Note: Equation 5-1 can be used as written unless the leakage rate observed during any of the mandatory leak checks (i.e., the post-test leak check or leak checks conducted prior to component changes) exceeds  $L_n$ . If  $L_n$  or  $L_n$  exceeds  $L_n$ , Equation 5-1 must be modified as follows:

(a) Case I. No component changes made during sampling run. In this case, replace  $V_n$  in Equation 5-1 with the expression:

$$V_n = (L_n - L_n) \theta$$

(b) Case II. One or more component changes made during the sampling run. In this case, replace  $V_n$  in Equation 5-1 by the expression:

$$V_n = (L_n - L_n) \theta_1$$

$$+ \sum_{i=2}^n (L_n - L_n) \theta_i + (L_n - L_n) \theta_n$$

and substitute only for those leakage rates ( $L_n$  or  $L_n$ ) which exceed  $L_n$ .

6.4 Volume of water vapor.

$$V_{n(tot)} = V_n \left( \frac{P_{std}}{P_n} \right) \left( \frac{RT_{std}}{P_{std}} \right) = K_2 V_n$$

Equation 5-2

where:

- $K_2$  = 0.001333 m<sup>3</sup>/m<sup>3</sup> for metric units  
 = 0.04707 (ft<sup>3</sup>/m<sup>3</sup>) for English units.  
 6.5 Moisture Content.

$$B_w = \frac{V_{n(tot)}}{V_{n(tot)} - V_{n(tot)}}$$

Equation 5-3

Note: In saturated or water droplet-laden gas streams, two calculations of the moisture content of the stack gas shall be made, one from the impinger analysis (Equation 5-3), and a second from the assumption of saturated conditions. The lower of the two values of  $B_w$  shall be considered correct. The procedure for determining the moisture content based upon assumption of saturated conditions is given in the Note of Section 1.2 of Method 1. For the purposes of this method, the average stack gas temperature from Figure 5-2 may be used to make this determination, provided that the accuracy of the in-stack temperature sensor is  $\pm 1^\circ$  C ( $\pm 2^\circ$  F).

6.6 Acetone Blank Concentration.

Equation 5-4

$$C_a = \frac{m_a}{V_{a,b}}$$

6.7 Acetone Wash Blank.

$$W_a = C_a V_{a,b} \quad \text{Equation 5-5}$$

6.8 Total Particulate Weight. Determine the total particulate catch from the sum of the weights obtained from containers 1 and 2 less the acetone blank (see Figure 5-3).

Note: Refer to Section 4.1.5 to assist in calculation of results involving two or more filter assemblies or two or more sampling trains.

6.9 Particulate Concentration.

$$C_p = (0.001 \text{ g/mg}) (m_p / V_{n(tot)}) \quad \text{Equation 5-6}$$

6.10 Conversion Factors:

From	To	Conversion Factor
ac	m <sup>3</sup>	0.02832
g/m <sup>3</sup>	g/m <sup>3</sup>	15.43
g/m <sup>3</sup>	lb/m <sup>3</sup>	2.205 x 10 <sup>-3</sup>
g/m <sup>3</sup>	g/m <sup>3</sup>	35.31
g	mg	0.001

6.11 Isokinetic Variation.

6.11.1 Calculation From Raw Data.

$$I = \frac{V_n Y}{100 T_n [K_1 V_n + (\frac{1}{T_n}) (P_{std} - \Delta H/13.6)]}$$

$$609 P_n A_n$$

Equation 5-7

where:

- $K_1$  = 0.003454 mm Hg-m<sup>3</sup>/m<sup>3</sup>-°K for metric units.  
 = 0.002569-in. Hg-(ft<sup>3</sup>/m<sup>3</sup>)-°R for English units.

6.11.2 Calculation From Intermediate Values.

$$I = \frac{T_n V_{n(tot)} P_{std} 100}{T_{n(tot)} P_n A_n P_{std} (1 - B_w)}$$

$$= K_1 \frac{T_n V_{n(tot)}}{P_n V_{n(tot)} (1 - B_w)}$$

Equation 5-8

where:

- $K_1$  = 4.320 for metric units  
 = 0.09450 for English units.

6.12 Acceptable Results. If 90 percent  $\leq I < 110$  percent, the results are acceptable. If the particulate results are low in comparison to the standard, and  $I$  is over 110 percent or less than 90 percent, the Administrator may accept the results. Citation 4 in the bibliography section can be used to make acceptability judgments. If  $I$  is judged to be unacceptable, reject the particulate results and repeat the test.

6.13 Stack Gas Velocity and Volumetric Flow Rate. Calculate the average stack gas velocity and volumetric flow rate, if needed, using data obtained in this method and the equations in Sections 5.2 and 5.3 of Method 2.

7. Alternative Procedures

7.1 Dry Gas Meter as a Calibration Standard. A dry gas meter may be used as a calibration standard for volume measurements in place of the wet test meter specified in Section 5.3, provided that it is calibrated initially and recalibrated periodically as follows:

7.1.1 Standard Dry Gas Meter Calibration.

7.1.1.1 The dry gas meter to be calibrated and used as a secondary reference meter should be of high quality and have an appropriately sized capacity, e.g., 3 liters/rev (0.1 ft<sup>3</sup>/rev), or equivalent, may be used for this calibration. Although a wet test meter is usually more practical. The wet test meter should have a capacity of 30 liters/rev (1 ft<sup>3</sup>/rev) and capable of measuring volume to within  $\pm 1.0$  percent; wet test meters should be checked against a spirometer or a liquid displacement meter to ensure the accuracy of the wet test meter. Spirometers or wet test meters of other sizes may be used, provided that the specified accuracies of the procedure are maintained.

7.1.1.2 Set up the components as shown in Figure 5.7. A spirometer, or equivalent, may be used in place of the wet test meter in the system. Run the pump for at least 5 minutes at a flow rate of about 10 liters/min (0.35 cfm) to condition the interior surface of the wet test meter. The pressure drop indicated by the manometer at the inlet side of the dry gas meter should be minimized (no greater than 100 mm H<sub>2</sub>O (4 in. H<sub>2</sub>O) at a flow rate of 30 liters/min (1 cfm)). This can be accomplished by using large diameter tubing connections and straight pipe fittings.



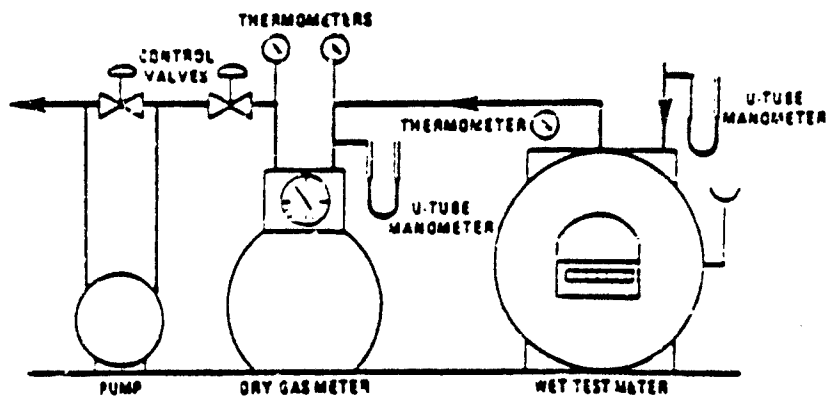


Figure 5.7. Equipment arrangement for dry-gas meter calibration.

7.1.1.3 Collect the data as shown in the example data sheet (see Figure 5-8). Make triplicate runs at each of the flow rates and at no less than five different flow rates. The

range of flow rates should be between 10 and 34 liters/min (0.25 and 1.2 cfm) or over the expected operating range.

DATE: \_\_\_\_\_

DRY GAS METER IDENTIFICATION: \_\_\_\_\_

BAROMETRIC PRESSURE ( $P_b$ ): \_\_\_\_\_ in. Hg

APPROXIMATE FLOW RATE ( $\bar{Q}$ ) cfm	SPIROMETER (WET METER) GAS VOLUME ( $V_s$ ) ft <sup>3</sup>	DRY GAS METER VOLUME ( $V_{dg}$ ) ft <sup>3</sup>	TEMPERATURES				DRY GAS METER 2 PRESSURE ( $\Delta p$ ) in. H <sub>2</sub> O	TIME ( $t$ ) min.	FLOW RATE ( $Q$ ) cfm	METER METER COEFFICIENT ( $V_{dm}$ )	AVERAGE METER COEFFICIENT ( $\bar{V}_{dm}$ )
			SPIROMETER (WET METER) ( $T_s$ ) °F	DRY GAS METER							
				INLET ( $T_i$ ) °F	OUTLET ( $T_o$ ) °F	AVERAGE ( $T_d$ ) °F					
0.00											
0.00											
0.00											
1.00											
1.20											

$$Q = 17.25 \cdot \frac{V_s}{t} \cdot \frac{P_b}{(P_b + \Delta P)}$$

$$V_{dm} = \frac{V_s}{V_{dm}} \cdot \frac{(T_s + 460)}{(T_{avg} + 460)} \cdot \frac{P_b}{P_b + \Delta P}$$

Figure 5.8. Example data sheet for calibration of a standard dry gas meter for method 5 sampling equipment (English units).

7.1.1.4 Calculate flow rate,  $Q$ , for each run using the wet test meter gas volume,  $V_w$ , and the run time,  $\theta$ . Calculate the dry gas meter coefficient,  $Y_m$ , for each run. These calculations are as follows:

$$Q = K \frac{P_w V_w}{L_w + L_m \theta}$$

$$Y_m = \frac{V_w}{V_m} \frac{(L_w + L_m)}{(L_w + L_m)} \frac{P_w}{\left(P_w + \frac{\Delta P}{13.6}\right)}$$

Where:

$K$  = 0.3858 for international system of units (SI); 17.64 for English units.

$V_w$  = Wet test meter volume, liters (ft<sup>3</sup>).

$V_m$  = Dry gas meter volume, liters (ft<sup>3</sup>).

$L_w$  = Average dry gas meter temperature, °C (°F).

$L_m$  = 273° C for SI units; 460° F for English units.

$L$  = Average wet test meter temperature, °C (°F).

$P_w$  = Barometric pressure, mm Hg (in. Hg).

$\Delta P$  = Dry gas meter inlet differential pressure, mm H<sub>2</sub>O (in. H<sub>2</sub>O).

$\theta$  = Run time, min.

7.1.1.5 Compare the three  $Y_m$  values at each of the flow rates and determine the maximum and minimum values. The difference between the maximum and minimum values at each flow rate should be no greater than 0.030. Extra sets of triplicate runs may be made in order to complete this requirement. In addition, the meter coefficients should be between 0.95 and 1.05. If these specifications cannot be met in three sets of successive triplicate runs, the meter is not suitable as a calibration standard and should not be used as such. If these specifications are met, average the three  $Y_m$  values at each flow rate resulting in five average meter coefficients,  $\bar{Y}_m$ .

7.1.1.6 Prepare a curve of meter coefficient,  $\bar{Y}_m$ , versus flow rate,  $Q$ , for the dry gas meter. This curve shall be used as a reference when the meter is used to calibrate other dry gas meters and to determine whether recalibration is required.

7.1.2 Standard Dry Gas Meter Recalibration.

7.1.2.1 Recalibrate the standard dry gas meter against a wet test meter or spirometer annually or after every 200 hours of operation, whichever comes first. This require-

ment is valid provided the standard dry gas meter is kept in a laboratory and, if transported, cared for as any other laboratory instrument. Abuse to the standard meter may cause a change in the calibration and will require more frequent recalibrations.

7.1.2.2 As an alternative to full recalibration, a two-point calibration check may be made. Follow the same procedure and equipment arrangement as for a full recalibration, but run the meter at only two flow rates (suggested rates are 14 and 38 liters/min (0.5 and 1.0 cfm)). Calculate the meter coefficients for these two points, and compare the values with the meter calibration curve. If the two coefficients are within  $\pm 1.5$  percent of the calibration curve values at the same flow rates, the meter need not be recalibrated until the next date for a recalibration check.

7.2 Critical Orifices As Calibration Standards. Critical orifices may be used as calibration standards in place of the wet test meter specified in Section 5.3, provided that they are selected, calibrated, and used as follows:

7.2.1 Section of Critical Orifices.

7.2.1.1 The procedure that follows describes the use of hypodermic needles or stainless steel needle tubings which have been found suitable for use as critical orifices. Other materials and critical orifice designs may be used provided the orifices act as true critical orifices; i.e., a critical vacuum can be obtained, as described in Section 7.2.2.3. Select five critical orifices that are appropriately sized to cover the range of flow rates between 10 and 34 liters/min or the expected operating range. Two of the critical orifices should bracket the expected operating range.

A minimum of three critical orifices will be needed to calibrate a Method 5 dry gas meter (DCM); the other two critical orifices can serve as spares and provide better selection for bracketing the range of operating flow rates. The needle sizes and tubing lengths shown below give the following approximate flow rates:

Gauge/ID	Flow rate (liters/min)	Gauge/ID	Flow rate (liters/min)
12/7.5	32.96	14/7.5	19.54
12/10.2	30.02	14/8.1	17.27
13/2.5	25.77	14/7.6	16.14
13/5.1	23.50	15/3.2	14.16
13/7.5	2.37	15/7.5	11.81
13/10.2	0.67	15/7.2	10.46

7.2.1.2 These needles can be adapted to a Method 5 type sampling train as follows: Insert a serum bottle stopper, 13- by 20-mm silicone type, into a 1/2-inch Swagelok quick connect. Insert the needle into the stopper as shown in Figure 5-6.

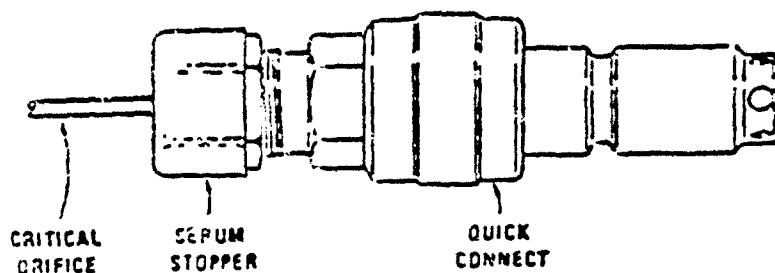


Figure 5-9. Critical orifice adaptation to Method 5 metering system.

7.2.2 Critical Orifice Calibration. The procedure described in this section uses the Method 5 meter box configuration with a DGM as described in Section 2.1.8 to calibrate the critical orifice. Other schemes may be used, subject to the approval of the Administrator.

7.2.2.1 Calibration of Meter Box. The critical orifices must be calibrated in the same configuration as they will be used. i.e., there should be no connections to the inlet of the orifice.

7.2.2.1.1 Before calibrating the meter box, leak check the system as follows: Fully open the coarse adjust valve, and completely close the by-pass valve. Plug the inlet. Then turn on the pump, and determine whether there is any leakage. The leakage rate shall be zero; i.e., no detectable movement of the DGM dial shall be seen for 1 minute.

7.2.2.1.2 Check also for leakage in that portion of the sampling train between the pump and the orifice meter. See Section 3.6 for the procedure; make any corrections, if necessary. If leakage is detected, check for

cracked gaskets, loose fittings, worn O-rings, etc., and make the necessary repairs.

7.2.2.1.3 After determining that the meter box is leakless, calibrate the meter box according to the procedure given in Section 5.3. Make sure that the wet test meter meets the requirements stated in Section 7.1.1.1. Check the water level in the wet test meter. Record the DGM calibration factor, Y.

7.2.2.2 Calibration of Critical Orifices. Set up the apparatus as shown in Figure 5-10.   
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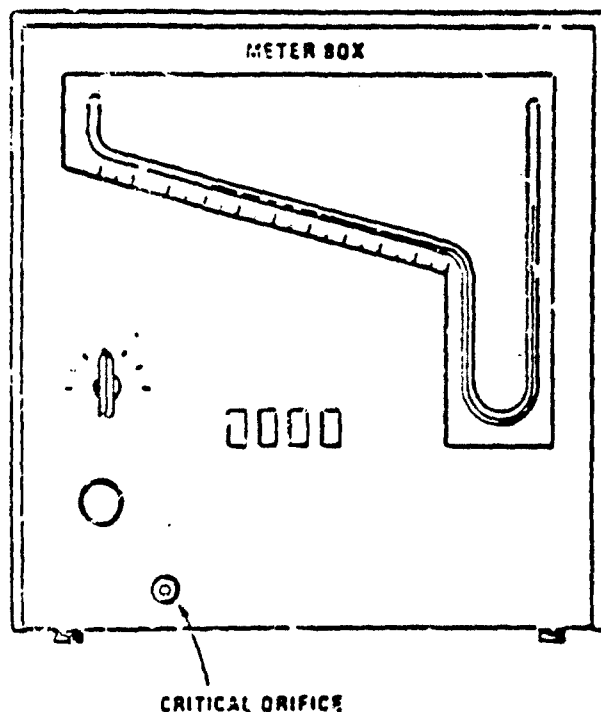


Figure 5-10. Apparatus setup.

7.2.2.2.1 Allow a warm-up time of 15 minutes. This step is important to equilibrate the temperature conditions through the DGM.

7.2.2.2.2 Leak check the system as in Section 7.2.2.1.1. The leakage rate shall be zero.

7.2.2.2.3 Before calibrating the critical orifice, determine its suitability and the appropriate operating vacuum as follows: Turn on the pump, fully open the coarse adjust valve, and adjust the by-pass valve to give a vacuum reading corresponding to about half of atmospheric pressure. Observe the meter box critical manometer reading, H. Slowly increase the vacuum reading until a stable reading is obtained on the meter box critical manometer. Record the critical vacuum for each orifice.

Orifices that do not reach a critical value shall not be used.

7.2.2.2.4 Obtain the barometric pressure using a barometer as described in Section 2.1.9. Record the barometric pressure,  $P_{amb}$ , in mm Hg (in. Hg).

7.2.2.2.5 Conduct duplicate runs at a vacuum of 25 to 50 mm Hg (1 to 2 in. Hg) above the critical vacuum. The runs shall be at least 5 minutes each. The DGM volume readings shall be in increments of 0.00283 m<sup>3</sup> (0.1 ft<sup>3</sup>) or in increments of complete revolutions of the DGM. As a guideline, the times should not differ by more than 5.0 seconds (this includes allowance for changes in the DGM temperatures) to achieve  $\pm 0.5$  percent in K'. Record the information listed in Figure 5-11.

7.2.2.2.6 Calculate K' using Equation 5-9.

K' = Critical orifice coefficient.

$T_{amb}$  = Absolute ambient temperature, °K (°R). Average the K' values. The individual K' values should not differ by more than  $\pm 0.5$  percent from the average.

$$K' = \frac{K_1 V_{std} Y (P_{amb} + \Delta H / 13.6) \sqrt{T_{amb}}}{P_{amb} T_{std} \phi} \quad \text{Eq. 5-9}$$

$$\frac{(m^3(^{\circ}K)^{1/2})}{(mm. Hg) (min)} \left[ \frac{(ft^3(^{\circ}R)^{1/2})}{(in. Hg) (min)} \right]$$

Sections 7.2.2.1 to 7.2.2.3. Record the information listed in Figure 5.12.

7.2.3 Using the Critical Orifices as Calibration Standards.

7.2.3.1 Record the barometric pressure.

Date \_\_\_\_\_ Train ID \_\_\_\_\_ DGM cal. factor \_\_\_\_\_ Critical orifice ID \_\_\_\_\_

Dry gas meter	Run No.	
	1	2
Final reading _____ m <sup>3</sup> (ft <sup>3</sup> )		
Initial reading _____ m <sup>3</sup> (ft <sup>3</sup> )		
Difference, $V_D$ _____ m <sup>3</sup> (ft <sup>3</sup> )		
Inlet/Outlet temperatures:		
Initial _____ °C (°F) _____ / _____ / _____		
Final _____ °C (°F) _____ / _____ / _____		
Avg. _____ °C (°F) _____		
Temperature, $T_{amb}$ _____		
Time, $\Theta$ _____ min/sec _____ / _____ / _____		
Orifice man. rdg., _____ mm (in.)		
$\Delta H$ _____ H <sub>2</sub> O _____		
Bar. pressure, $P_{amb}$ _____ mm (in.) Hg _____		
Ambient temperature, $T_{amb}$ _____ °C (°F) _____		
Pump vacuum _____ mm (in.) Hg _____		
K' factor _____		
Average _____		

Figure 5-11. Data sheet for determining K' factor.

7.2.3.2 Calibrate the metering system according to the procedure outlined in

7.2.3.3 Calculate the standard volume of air passed through the DGM and the critical orifice, and calculate the DGM calibration factor, Y, using the equations below:

$$V_{std} = K_1 V_D \frac{P_{amb} + (\Delta H / 13.6)}{T_{amb}} \quad \text{Eq. 5-10}$$

$$V_{std} = K' \frac{P_{amb} \Theta}{T_{amb}} \quad \text{Eq. 5-11}$$

$$Y = \frac{V_{std}}{V_D} \quad \text{Eq. 5-12}$$

where:

$V_{std}$  = Volume of gas sample passed through the critical orifice, corrected to standard conditions, dm<sup>3</sup> (scf).

$K_1$  = 0.2856 °K/mm Hg for metric units = 17.04 °R/in. Hg for English units.

7.2.3.4 Average the DGM calibration values for each of the flow rates. The calibration factor, Y, at each of the flow rates should not differ by more than  $\pm 2$  percent from the average.

7.2.3.5 To determine the need for recalibrating the critical orifices, compare the DGM Y factors obtained from two adjacent orifices each time a DGM is calibrated; for example, when checking 13/2.5, use orifices 12/10.5 and 13/5.1. If any critical orifice yields a DGM Y factor differing by more than 2 percent from the others, recalibrate the critical orifice according to Section 7.2.2.

Date \_\_\_\_\_ Train ID \_\_\_\_\_ Critical orifice ID \_\_\_\_\_ Critical orifice K' factor \_\_\_\_\_

Dry gas meter	Run No.	
	1	2
Final reading _____ m <sup>3</sup> (ft <sup>3</sup> )		
Initial reading _____ m <sup>3</sup> (ft <sup>3</sup> )		
Difference, $V_D$ _____ m <sup>3</sup> (ft <sup>3</sup> )		
Inlet/Outlet temperatures:		
Initial _____ °C (°F) _____ / _____ / _____		
Final _____ °C (°F) _____ / _____ / _____		
Avg. _____ °C (°F) _____		
Temperature, $T_{amb}$ _____		
Time, $\Theta$ _____ min/sec _____ / _____ / _____		
Orifice man. rdg., _____ mm (in.)		
$\Delta H$ _____ H <sub>2</sub> O _____		
Bar. pressure, $P_{amb}$ _____ mm (in.) Hg _____		
Ambient temperature, $T_{amb}$ _____ °C (°F) _____		
Pump vacuum _____ mm (in.) Hg _____		
$V_{std}$ _____ m <sup>3</sup> (ft <sup>3</sup> )		
$V_D$ _____ m <sup>3</sup> (ft <sup>3</sup> )		
DGM cal. factor, Y _____		

Figure 5-12. Data sheet for determining DGM Y factor

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[FR Doc. 87-4551 Filed 3-25-87; 9:48 am]

July 1990  
Revision: Final

**EPA METHOD 3A**

**DETERMINATION OF OXYGEN AND CARBON DIOXIDE  
CONCENTRATIONS IN EMISSIONS FROM STATIONARY SOURCES**

**Method 3A—Determination of Oxygen and Carbon Dioxide Concentrations in Emissions From Stationary Sources (Instrumental Analyzer Procedure)**

**1. Applicability and Principle.**

1.1 **Applicability.** This method is applicable to the determination of oxygen ( $O_2$ ) and carbon dioxide ( $CO_2$ ) concentrations in emissions from stationary sources only when specified within the regulations.

1.2 **Principle.** A sample is continuously extracted from the effluent stream; a portion of the sample stream is conveyed to an instrumental analyzer(s) for determination of  $O_2$  and  $CO_2$  concentration(s). Performance specifications and test procedures are provided to ensure reliable data.

**2. Range and Sensitivity.**

Same as Method 6C, Sections 2.1 and 2.2, except that the span of the monitoring system shall be selected such that the average  $O_2$  or  $CO_2$  concentration is not less than 20 percent of the span.

**3. Definitions.**

3.1 **Measurement System.** The total equipment required for the determination of the  $O_2$  or  $CO_2$  concentration. The measurement system consists of the same major subsystems as defined in Method 6C, Sections 3.1.1, 3.1.2, and 3.1.3.

3.2 **Span, Calibration Gas, Analyzer Calibration Error, Sampling System Bias, Zero Drift, Calibration Drift, Response Time, and Calibration Curve.** Same as Method 6C, Sections 3.2 through 3.4, and 3.10.

3.3 **Interference Response.** The output response of the measurement system to a component in the sample gas, other than the gas component being measured.

**4. Measurement System Performance Specifications.**

Same as Method 6C, Sections 4.1 through 4.4.

**5. Apparatus and Reagents.**

5.1 **Measurement System.** Any measurement system for  $O_2$  or  $CO_2$  that meets the specifications of this method. A schematic of an acceptable measurement system is shown in Figure 6C-1 of Method 6C. The essential components of the measurement system are described below:

5.1.1 **Sample Probe.** A leak-free probe, of sufficient length to traverse the sample points.

5.1.2 **Sample Line.** Tubing to transport the sample gas from the probe to the moisture removal system. A heated sample line is not required for systems that measure the  $O_2$  or  $CO_2$  concentration on a dry basis, or transport dry gases.

5.1.3 **Sample Transport Line.** Calibration Value Assembly, Moisture Removal System, Particulate Filter, Sample Pump, Sample Flow Rate Control, Sample Gas Manifold, and Data Recorder. Same as Method 6C, Sections 5.1.3 through 5.1.8, and 5.1.11, except that the requirements to use stainless steel, Teflon, and nonreactive glass filters do not apply.

5.1.4 **Gas Analyzer.** An analyzer to determine continuously the  $O_2$  or  $CO_2$  concentration in the sample gas stream. The analyzer shall meet the applicable performance specifications of Section 4. A means of controlling the analyzer flow rate

and a device for determining proper sample flow rate (e.g., precision rotameter, pressure gauge downstream of all flow controls, etc.) shall be provided at the analyzer. The requirements for measuring and controlling the analyzer flow rate are not applicable if data are presented that demonstrate the analyzer is insensitive to flow variations over the range encountered during the test.

5.2 **Calibration Gases.** The calibration gases for  $CO_2$  analyzers shall be  $CO_2$  in  $N_2$  or  $CO_2$  in air. Alternatively,  $CO_2/SO_2$ ,  $O_2/SO_2$ , or  $O_2/CO_2/SO_2$  gas mixtures in  $N_2$  may be used. Three calibration gases, as specified Section 5.3.1 through 5.3.3 of Method 6C, shall be used. For  $O_2$  monitors that cannot analyze zero gas, a calibration gas concentration equivalent to less than 10 percent of the span may be used in place of zero gas.

**6. Measurement System Performance Test Procedures.**

Perform the following procedures before measurement of emissions (Section 7).

6.1 **Calibration Concentration Verification.** Follow Section 6.1 of Method 6C, except if calibration gas analysis is required, use Method 3 and change the acceptance criteria for agreement among Method 3 results to 3 percent (or 0.2 percent by volume, whichever is greater).

6.2 **Interference Response.** Conduct an interference response test of the analyzer prior to its initial use in the field. Thereafter, recheck the measurement system if changes are made in the instrumentation that could alter the interference response (e.g., changes in the type of gas detector). Conduct the interference response in accordance with Section 5.4 of Method 2B.

6.3 **Measurement System Preparation.** Analyzer Calibration Error, and Sampling System Bias Check. Follow Sections 6.2 through 6.4 of Method 6C.

**7. Emission Test Procedure.**

7.1 **Selection of Sampling Site and Sampling Points.** Select a measurement site and sampling points using the same criteria that are applicable to tests performed using Method 3.

7.2 **Sample Collection.** Position the sampling probe at the first measurement point, and begin sampling at the same rate as used during the sampling system bias check. Maintain constant rate sampling (i.e.,  $\pm 10$  percent) during the entire run. The sampling time per run shall be the same as for tests conducted using Method 3 plus twice the system response time. For each run, use only those measurements obtained after twice the response time of the measurement system has elapsed to determine the average effluent concentration.

7.3 **Zero and Calibration Drift Test.** Follow Section 7.4 of Method 6C.

**8. Quality Control Procedures.**

The following quality control procedures are recommended when the results of this method are used for an emission rate correction factor, or excess air determination. The tester should select one of the following options for validating measurement results:

8.1 If both  $O_2$  and  $CO_2$  are measured using Method 3A, the procedures described in Section 4.4 of Method 3 should be followed to validate the  $O_2$  and  $CO_2$  measurement results.

8.2 If only  $O_2$  is measured using Method 3A, measurements of the sample stream  $CO_2$  concentration should be obtained at the sample by-pass vent discharge using an Orsat or Fyrite analyzer, or equivalent. Duplicate samples should be obtained concurrently with at least one run. Average the duplicate Orsat or Fyrite analysis results for each run. Use the average  $CO_2$  values for comparison with the  $O_2$  measurements in accordance with the procedures described in Section 4.4 of Method 3.

8.3 If only  $CO_2$  is measured using Method 3A, concurrent measurements of the sample stream  $O_2$  concentration should be obtained using an Orsat or Fyrite analyzer as described in Section 8.2. For each run, differences greater than 0.5 percent between the Method 3A results and the average of the duplicate Fyrite analysis should be investigated.

**9. Emission Calculation.**

For all  $CO_2$  analyzers, and for  $O_2$  analyzers that can be calibrated with zero gas, follow Section 9 of Method 6C, except express all concentrations as percent, rather than ppm.

For  $O_2$  analyzers that use a low-level calibration gas in place of a zero gas, calculate the effluent gas concentration using Equation 3A-1.

$$C_{em} = \frac{C_{cal} - C_{cal}}{C_{cal} - C_0} (C - C_0) + C_{cal}$$

Eq. 3A-1

where:

$C_{em}$  = Effluent gas concentration, dry basis, percent.

$C_{cal}$  = Actual concentration of the upscale calibration gas, percent.

$C_0$  = Actual concentration of the low-level calibration gas, percent.

$C_{cal}$  = Average of initial and final system calibration bias check responses for the upscale calibration gas, percent.

$C_0$  = Average of initial and final system calibration bias check responses for the low-level gas, percent.

$C$  = Average gas concentration indicated by the gas analyzer, dry basis, percent.

**10. Bibliography.**

Same as bibliography of Method 6C.

4.2.5 To insure complete absorption of the  $\text{CO}_2$ ,  $\text{O}_2$ , or if applicable,  $\text{CO}$ , make repeated passes through each absorbing solution until two consecutive readings are the same. Several passes (three or four) should be made between readings. If constant readings cannot be obtained after three consecutive readings, replace the absorbing solution.

4.2.6 Repeat the analysis until the following criteria are met:

4.2.6.1 For percent  $\text{CO}_2$ , repeat the analytical procedure until the results of any three analyses differ by no more than (a) 0.3 percent by volume when  $\text{CO}_2$  is greater than 4.0 percent or (b) 0.2 percent by volume when  $\text{CO}_2$  is less than or equal to 4.0 percent. Average the three acceptable values of percent  $\text{CO}_2$  and report the results to the nearest 0.1 percent.

4.2.6.2 For percent  $\text{O}_2$ , repeat the analytical procedure until the results of any three analyses differ by no more than (a) 0.3 percent by volume when  $\text{O}_2$  is less than 15.0 percent or (b) 0.2 percent by volume when  $\text{O}_2$  is greater than or equal to 15.0 percent. Average the three acceptable values of percent  $\text{O}_2$  and report the results to the nearest 0.1 percent.

4.2.6.3 For percent  $\text{CO}$ , repeat the analytical procedure until the results of any three analyses differ by no more than 0.3 percent. Average the three acceptable values of percent  $\text{CO}$  and report the results to the nearest 0.1 percent.

4.2.7 After the analysis is completed, leak-check (mandatory) the Orsat analyzer once again, as described in Section 5. For the results of the analysis to be valid, the Orsat analyzer must pass this leak test before an after the analysis.

NOTE: Although in most instances only  $\text{CO}_2$  or  $\text{O}_2$  is required, it is recommended that both  $\text{CO}_2$  and  $\text{O}_2$  be measured, and that Section 4.4.1 be used to validate the analytical data.

4.3 Multi-Point, Integrated Sampling and Analytical Procedure.

4.3.1 Both the minimum number of sampling points and the sampling point location shall be as specified in Section 3.3.1 of this method. The use of fewer points than specified is subject to the approval of the Administrator.

4.3.2 Follow the procedures outlined in Sections 4.2.2 through 4.2.7, except for the following: Traverse all sampling points and sample at each point for an equal length of time. Record sampling data as shown in Figure 3-3.

#### 4.4 Quality Control Procedures.

4.4.1 Data Validation When Both  $\text{CO}_2$  and  $\text{O}_2$  Are Measured. Although in most instances, only  $\text{CO}_2$  or  $\text{O}_2$  measurement is required, it is recommended that both  $\text{CO}_2$  and  $\text{O}_2$  be measured to provide a check on the quality of the data. The following quality control procedure is suggested.

NOTE: Since the method for validating the  $\text{CO}_2$  and  $\text{O}_2$  analyses is based on combustion of organic and fossil fuels and dilution of the gas stream with air, this method does not apply to sources that (1) remove  $\text{CO}_2$  or  $\text{O}_2$  through processes other than combustion, (2) add  $\text{O}_2$  (e.g., oxygen enrichment) and  $\text{N}_2$  in proportions different from that of air, (3) add  $\text{CO}_2$  (e.g., cement or lime kilns), or (4) have no fuel factor,  $F_p$ , values obtainable (e.g., extremely variable waste mixtures). This method validates the measured proportions of  $\text{CO}_2$  and  $\text{O}_2$  for the fuel type, but the method does not detect sample dilution resulting from leaks during or after sample collection. The method is applicable

for samples collected downstream of most lime or limestone flue-gas desulfurization units as the  $\text{CO}_2$  added or removed from the gas stream is not significant in relation to the total  $\text{CO}_2$  concentration. The  $\text{CO}_2$  concentrations from other types of scrubbers using only water or basic slurry can be significantly affected and would render the  $F_p$  check minimally useful.

4.4.1.1 Calculate a fuel factor,  $F_p$ , using the following equation:

$$F_p = \frac{20.9 - \% \text{O}_2}{\% \text{CO}_2}$$

#### Eq. 3-3

Where:

$\% \text{O}_2$  = Percent  $\text{O}_2$  by volume (dry basis).

$\% \text{CO}_2$  = Percent  $\text{CO}_2$  by volume (dry basis).

20.9 = Percent  $\text{O}_2$  by volume in ambient air.

If  $\text{CO}$  is present in quantities measurable by this method, adjust the  $\text{O}_2$  and  $\text{CO}_2$  values before performing the calculation for  $F_p$ , as follows:

$$\% \text{CO}_2(\text{adj}) = \% \text{CO}_2 + \% \text{CO}$$

$$\% \text{O}_2(\text{adj}) = \% \text{O}_2 - 0.5 \% \text{CO}$$

Where:  $\% \text{CO}$  = Percent  $\text{CO}$  by volume (dry basis).

4.4.1.2 Compare the calculated  $F_p$  factor with the expected  $F_p$  values. The following table may be used in establishing acceptable ranges for the expected  $F_p$  if the fuel being burned is known. When fuels are burned in combination, calculate the combined fuel  $F_p$  and  $F_p$  factors (as defined in Method 19) according to the procedure in Method 19 Section 5.2.3. Then calculate the  $F_p$  factor as follows:

$$F_p = \frac{0.209 F_p}{F_p}$$

#### Eq. 3-4

Fuel type	$F_p$ range
Coal:	
Anthracite and lignite	1.018-1.130
Subbituminous	1.083-1.220
Oil:	
Crude oil	1.280-1.413
Residual	1.210-1.370
Gas:	
Natural	1.800-1.838
Propane	1.434-1.588
Butane	1.405-1.583
Wood:	
Wood bark	1.000-1.120

Calculated  $F_p$  values beyond the acceptable ranges shown in this table should be investigated before accepting the test results. For example, the strength of the solutions in the gas analyzer and the analyzing technique should be checked by sampling and analyzing a known concentration, such as air; the fuel factor should be reviewed and verified. An acceptability range of  $\pm 12$  percent is appropriate for the  $F_p$  factor of mixed fuels with variable fuel ratios. The level of the emission rate relative to the compliance level should be considered in determining if a retest is appropriate, i.e., if the measured emissions are much lower or much greater than the compliance limit, repetition of the test would not significantly change the compliance status of the source and would be unnecessarily time-consuming and costly.

5. Leak-Check Procedure for Orsat Analyzer. Moving an Orsat analyzer frequently causes it to leak. Therefore, an Orsat analyzer should be thoroughly leak-checked site before the flue gas sample is introduced into it. The procedure for leak-checking an Orsat analyzer is:

5.1.1 Bring the liquid level in each pipette up to the reference mark on the delivery tubing and then close the pipette cock.

5.1.2 Raise the leveling bulb sufficiently to bring the confining liquid meniscus the graduated portion of the burette then close the manifold stopcock.

5.1.3 Record the meniscus position.

5.1.4 Observe the meniscus in the bulb and the liquid level in the pipette for a moment over the next 4 minutes.

5.1.5 For the Orsat analyzer to pass leak-check, two conditions must be met.

5.1.5.1 The liquid level in each pipette must not fall below the bottom of the delivery tubing during this 4-minute interval.

5.1.5.2 The meniscus in the burette must not change by more than 0.2 ml during 4-minute interval.

5.1.6 If the analyzer fails the leak-check procedure, all rubber connections and cocks should be checked until the cause of the leak is identified. Leaking stops must be disassembled, cleaned, and greased. Leaking rubber connections must be replaced. After the analyzer is repaired, the leak-check procedure must be repeated.

#### 6. Calculations

##### 6.1 Nomenclature.

$M_w$  = Dry molecular weight, g/g-mole (lb/mole).

$\% \text{EA}$  = Percent excess air.

$\% \text{CO}_2$  = Percent  $\text{CO}_2$  by volume (dry basis).

$\% \text{O}_2$  = Percent  $\text{O}_2$  by volume (dry basis).

$\% \text{CO}$  = Percent  $\text{CO}$  by volume (dry basis).

$\% \text{N}_2$  = Percent  $\text{N}_2$  by volume (dry basis).

0.284 = Ratio of  $\text{O}_2$  to  $\text{N}_2$  in air, v/v.

0.280 = Molecular weight of  $\text{N}_2$  or  $\text{CO}_2$ , divided by 100.

0.320 = Molecular weight of  $\text{O}_2$ , divided by 100.

0.440 = Molecular weight of  $\text{CO}$ , divided by 100.

6.2 Percent Excess Air. Calculate the percent excess air (if applicable), by substituting the appropriate values of percent  $\text{CO}_2$  and  $\text{N}_2$  (obtained from Section 4.1 4.2.4) into Equation 3-1.

$\% \text{EA} =$

$$\frac{\% \text{O}_2 - 0.5 \% \text{CO}}{0.284 \% \text{N}_2 - (\% \text{O}_2 - 0.5 \% \text{CO})} \times$$

Equation:

NOTE: The equation above assumes ambient air is used as the source of  $\text{O}_2$  that the fuel does not contain appreciable amounts of  $\text{N}_2$  (as do coke oven or blast furnace gases). For those cases when appreciable amounts of  $\text{N}_2$  are present (coal, oil, natural gas do not contain appreciable amounts of  $\text{N}_2$ ) or when oxygen enrichment is used, alternate methods, subject to approval of the Administrator, are required.

6.3 Dry Molecular Weight. Use Equation 3-2 to calculate the dry molecular weight of the stack gas.

$$M_w = 0.440 (\% \text{CO}_2) + 0.320 (\% \text{O}_2) + 0.280 (\% \text{N}_2) + 9$$

Equation



NOTE: The above equation does not consider argon in air (about 0.9 percent, molecular weight of 39.9). A negative error of about 0.4 percent is introduced. The tester may opt to include argon in the analysis using procedures subject to approval of the Administrator.

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July 1990  
Revision: Final

**EPA METHOD 7E**  
**DETERMINATION OF NITROGEN OXIDE EMISSIONS**  
**FROM STATIONARY SOURCES**

**Method 7E—Determination of Nitrogen Oxides Emissions From Stationary Sources (Instrumental Analyzer Procedure)**

**1. Applicability and Principle**

1.1 **Applicability.** This method is applicable to the determination of nitrogen oxides ( $\text{NO}_x$ ) concentrations in emissions from stationary sources only when specified within the regulations.

1.2 **Principle.** A gas sample is continuously extracted from a stack, and a portion of the sample is conveyed to an instrumental chemiluminescent analyzer for determination of  $\text{NO}_x$  concentration. Performance specifications and test procedures are provided to ensure reliable data.

**2. Range and Sensitivity**

Same as Method 6C, Sections 2.1 and 2.2.

**3. Definitions**

3.1 **Measurement System.** The total equipment required for the determination of  $\text{NO}_x$  concentration. The measurement system consists of the following major subsystems:

3.1.1 **Sample Interface, Gas Analyzer, and Data Recorder.** Same as Method 6C, Sections 3.1.1, 3.1.2, and 3.1.3.

3.1.2  **$\text{NO}_x$  to  $\text{NO}$  Converter.** A device that converts the nitrogen dioxide ( $\text{NO}_2$ ) in the sample gas to nitrogen oxide ( $\text{NO}$ ).

3.2 **Span, Calibration Gas, Analyzer Calibration Error, Sampling System Bias, Zero Drift, Calibration Drift, and Response Time.** Same as Method 6C, Sections 3.2 through 3.4.

3.3 **Interference Response.** The output response of the measurement system to a component in the sample gas, other than the gas component being measured.

**4. Measurement System Performance Specifications**

Same as Method 6C, Sections 4.1 through 4.4.

**5. Apparatus and Reagents**

5.1 **Measurement System.** Any measurement system for  $\text{NO}_x$  that meets the specifications of this method. A schematic of an acceptable measurement system is shown in Figure 6C-1 of Method 6C. The essential components of the measurement system are described below:

5.1.1 **Sample Probe, Sample Line, Calibration Valve Assembly, Moisture Removal System, Particulate Filter, Sample Pump, Sample Flow Rate Control, Sample Gas Manifold, and Data Recorder.** Same as Method 6C, Sections 5.1.1 through 5.1.9, and 5.1.11.

5.1.2  **$\text{NO}_x$  to  $\text{NO}$  Converter.** That portion of the system that converts the nitrogen dioxide ( $\text{NO}_2$ ) in the sample gas to nitrogen oxide ( $\text{NO}$ ). An  $\text{NO}_x$  to  $\text{NO}$  converter is not necessary if data are presented to

demonstrate that the  $\text{NO}_2$  portion of the exhaust gas is less than 5 percent of the total  $\text{NO}_x$  concentration.

5.1.3  **$\text{NO}_x$  Analyzer.** An analyzer based on the principles of chemiluminescence, to determine continuously the  $\text{NO}_x$  concentration in the sample gas stream. The analyzer shall meet the applicable performance specifications of Section 4. A means of controlling the analyzer flow rate and a device for determining proper sample flow rate (e.g., precision rotameter, pressure gauge downstream of all flow controls, etc.) shall be provided at the analyzer.

5.2  **$\text{NO}_x$  Calibration Gases.** The calibration gases for the  $\text{NO}_x$  analyzer shall be  $\text{NO}$  in  $\text{N}_2$ . Three calibration gases, as specified in Sections 5.3.1 through 5.3.3, of Method 6C, shall be used. Ambient air may be used for the zero gas.

**6. Measurement System Performance Test Procedures**

Perform the following procedures before measurement of emissions (Section 7).

6.1 **Calibration Gas Concentration Verification.** Follow Section 6.1 of Method 6C, except if calibration gas analysis is required, use Method 7, and change all 5 percent performance values to 10 percent (or 10 ppm, whichever is greater).

6.2 **Interference Response.** Conduct an interference response test of the analyzer prior to its initial use in the field. Thereafter, recheck the measurement system if changes are made in the instrumentation that could alter the interference response (e.g., changes in the gas detector). Conduct the interference response in accordance with Section 5.4 of Method 20.

6.3 **Measurement System Preparation, Analyzer Calibration Error, and Sample System Bias Check.** Follow Sections 6.2 through 6.4 of Method 6C.

6.4  **$\text{NO}_x$  to  $\text{NO}$  Conversion Efficiency.** Unless data are presented to demonstrate that the  $\text{NO}_2$  concentration within the sample stream is not greater than 5 percent of the  $\text{NO}_x$  concentration, conduct an  $\text{NO}_x$  to  $\text{NO}$  conversion efficiency test in accordance with Section 5.8 of Method 20.

**7. Emission Test Procedure**

7.1 **Selection of Sampling Site and Sampling Points.** Select a measurement site and sampling points using the same criteria that are applicable to tests performed using Method 7.

7.2 **Sample Collection.** Position the sampling probe at the first measurement point, and begin sampling at the same rate as used during the system calibration drift test. Maintain constant rate sampling (i.e.,  $\pm 10$  percent) during the entire run. The sampling time per run shall be the same as the total time required to perform a run using Method 7, plus twice the system response time. For each run, use only those measurements obtained after twice the response time of the measurement system has elapsed, to determine the average effluent concentration.

7.3 **Zero and Calibration Drift Test.** Follow Section 7.4 of Method 6C.

8. **Emission Calculation.** Follow Section 8 of Method 6C.

**9. Bibliography**

Same as bibliography of Method 6C.

July 1990  
Revision: Final

**APPENDIX C**  
**DESCRIPTION OF CEM SYSTEM**

## C.0 DESCRIPTION OF CONTINUOUS EMISSION MONITORING SAMPLING SYSTEM

The CEM system used for gaseous pollutant monitoring by EPA Methods 3A, 7E, 10, and 25A is shown in Figure C-1. The sample gas handling system is shown in Figure C-2.

**C.1 Sampling system.** Exhaust gas is drawn from the duct or stack through a heated stainless steel (S.S.) probe that is inserted into the duct or stack through one of the test ports. A S.S. valve is located at the probe exit to permit introduction of certified zero and calibration span gases. A heated teflon line is used to transport the sample or zero/calibration gases to the Continuous Emission Monitoring (CEM) trailer. Temperatures are monitored at the exit of each section of line to ensure temperatures are above the sample dew point. Once inside the CEM trailer, the sample line enters a heated junction box where the sample is split into three fractions, and each fraction is directed to one of the following:

- (a) Charleton Model SC-14 Sample Conditioner.
- (b) Thermo Electron Model 900 Sample Conditioner.
- (c) Direct Connection to Total Hydrocarbon Analyzers.

The Charleton Model SC-14 unit is an extractive sample conditioner that removes particulates and moisture from the sample gas. The extracted sample gas is passed through a sintered stainless bypass filter, which removes particulates down to 1 micron or less by an internal filtration technique. The filter is maintained at a temperature above the dew point of the sample gases.

The clean, filtered sample is then introduced to a permeation dryer where moisture is removed without condensation or dilution to achieve a sample dew point well below that of the ambient temperature. The clean, dried sample is then directed to the carbon monoxide (CO), carbon dioxide (CO<sub>2</sub>), oxygen (O<sub>2</sub>), and nitrous oxides (NO<sub>x</sub>) analyzers using a teflon-headed sample pump.

The dilution ratio of the Thermo Electron Model 900 sample conditioner is a function of sample/dilution air pressure and capillary tube size. Once set, the dilution ratio is a constant. Sample concentrations are determined by multiplying the analyzer output times the dilution ratio. Nominal dilution ratio for the Thermo Electron Model 900 is 10 to 1.

In the J.U.M. Engineer VE-7 Total Hydrocarbon Analyzer, a S.S. sample filter and detector are contained in a temperature controlled oven. This permits the direct analysis of total hydrocarbons on a wet basis without condensation or loss of sample.

**C.2 CEM system calibration procedures.** Calibrations are conducted on a daily basis. The following procedures are performed each day of testing:

- (a) Analyzer calibration error (pretest).
- (b) Sampling system bias check (pretest).
- (c) Sampling system bias check (post-test).

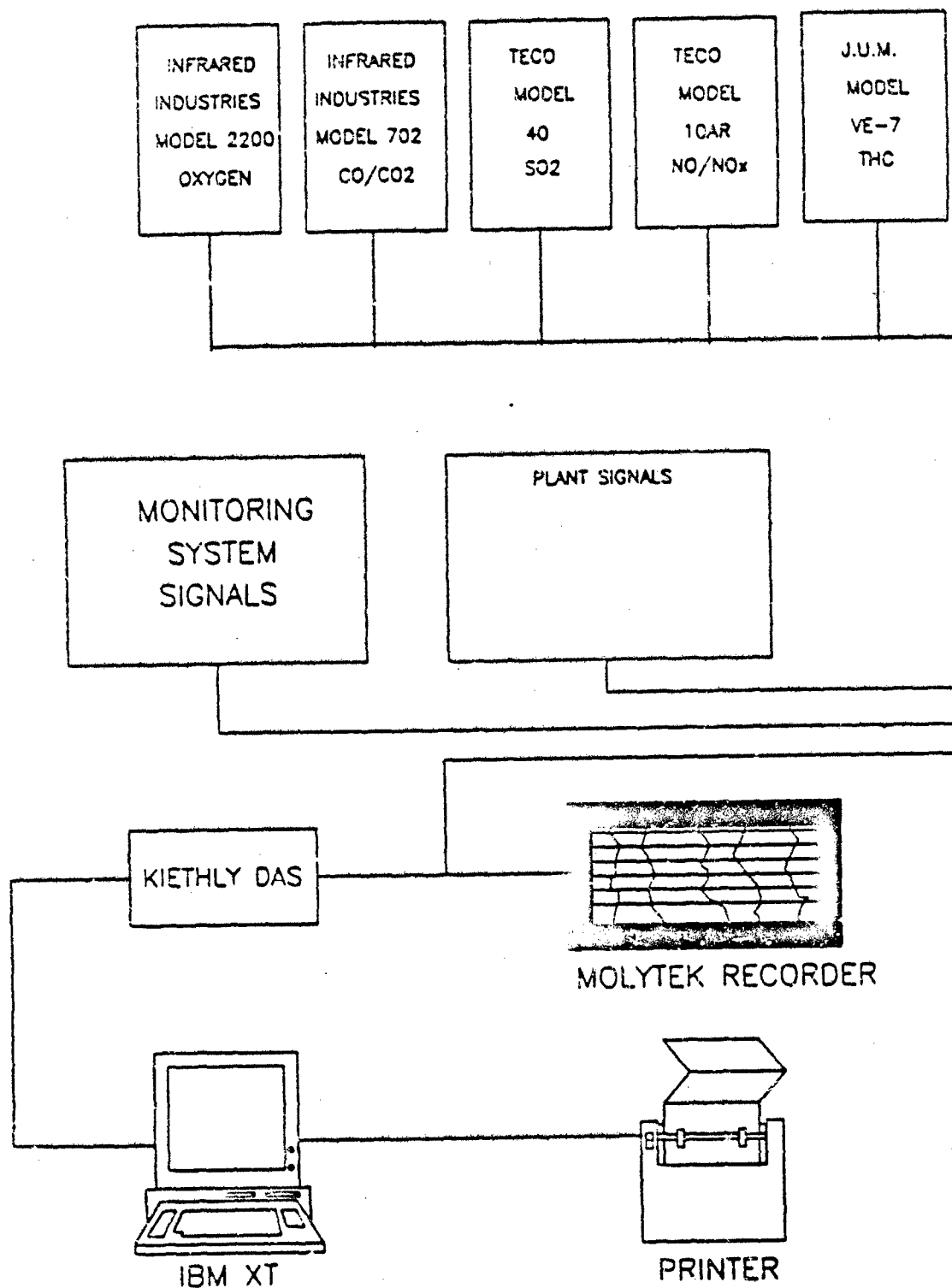


FIGURE C-1. CEM System

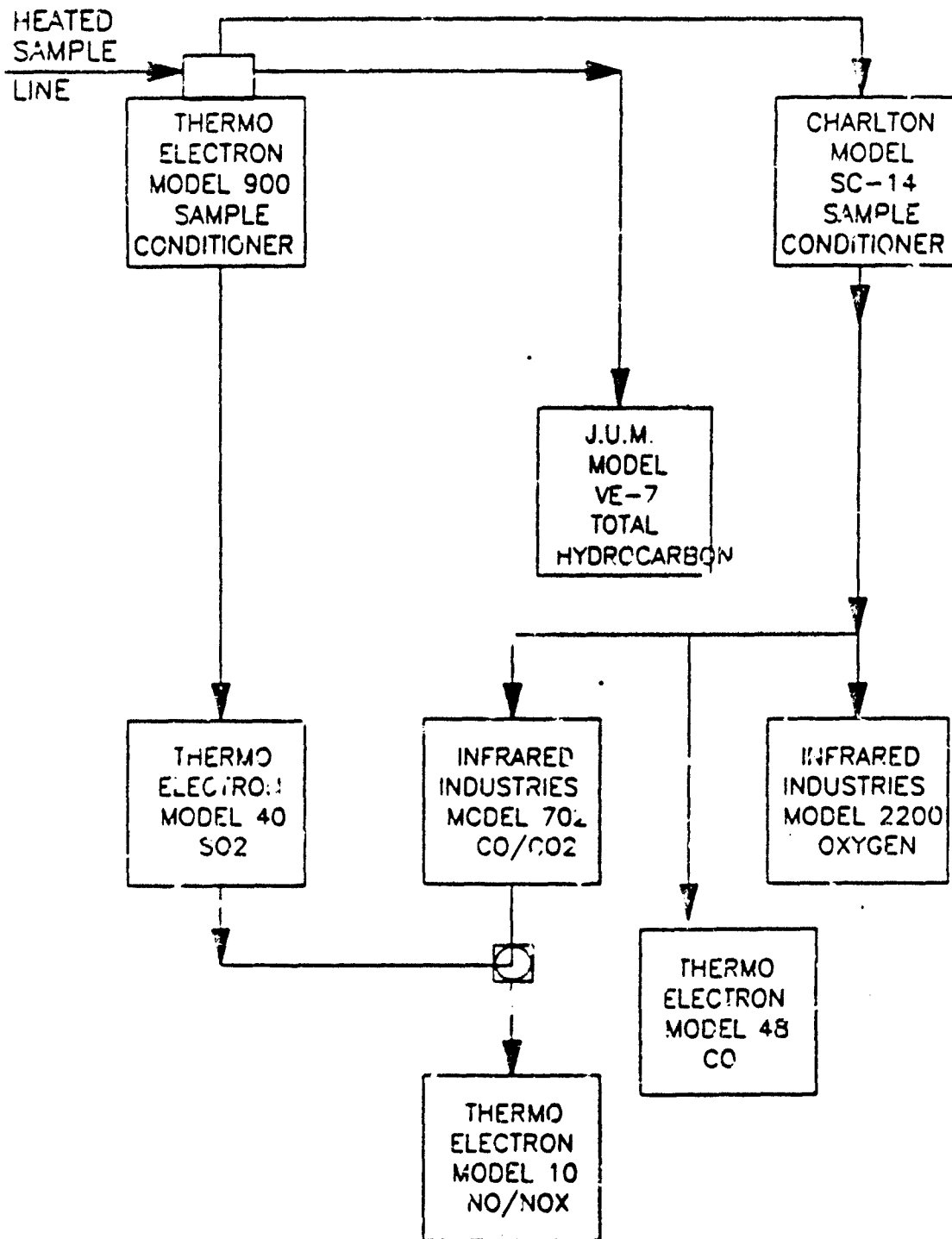


FIGURE C-2. CEM Sample Gas Flow Path

Calibrations used cylinder gas standards prepared according to EPA Protocol 1, where available. All other calibration gases are traceable to National Bureau of Standards (NBS) standards.

C.3 CEM system data collection. Signals from the CEM sampling system are recorded on two devices. Data are available in hard copy from a Molytek strip chart recorder/data logger. In addition, data are recorded in 10-second increments using the Kiethly DAS/IBM PC-XT acquisition system. Data are summarized as one minute averages and are available onsite using the PC-XT system.



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**APPENDIX D**  
**RAW OPERATIONAL DATA SHEETS**

Appendix D presents raw operational data collected from process equipment and test items. For each test run, four types of data sheets are enclosed.

The first data sheet (Data Sheet 1) provides information on the physical characteristics of test items evaluated in each test run. The following information is provided:

- Equipment type.
- Contaminants evaluated.
- Dimensions of test item.
- Initial weight of test item.
- Final weight of test item.
- Type of sample collected (rinsate, wipe or solid).
- An indication of type of contaminant spiked to test item (TNT or ammonium picrate).
- Initial and final contaminant concentration (since these items were not known at the time of testing, these columns are generally left blank).
- Thermocouple number.
- Observations (pre- and post-test).

A schematic of the rail cart is included; locations of each type of test item are provided. The following abbreviations are applicable:

- PB - Powder Box.
- SHR - Steam Heated Riser.
- SSR - Shell Support Rack.
- SHV - Steam Heated Discharge Valve.
- CP - Clay Pipe.
- SM - Ship Mine.
- SP - Steel Pipe.
- AP - Aluminum Pipe.
- 1 - denotes test items designated for post-test sampling and analysis.
- 2 - denotes test items designated as spares; items were sampled for analysis only in the event of field or laboratory contamination.
- 0 - Diameter.
- F - Flush.
- R - Rinsate.
- W - Wipe.
- S - Side (thermocouple location).
- I - Inside (thermocouple location).

For the first few test runs, the procedures used to record data were still being developed; therefore, some of the information provided on the data sheets is not complete (i.e., contaminants evaluated, sample type, initial/final contaminant concentration, and thermocouple number).

The second data sheet (Data Sheet 2) provides information collected from the following process equipment items:

- Main Control Panel
  - Air preheater inlet damper position (H1C-201)
  - Air preheater inlet air flow (PI-202)
  - Air preheater exit gas temperature (TIC-304)
  - Afterburner inlet air temperature (TI-224)
  - Building (Flash Chamber) Pressure (PIC-201)
  - Afterburner exit gas temperature (TIC-324)
- Air Preheater
  - Gas Pressure (PI-303)
  - Burner Pressure (PI-310)
- Afterburner
  - Gas Pressure (PI-323)
  - Burner Pressure (PI-330)
- Propane Gas Supply Tank
  - Tank Capacity Remaining
  - Tank Temperature
  - Line Pressure
  - Line Temperature

The following discharge emissions were monitored by the Continuous Emissions Monitor (CEM) System and recorded by WESTON personnel:

- Air Preheater Discharge
  - Total Hydrocarbons (THC)
- Flash Chamber Discharge
  - Total Hydrocarbons (THC)
- Afterburner Discharge
  - Total Hydrocarbons (THC)
  - Carbon Dioxide (CO)
  - Carbon Monoxide (CO<sub>2</sub>)
  - Oxygen (O<sub>2</sub>)
  - Nitrous Oxides (NO<sub>x</sub>)

The following key of abbreviations is applicable:

- PSIG = Pounds per Square Inch Gauge.
- PPM/V = Parts Per Million based on Volume.
- % = Percentage.

The following information was monitored and recorded by WESTON personnel:

- Dry bulb temperature of ambient air.
- Wet bulb temperature of ambient air.
- Moisture content of ambient air (as determined using a psychrometric chart).

The collection times correspond to real time beginning with 0000 hrs and running through 2300 hrs. A separate data sheet is included for each operational day.

Monitoring data were collected and recorded every hour beginning with the firing of the afterburner and continuing until the flash chamber reached the steady state target temperature. After reaching steady state temperature, personnel were not required to be present on the test site. The team left the site and the system operated automatically. During unmanned operation, no data were recorded (except for data recorded during "spot" checks and CEM system data). Data gaps, therefore, exist in the data sheets.

WESTON personnel recorded notes regarding the operation of the system along the sides of the data sheets. These notes usually reflect times when the system reached steady state, and cases where the system shut down, the air preheater started, etc.

The third data sheet (Data Sheet 3) provides temperatures monitored by thermocouples placed on test items within and various locations in the flash chamber. Collection times correspond to real time beginning with 0030 hours and continuing to 2330 hours. Each thermocouple was tagged with an identification number. The thermocouple number is provided across the top of the data sheet (numbers 1 through 20). The test item and flash chamber location monitored are listed below the thermocouple number (i.e., thermocouple 1 monitored the temperature of the diffuser support, etc.). The location of the thermocouple on the test items is provided and is listed as an (I) for internal surfaces or (S or E) for side and external surface areas.

Following the raw data sheets are computer-generated summary sheets (Data Sheet 4). Two data summary sheets are provided for each test. The first sheet contains data collected from the process equipment; the second sheet contains the temperatures collected from the test items and flash chamber. The elapsed time is provided and represents the total number of hours data were collected during a test period. At the end of each summary sheet are values for the mean, maximum, and minimum of the data over the following three time periods: (1) steady state operation, (2) heatup and steady state operation, and (3) total test operation. The averages generated by the computer were used to generate summary tables in Section 8 of the report.

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TEST RUN 2  
400°F/24 HOURS

1311R2

DATA SHEET 1  
PAGE 1 OF 1

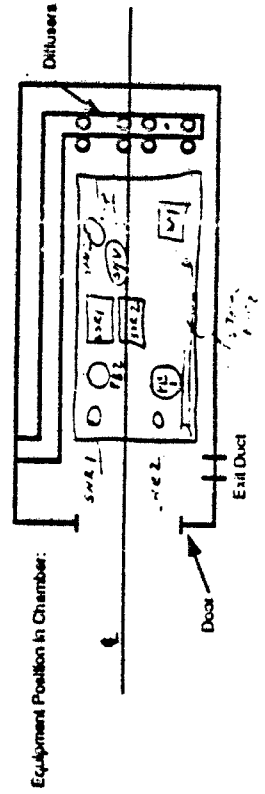
Test Run T2 Date 7-18-89  
 Test Duration 24 hrs Time 12:00 hrs  
 Heat Up Rate 50/hr  
 Flash Chamber Temperature 400 °F

X = INSIDE  
S = OUT

Flash Chamber Interior

Equipment Type	Contaminant(s)	Dimensions L x H x W	Initial Wt. (lbs.)	Final Wt. (lbs.)	Sample Type	Equipment Spike	Initial Concentration	Final Concentration	Thermocouple #	Observations Pre-Test	Post-Test
1. PBI	TNT	16" x 14"	12	12	F	TNT			12.5		
2. PBI	"	15" x 14"	6	6	F				15.1		
3. SHR-1	"	7" x 9"	13	12	-						
4. SHR-2	"	7" x 9"	13	12	-						
5. SSR-1	explosive	36" x 20" x 17"	85	80	W						
6. SSR-2	"	36" x 20" x 17"	87	87	W				11.5		
7. SHV-1	"	33" x 18" x 14"	210	210	-				16.1		
8. SHV-2	"	33" x 18" x 14"	190	190	-				20.1 18.5		
9. CP		25" x 17" x 11"	88	88	-				19.1 17.5		
10. SM			728	731					14.5		
11. SP											
12.											
13.											
14.											
15.											

- 1' DIFFUSER SUMMIT  
 2' REAR FLOW  
 3' ROOF WALL  
 4' FLOW IN TIGHT  
 5' DIFFUSAL  
 6' INLET WALL  
 7' EXIT GAS  
 8' FLOW IN TIGHT  
 9' ROOF



177 8576

182

DATA SHEET 2  
PAGE 1 OF 3

LB 1120 / 11.1A

.0112

Date 24 July 89 Test Number T-2 400°F 24hr test.

Time	Main Period										Propose Tank				Propose Tank				Atmosphere Discharge			
	Atmosphere Temp T-101	Atmosphere Temp T-102	Atmosphere Temp T-103	Atmosphere Temp T-104	Atmosphere Temp T-105	Atmosphere Temp T-106	Atmosphere Temp T-107	Atmosphere Temp T-108	Atmosphere Temp T-109	Atmosphere Temp T-110	Atmosphere Temp T-111	Atmosphere Temp T-112	Atmosphere Temp T-113	Atmosphere Temp T-114	Atmosphere Temp T-115	Atmosphere Temp T-116	Atmosphere Temp T-117	Atmosphere Temp T-118	Atmosphere Temp T-119	Atmosphere Temp T-120	Atmosphere Temp T-121	Atmosphere Temp T-122
0000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0600	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0900	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1600	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1900	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
2400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

0.200 0.200

0.0112

28/32

233

1111

Date 25 July 89 T-2 400°F / 24 hr test.

Time	Main Period						Propane Test			Flash Chamber Discharge			Alkylarmer Discharge		
	Ar Flow Rate SCFH	Ar Flow Rate L/min	Ar Flow Rate m³/hr	Ar Flow Rate m³/min	Ar Flow Rate m³/hr	Ar Flow Rate m³/min	Ar Flow Rate m³/hr	Ar Flow Rate m³/min	Ar Flow Rate m³/hr	Ar Flow Rate m³/min	Ar Flow Rate m³/hr	Ar Flow Rate m³/min	Ar Flow Rate m³/hr	Ar Flow Rate m³/min	Ar Flow Rate m³/hr
0800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0900	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1600	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1700	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1900	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

0800 - Start  
Alkylarmer  
Discharge

0810 - Low Temp Alarm

2040 - High Press Alarm

1430 (1430) Discharge occurs

1730 - 1730

1730 - 1730

1730 - 1730

1730 - 1730

2335 - 24th STACK TEST COMPLETE

Alkylarmer Discharge



7/26/89 T-2 400°F/24 hrs

Q100	Q101	Q102	Q103	Q104	Q105	Q106	Q107	Q108	Q109	Q110	Q111	Q112	Q113	Q114	Q115	Q116	Q117	Q118	Q119	Q120
Adm. 100	Adm. 101	Adm. 102	Adm. 103	Adm. 104	Adm. 105	Adm. 106	Adm. 107	Adm. 108	Adm. 109	Adm. 110	Adm. 111	Adm. 112	Adm. 113	Adm. 114	Adm. 115	Adm. 116	Adm. 117	Adm. 118	Adm. 119	Adm. 120

10/2

Equip.	Key:																				Powder Boxes - PB	Shell Support Rack - SSR	Clay Pipe - CP	Strip Mine - SM	Steam Heated Riser - SHR	Steel Pipe - SP	Aluminum Pipe - AP	Motor with Gear Reducer - M	Steam Heated Discharge Valve - SDV
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20									
0030	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55	55									
0130	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50									
0230																													
0330	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50									
0430																													
0530	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50									
0630	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50									
0730	103	105	111	117	123	129	135	141	147	153	159	165	171	177	183	189	195	201	207	213									
0830	201	203	205	207	209	211	213	215	217	219	221	223	225	227	229	231	233	235	237	239									
0930	301	303	305	307	309	311	313	315	317	319	321	323	325	327	329	331	333	335	337	339									
1030	401	403	405	407	409	411	413	415	417	419	421	423	425	427	429	431	433	435	437	439									
1130	501	503	505	507	509	511	513	515	517	519	521	523	525	527	529	531	533	535	537	539									
1230	601	603	605	607	609	611	613	615	617	619	621	623	625	627	629	631	633	635	637	639									
1330	701	703	705	707	709	711	713	715	717	719	721	723	725	727	729	731	733	735	737	739									
1430	801	803	805	807	809	811	813	815	817	819	821	823	825	827	829	831	833	835	837	839									
1530	901	903	905	907	909	911	913	915	917	919	921	923	925	927	929	931	933	935	937	939									
1630																													
1730	1001	1003	1005	1007	1009	1011	1013	1015	1017	1019	1021	1023	1025	1027	1029	1031	1033	1035	1037	1039									
1830	1101	1103	1105	1107	1109	1111	1113	1115	1117	1119	1121	1123	1125	1127	1129	1131	1133	1135	1137	1139									
1930	1201	1203	1205	1207	1209	1211	1213	1215	1217	1219	1221	1223	1225	1227	1229	1231	1233	1235	1237	1239									
2030	1301	1303	1305	1307	1309	1311	1313	1315	1317	1319	1321	1323	1325	1327	1329	1331	1333	1335	1337	1339									
2130	1401	1403	1405	1407	1409	1411	1413	1415	1417	1419	1421	1423	1425	1427	1429	1431	1433	1435	1437	1439									
2230	1501	1503	1505	1507	1509	1511	1513	1515	1517	1519	1521	1523	1525	1527	1529	1531	1533	1535	1537	1539									
2330	1601	1603	1605	1607	1609	1611	1613	1615	1617	1619	1621	1623	1625	1627	1629	1631	1633	1635	1637	1639									



2

11-Jan-80

DATA SHEET 4  
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Time	T-1		T-2		T-3		T-4		T-5		T-6		T-7		T-8		T-9		T-10		T-11		T-12		T-13		T-14		T-15		T-16		T-17		T-18		T-19		T-20		T-21		T-22		T-23		T-24		T-25		T-26		T-27		T-28		T-29		T-30		T-31		T-32		T-33		T-34		T-35		T-36		T-37		T-38		T-39		T-40		T-41		T-42		T-43		T-44		T-45		T-46		T-47		T-48		T-49		T-50		T-51		T-52		T-53		T-54		T-55		T-56		T-57		T-58		T-59		T-60		T-61		T-62		T-63		T-64		T-65		T-66		T-67		T-68		T-69		T-70		T-71		T-72		T-73		T-74		T-75		T-76		T-77		T-78		T-79		T-80		T-81		T-82		T-83		T-84		T-85		T-86		T-87		T-88		T-89		T-90		T-91		T-92		T-93		T-94		T-95		T-96		T-97		T-98		T-99		T-100		T-101		T-102		T-103		T-104		T-105		T-106		T-107		T-108		T-109		T-110		T-111		T-112		T-113		T-114		T-115		T-116		T-117		T-118		T-119		T-120		T-121		T-122		T-123		T-124		T-125		T-126		T-127		T-128		T-129		T-130		T-131		T-132		T-133		T-134		T-135		T-136		T-137		T-138		T-139		T-140		T-141		T-142		T-143		T-144		T-145		T-146		T-147		T-148		T-149		T-150		T-151		T-152		T-153		T-154		T-155		T-156		T-157		T-158		T-159		T-160		T-161		T-162		T-163		T-164		T-165		T-166		T-167		T-168		T-169		T-170		T-171		T-172		T-173		T-174		T-175		T-176		T-177		T-178		T-179		T-180		T-181		T-182		T-183		T-184		T-185		T-186		T-187		T-188		T-189		T-190		T-191		T-192		T-193		T-194		T-195		T-196		T-197		T-198		T-199		T-200		T-201		T-202		T-203		T-204		T-205		T-206		T-207		T-208		T-209		T-210		T-211		T-212		T-213		T-214		T-215		T-216		T-217		T-218		T-219		T-220		T-221		T-222		T-223		T-224		T-225		T-226		T-227		T-228		T-229		T-230		T-231		T-232		T-233		T-234		T-235		T-236		T-237		T-238		T-239		T-240		T-241		T-242		T-243		T-244		T-245		T-246		T-247		T-248		T-249		T-250		T-251		T-252		T-253		T-254		T-255		T-256		T-257		T-258		T-259		T-260		T-261		T-262		T-263		T-264		T-265		T-266		T-267		T-268		T-269		T-270		T-271		T-272		T-273		T-274		T-275		T-276		T-277		T-278		T-279		T-280		T-281		T-282		T-283		T-284		T-285		T-286		T-287		T-288		T-289		T-290		T-291		T-292		T-293		T-294		T-295		T-296		T-297		T-298		T-299		T-300		T-301		T-302		T-303		T-304		T-305		T-306		T-307		T-308		T-309		T-310		T-311		T-312		T-313		T-314		T-315		T-316		T-317		T-318		T-319		T-320		T-321		T-322		T-323		T-324		T-325		T-326		T-327		T-328		T-329		T-330		T-331		T-332		T-333		T-334		T-335		T-336		T-337		T-338		T-339		T-340		T-341		T-342		T-343		T-344		T-345		T-346		T-347		T-348		T-349		T-350		T-351		T-352		T-353		T-354		T-355		T-356		T-357		T-358		T-359		T-360		T-361		T-362		T-363		T-364		T-365		T-366		T-367		T-368		T-369		T-370		T-371		T-372		T-373		T-374		T-375		T-376		T-377		T-378		T-379		T-380		T-381		T-382		T-383		T-384		T-385		T-386		T-387		T-388		T-389		T-390		T-391		T-392		T-393		T-394		T-395		T-396		T-397		T-398		T-399		T-400		T-401		T-402		T-403		T-404		T-405		T-406		T-407		T-408		T-409		T-410		T-411		T-412		T-413		T-414		T-415		T-416		T-417		T-418		T-419		T-420		T-421		T-422		T-423		T-424		T-425		T-426		T-427		T-428		T-429		T-430		T-431		T-432		T-433		T-434		T-435		T-436		T-437		T-438		T-439		T-44
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Tank Number		T-1		T-2		T-3		T-4		T-5		T-6		T-7		T-8		T-9		T-10		T-11		T-12		T-13		T-14		T-15		T-16		T-17		T-18		T-19		T-20		T-21		T-22		T-23		T-24		T-25		T-26		T-27		T-28		T-29		T-30		T-31		T-32		T-33		T-34		T-35		T-36		T-37		T-38		T-39		T-40		T-41		T-42		T-43		T-44		T-45		T-46		T-47		T-48		T-49		T-50		T-51		T-52		T-53		T-54		T-55		T-56		T-57		T-58		T-59		T-60		T-61		T-62		T-63		T-64		T-65		T-66		T-67		T-68		T-69		T-70		T-71		T-72		T-73		T-74		T-75		T-76		T-77		T-78		T-79		T-80		T-81		T-82		T-83		T-84		T-85		T-86		T-87		T-88		T-89		T-90		T-91		T-92		T-93		T-94		T-95		T-96		T-97		T-98		T-99		T-100																																																																																																																																										
Temperature	Pressure	Flow	Level	Height	Width	Depth	Volume	Weight	Force	Energy	Power	Speed	Acceleration	Velocity	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber	Frequency	Wavelength	Amplitude	Phase	Polarization	Intensity	Flux	Current	Voltage	Resistance	Capacitance	Inductance	Conductance	Permittivity	Permeability	Refractive Index	Optical Density	Wavenumber

DATA SHEET 4 OF 4  
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PAGE 6

[illegible]

July 1990  
Revision: Final

TEST RUN 3  
500°F/36 HOURS

(13)

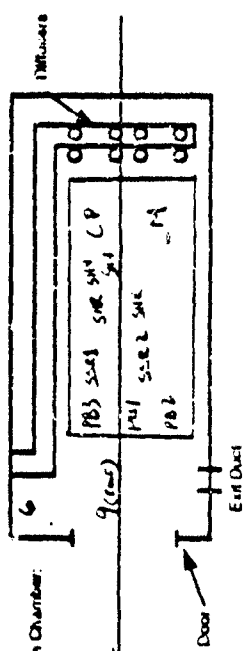
DATA SHEET 1  
PAGE 1 OF 2

Test Run T3  
Test Duration 362 HRS  
Head Up Run 500 OF  
Flash Chamber Temperature 500 OF

Flash Chamber Volume

Equipment Type	Coordinates	Dimensions L x H x W	Initial Wt (g)	Final Wt (g)	Peak Sample Type	Equipment Spilled	Initial Concentration	Final Concentration	Thermocouple #	Pipe Test	Observations
1. TB	TNT	5.5 x 4.1 x 1.1	10	10							
2. PB1		5.5 x 4.1 x 1.1	10	10		10g					
3. PB2		5.5 x 4.1 x 1.1	10	10		10g					
4. SH1		5.5 x 4.1 x 1.1	11	11		10g					
5. SH2		5.5 x 4.1 x 1.1	11	11		10g					
6. SH3		5.5 x 4.1 x 1.1	11	11		10g					
7. SH4		5.5 x 4.1 x 1.1	11	11		10g					
8. SH5		5.5 x 4.1 x 1.1	11	11		10g					
9. SH6		5.5 x 4.1 x 1.1	11	11		10g					
10. SH7		5.5 x 4.1 x 1.1	11	11		10g					
11. SH8		5.5 x 4.1 x 1.1	11	11		10g					
12. SH9		5.5 x 4.1 x 1.1	11	11		10g					
13. SH10		5.5 x 4.1 x 1.1	11	11		10g					
14. SH11		5.5 x 4.1 x 1.1	11	11		10g					
15. SH12		5.5 x 4.1 x 1.1	11	11		10g					
16. SH13		5.5 x 4.1 x 1.1	11	11		10g					
17. SH14		5.5 x 4.1 x 1.1	11	11		10g					
18. SH15		5.5 x 4.1 x 1.1	11	11		10g					
19. SH16		5.5 x 4.1 x 1.1	11	11		10g					
20. SH17		5.5 x 4.1 x 1.1	11	11		10g					
21. SH18		5.5 x 4.1 x 1.1	11	11		10g					
22. SH19		5.5 x 4.1 x 1.1	11	11		10g					
23. SH20		5.5 x 4.1 x 1.1	11	11		10g					
24. SH21		5.5 x 4.1 x 1.1	11	11		10g					
25. SH22		5.5 x 4.1 x 1.1	11	11		10g					
26. SH23		5.5 x 4.1 x 1.1	11	11		10g					
27. SH24		5.5 x 4.1 x 1.1	11	11		10g					
28. SH25		5.5 x 4.1 x 1.1	11	11		10g					
29. SH26		5.5 x 4.1 x 1.1	11	11		10g					
30. SH27		5.5 x 4.1 x 1.1	11	11		10g					
31. SH28		5.5 x 4.1 x 1.1	11	11		10g					
32. SH29		5.5 x 4.1 x 1.1	11	11		10g					
33. SH30		5.5 x 4.1 x 1.1	11	11		10g					
34. SH31		5.5 x 4.1 x 1.1	11	11		10g					
35. SH32		5.5 x 4.1 x 1.1	11	11		10g					
36. SH33		5.5 x 4.1 x 1.1	11	11		10g					
37. SH34		5.5 x 4.1 x 1.1	11	11		10g					
38. SH35		5.5 x 4.1 x 1.1	11	11		10g					
39. SH36		5.5 x 4.1 x 1.1	11	11		10g					
40. SH37		5.5 x 4.1 x 1.1	11	11		10g					
41. SH38		5.5 x 4.1 x 1.1	11	11		10g					
42. SH39		5.5 x 4.1 x 1.1	11	11		10g					
43. SH40		5.5 x 4.1 x 1.1	11	11		10g					
44. SH41		5.5 x 4.1 x 1.1	11	11		10g					
45. SH42		5.5 x 4.1 x 1.1	11	11		10g					
46. SH43		5.5 x 4.1 x 1.1	11	11		10g					
47. SH44		5.5 x 4.1 x 1.1	11	11		10g					
48. SH45		5.5 x 4.1 x 1.1	11	11		10g					
49. SH46		5.5 x 4.1 x 1.1	11	11		10g					
50. SH47		5.5 x 4.1 x 1.1	11	11		10g					
51. SH48		5.5 x 4.1 x 1.1	11	11		10g					
52. SH49		5.5 x 4.1 x 1.1	11	11		10g					
53. SH50		5.5 x 4.1 x 1.1	11	11		10g					
54. SH51		5.5 x 4.1 x 1.1	11	11		10g					
55. SH52		5.5 x 4.1 x 1.1	11	11		10g					
56. SH53		5.5 x 4.1 x 1.1	11	11		10g					
57. SH54		5.5 x 4.1 x 1.1	11	11		10g					
58. SH55		5.5 x 4.1 x 1.1	11	11		10g					
59. SH56		5.5 x 4.1 x 1.1	11	11		10g					
60. SH57		5.5 x 4.1 x 1.1	11	11		10g					
61. SH58		5.5 x 4.1 x 1.1	11	11		10g					
62. SH59		5.5 x 4.1 x 1.1	11	11		10g					
63. SH60		5.5 x 4.1 x 1.1	11	11		10g					
64. SH61		5.5 x 4.1 x 1.1	11	11		10g					
65. SH62		5.5 x 4.1 x 1.1	11	11		10g					
66. SH63		5.5 x 4.1 x 1.1	11	11		10g					
67. SH64		5.5 x 4.1 x 1.1	11	11		10g					
68. SH65		5.5 x 4.1 x 1.1	11	11		10g					
69. SH66		5.5 x 4.1 x 1.1	11	11		10g					
70. SH67		5.5 x 4.1 x 1.1	11	11		10g					
71. SH68		5.5 x 4.1 x 1.1	11	11		10g					
72. SH69		5.5 x 4.1 x 1.1	11	11		10g					
73. SH70		5.5 x 4.1 x 1.1	11	11		10g					
74. SH71		5.5 x 4.1 x 1.1	11	11		10g					
75. SH72		5.5 x 4.1 x 1.1	11	11		10g					
76. SH73		5.5 x 4.1 x 1.1	11	11		10g					
77. SH74		5.5 x 4.1 x 1.1	11	11		10g					
78. SH75		5.5 x 4.1 x 1.1	11	11		10g					
79. SH76		5.5 x 4.1 x 1.1	11	11		10g					
80. SH77		5.5 x 4.1 x 1.1	11	11		10g					
81. SH78		5.5 x 4.1 x 1.1	11	11		10g					
82. SH79		5.5 x 4.1 x 1.1	11	11		10g					
83. SH80		5.5 x 4.1 x 1.1	11	11		10g					
84. SH81		5.5 x 4.1 x 1.1	11	11		10g					
85. SH82		5.5 x 4.1 x 1.1	11	11		10g					
86. SH83		5.5 x 4.1 x 1.1	11	11		10g					
87. SH84		5.5 x 4.1 x 1.1	11	11		10g					
88. SH85		5.5 x 4.1 x 1.1	11	11		10g					
89. SH86		5.5 x 4.1 x 1.1	11	11		10g					
90. SH87		5.5 x 4.1 x 1.1	11	11		10g					
91. SH88		5.5 x 4.1 x 1.1	11	11		10g					
92. SH89		5.5 x 4.1 x 1.1	11	11		10g					
93. SH90		5.5 x 4.1 x 1.1	11	11		10g					
94. SH91		5.5 x 4.1 x 1.1	11	11		10g					
95. SH92		5.5 x 4.1 x 1.1	11	11		10g					
96. SH93		5.5 x 4.1 x 1.1	11	11		10g					
97. SH94		5.5 x 4.1 x 1.1	11	11		10g					
98. SH95		5.5 x 4.1 x 1.1	11	11		10g					
99. SH96		5.5 x 4.1 x 1.1	11	11		10g					
100. SH97		5.5 x 4.1 x 1.1	11	11		10g					
101. SH98		5.5 x 4.1 x 1.1	11	11		10g					
102. SH99		5.5 x 4.1 x 1.1	11	11		10g					
103. SH100		5.5 x 4.1 x 1.1	11	11		10g					

Chain wt = 7 lbs  
Clutch wt = 2 lbs



103. Chain wt = 7.250 (SHE, SHE, SHE)  
and up to 103.5 wt = 2.160 (SHE)

\* NOTE: SCALE WAS OFF, due to a MISSING LOCK NUT. FINAL WT. MAY NOT BE 100% ACCURATE

Test Run T3 Date 7/15/89  
Test Duration 36 hours Time

Flash Chamber Temperature 500°F

Equipment Type	Concentration(s)	Concentration L H W	Initial Vol (cc)	Final Vol (cc)	Final Wt (cc)	Pic Sample Type	Equipment Spiked	Initial Concentration	Final Concentration	Thermocouple #	Pre-Test	Post-Test
1. PB	TNT	15% d.i.	10	10	10	N	-				70% d.i.	Quench
2. PB1		15% d.i.	10	10	10	F	10%				3rd d.i.	
3. PB2		15% d.i.	10	10	10	F	10%			10	3rd d.i.	
4. SHR1		7% d.i.	11	12	12	F	10%			105 / 125	3rd d.i.	
5. SHR2		15% d.i.	11	12	12	F	10%				3rd d.i.	
6. SR1		15% d.i.	70	70	70	N/W	10%				3rd d.i.	
7. SR2		15% d.i.	70	70	70	N/W	10%				3rd d.i.	
8. SR3		15% d.i.	90	90	90	N/W	10%			125	3rd d.i.	
9. SR4		15% d.i.	730	730	730	N/W	10%			125	3rd d.i.	
10. SHV1		15% d.i.	250	250	250	F	10%			205	3rd d.i.	
11. SHV2		15% d.i.	240	240	240	F	10%			8	3rd d.i.	
12. SHV3		15% d.i.	240	240	240	F	10%			11	3rd d.i.	
13. SHV4		15% d.i.	240	240	240	F	10%			12	3rd d.i.	
14. SHV5		15% d.i.	240	240	240	F	10%			13	3rd d.i.	
15. SHV6		15% d.i.	240	240	240	F	10%			14	3rd d.i.	

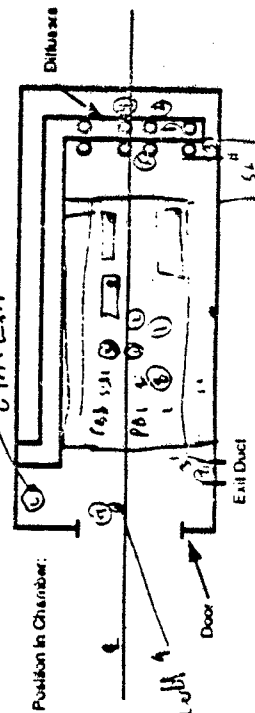
handle packed  
in (keto)

201.2

190-  
Flax. 12. 2. 11

Stylidium lineare

Chain Weight = 7 lbs



Well Man High  
Differ Equipmen  
Violet

Flora to study  
11/06/3111  
Wan Wan

1912

*[Handwritten signature]*

1000

100

DATA SHEET 2  
PAGE 1 OF 4

Date 7/16/89 (Sun) Test Number T3

Blue, Green &  
- 0.2 MUMMATIC

1055 hrs. START  
AFTERBURST  
1100 - System down  
1110 - START UP

System down @ 1145 for  
15 minutes (low to fuel in  
Jettisoned C49 to SLS.

2345 5.0. Temp  
@ 1946 5.0 - Wind  
to start A.H. & get  
low-low big pressure. after  
shut down system.

Time	Main Panel						Air			After Burner			Flash Chamber Discharge			Afterburner Discharge		
	HC-201	HC-202	HC-203	HC-204	HC-205	HC-206	HC-207	HC-208	HC-209	HC-210	HC-211	HC-212	HC-213	HC-214	HC-215	HC-216	HC-217	HC-218
0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0600	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0700	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0900	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1110	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1120	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1130	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1140	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1150	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1600	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1700	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1900	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

Low pressure  
1100 - 1150

To Start

Note: when starting



NOTES:

0030 - have been at  
study state a total  
of 12 hrs. during  
any missteps 36 hr.  
should be at 2130  
on Wed. 7/18/89.

will Sunday morning

1430 since test #3  
begins

What continue to state

2151 - 2206  
out of town - 2206  
36 hrs of study state  
to be at 2130 per  
Cosmo & Johnson.

Date 7-18-89 (Tues.) Test Number T3

Time	Main Period				Air Temp PSI	Amb. Temp PSI	Propane Test			CEM			
	At 1000 PSI	At 1000 PSI	At 1000 PSI	At 1000 PSI			At 1000 PSI	At 1000 PSI	At 1000 PSI	Flash Chamber Discharge	At Heater Discharge	Flash Chamber Discharge	Airburner Discharge
0000	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0100	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0200	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0300	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0400	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0500	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0600	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0700	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0800	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
0900	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1000	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1100	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1200	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1300	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1400	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1500	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1600	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1700	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1800	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
1900	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
2000	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
2100	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
2200	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0
2300	67.3	67.3	67.3	67.3	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0	10.0

2135 - Start Test 3 ends

2152 → A.H. burner shut down, leave fan running for cool down  
reduce A.H. tank dumper setting

Date 7/12/89 Test Number T3 Codman

Time	Main Panel				Air Handling				After Burner			Propose Test			Propose Test			Flash Chamber Discharge			Afterburner Discharge		
	MC-201	MC-202	MC-203	MC-204	MC-205	MC-206	MC-207	MC-208	MC-209	MC-210	MC-211	MC-212	MC-213	MC-214	MC-215	MC-216	MC-217	MC-218	MC-219	MC-220	MC-221	MC-222	MC-223
6:00																							
7:00																							
8:00																							
9:00																							
10:00																							
11:00																							
12:00																							
13:00																							
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16:00																							
17:00																							
18:00																							
19:00																							
20:00																							
21:00																							
22:00																							
23:00																							

721

1320 - Level

512



13

Chapman / #	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030 - O	44	105	104	120	109	120	120	113	113	104	117	113	111	115	115	117	111	42	117	117										
0130	348	132	238	326	244	276	276	177	259	175	152	159	170	130	131	122	153	153	203	137										
0230	468	165	331	148	457	356	378	258	137	244	165	165	224	204	196	167	189	167	200	310										
0330	465	171	352	162	424	350	350	276	341	278	182	110	203	245	242	214	249	597	245	331										
0430	443	309	350	172	416	354	348	256	337	291	192	197	279	268	265	250	277	395	269	346										
0530	514	226	399	183	457	406	400	332	322	337	208	215	327	276	272	278	277	262	200	395										
0630	519	251	449	198	500	424	416	467	405	364	223	224	351	333	321	216	349	477	335	418										
0730	446	250	401	201	465	394	402	345	384	355	221	224	320	323	328	247	454	454	133	390										
0830	580	273	453	213	504	456	450	512	478	350	244	254	381	354	355	341	540	538	27	424										
0930	211	310	515	241	607	515	502	444	445	446	264	261	440	440	440	440	542	542	477	500										
1030	644	337	535	257	605	504	514	544	515	462	272	245	444	444	444	444	540	540	697	430	500									
1130	673	340	478	271	626	524	523	476	530	474	245	245	475	458	458	440	501	611	474	350										
1230	603	302	502	292	626	544	527	445	440	441	311	309	445	473	473	482	510	631	445	500										
1330	615	346	504	296	631	553	511	441	510	441	317	317	441	441	441	441	513	513	602	502	500									
1430	680	410	569	321	637	627	540	400	541	441	318	318	441	441	441	441	513	513	620	510	575									
1530	618	410	541	325	637	637	541	401	541	441	314	314	441	441	441	441	513	513	620	510	575									
1630	655	411	568	322	617	655	547	503	539	501	320	320	441	441	441	441	513	513	620	510	575									
1730	649	421	560	310	613	613	543	400	531	441	315	315	441	441	441	441	513	513	620	510	575									
1830	650	421	551	344	610	533	535	449	535	445	345	345	441	441	441	441	513	513	620	510	575									
1930	452	204	420	335	493	343	410	417	432	352	322	337	535	442	442	442	472	411	472	410										
2030	455	338	426	295	435	376	427	358	300	301	302	301	382	381	380	415	401	440	408	414										
2130	515	244	472	301	544	480	471	411	481	350	346	346	401	346	342	441	411	514	417	440										
2230	641	216	527	302	607	502	502	451	518	471	327	335	441	441	441	441	513	513	620	510	575									
2330	640	594	330	337	601	517	518	478	519	478	351	346	445	440	457	458	486	600	477	544										

DATA SHEET 3

Page 2 of 3

S = SURFACE  
I = INTERIOR

Date: 7/18/07

Tail: #T3

026 TR4 2 3 1 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21

Channel #	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Equip.																														
0030	411	412	519	348	307	509	535	481	529	501	310	315	481	474	471	478	478	599	484	599										
0130	636	470	516	353	611	523	525	490	505	429	342	361	780	478	479	485	502	606	492	553										
0230	640	425	550	359	606	525	535	485	532	494	349	367	487	481	483	470	507	600	497	555										
0330	638	424	577	367	606	538	535	483	529	510	351	372	497	487	488	496	517	510	502	558										
0430	634	433	552	370	600	538	535	500	530	497	353	374	495	482	488	494	512	601	504	558										
0530	637	437	550	372	605	535	535	491	531	505	355	376	491	491	491	501	513	611	506	560										
0630	636	431	550	374	603	539	540	502	533	502	357	381	492	493	493	504	515	607	507	561										
0730	632	441	555	376	611	537	537	502	535	506	361	382	497	494	494	504	514	618	507	564										
0830	644	448	555	374	600	542	541	500	532	514	364	385	491	497	496	507	520	616	512	515										
0930	647	453	553	374	591	531	531	504	533	516	364	388	491	491	498	508	521	621	513	519										
1030	645	452	552	382	603	534	534	506	535	516	369	389	491	497	497	504	522	604	512	521										
1130	640	454	551	380	598	533	533	500	532	510	360	380	492	496	495	508	521	604	511	524										
1230	640	455	552	381	599	534	534	501	533	511	369	380	496	495	495	507	518	605	510	525										
1330	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
1430	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
1530	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
1630	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
1730	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
1830	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
1930	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
2030	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
2130	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
2230	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										
2330	640	455	551	381	597	533	533	501	532	510	369	380	496	495	495	507	518	605	510	525										

Powder Boxes - PB

Steel Support Rack - SSR

Clay Pipe - CP

Slip Line - SL

Steam Heated Riser - SHR

Steel Pipe - SP

Aluminum Pipe - AP

Motor with Gear Reducer - M

Steam Heated Discharge Valve - SDV

1120101

Page 3 of 2

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Key:	
Equip.	108																															Powder Boxes - PB
	108																															Shelf Support Rack - SSR
0030	49																															Clay Pipe - CP
0130	49																															Ship Mine - SM
0230	50																															Steam Heated Riser - SHR
0330	51																															Steel Pipe - SP
0430	51																															Aluminum Pipe - AP
0530	52																															Motor with Gear Reducer - M
0630	54																															Steam Heated Discharge Valve - SDV
0730	55																															
0830	56																															
0930	57																															
1030	58																															
1130																																
1230																																
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1730																																
1830																																
1930																																
2030																																
2130																																
2230																																
2330																																

77 8576

0400

177 857c

[illegible]



[illegible]







[illegible]

July 1990  
Revision: Final

TEST RUN 5  
500°F/24 HOURS

1311R2

DATA SHEET 1 OF 1  
PAGE 1

DATA SHEET 1 OF 2  
PAGE 1

68/2/8 S-1 159 40 PVR

Date 7/25/82  
Time 2:10

Test T-5 24 hrs

Test Duration 24 hrs  
 Head Up Angle 4

Heat Up Rate 7  
Flash Chamber Temperature 500 °F

Flash Chamber Inventory -

Equipment Type	Contaminant(s)	Dimensions L H W	Initial Wt (lbs.)	Final Wt (lbs.)	Sample Type	Equipment Spilled	Initial Contaminant Concentration	Final Contaminant Concentration	Thermocouple #	Pre-Test	Post-Test	Observations
1 PB 1		15" x 18" x 18"	5	6					12	No L.D. High Max. Bear size sample.		
2 PB 2		15" x 18" x 18"	8	10								
3 SHR 1		7" x 9" x 11"	11	12					151	125		
4 SHR 2		7" x 9" x 11"	10	12								
5 SHR 1		15" x 18" x 18"	86	86.5								
6 SHR 2		15" x 18" x 18"	84	85.5								
7 SM			725	722					171	165		
8 CP			100	85.5					171	175		
9 Motor (w)			932	919					171	175		
10 1" x 1" x 1"									171	175		
11 Wall (w)									171	175		
12 Wall (w)									171	175		
13 Roof									171	175		
14 1" x 1" x 1"									171	175		
15									171	175		

oil coming out of  
molex clean plug.

- SAMPLING  
Template size = 5" x 5"
- Post test T-S more soak - ~~200~~ 104 Liters of Acetonitrile placed in 55 gal drum. Drum HT = 35"
- solvent depth = 24"

Powder Box #1 - No Lip on top of Box. Lid does not close all the way.

Powder Box #2 - Rounded lip. Lid does not close all the way.

Steam Heated Riser #1 - Good Shape, Both handles in tact.

SR #2 - Orange Paint on side of riser. Good Shape.

Shell Support Riser #1 - Larger in size. Several stained areas on bottom of Rack

SR #2 - Smaller in height than SR #1. Minimal bottom staining

Steel Pipe - 6 ft. in length. Black Color. Purchased in West Chester, PA.

Clay Pipe - Franco and Bacon - 8" x 11 1/2" - large amt of dirt



3" x 9" x 30 1/2" of pipe

Ship Mine - Green in color. Same as all other ship mines

Date 28 July 81 Co. Test Number T-5

Time	Main Panel								Air Preheater		After Burner		Propane Tank				Propane Tank		Flash Chamber Discharge		Afterburner Discharge			
	As Heater Vent Discharge HC-201	As Heater Vent Air Flow P-202	As Heater Temperature TC-204	T.O. Fuel Air T-224	Bag Pressure PT-221	Exhaust Air Valve Position HC-221	T.O. Temperature TC-224	Exhaust Air Valve Position HC-221	Dry Bulk Temperature T-204	Wet Bulk Temperature T-205	Gas Pressure P-203	Burner Pressure P-210	Gas Pressure P-223	Burner Pressure P-224	Altitude PS-2	Capacity	Low Temperature	Low Pressure	Low Temperature	HC	CO	CO <sub>2</sub>	O <sub>2</sub>	NO <sub>x</sub>
00:00																								
01:00																								
02:00																								
03:00																								
04:00																								
05:00																								
06:00																								
07:00																								
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21:00																								
22:00																								
23:00																								
24:00																								

Sample T-5  
Date 7/29/89 Test Number

Time	Main Panel										Propose Tank				Propose Tank				Afterburner Discharge			
	At Temp Fuel Gauge	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow	At Temp Fuel Air Flow
0000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0600	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0700	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
0900	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1500	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1600	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1700	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1800	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
1900	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2000	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2100	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2200	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2300	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0
2400	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0	0

0940 - START PREHEAT  
1045  
1145  
1730 - STEADY STATE

Date 7/30/89 Summary Test Number TS

Time	Main Period										Air			Alar.			Propane Tank			Air Header Discharge			Flash Chamber Discharge			Afterburner Discharge		
	Ar Header Fuel Air Flow MFC-201	Ar Header Fuel Air Flow P-202	Ar Header Temp TIC-201	Ar Header Temp TIC-202	Ar Header Temp TIC-203	Ar Header Temp TIC-204	Ar Header Temp TIC-205	Ar Header Temp TIC-206	Ar Header Temp TIC-207	Ar Header Temp TIC-208	Ar Pressure P-201	Ar Pressure P-202	Ar Pressure P-203	Ar Pressure P-204	Ar Pressure P-205	Ar Pressure P-206	Ar Pressure P-207	Ar Pressure P-208	Ar Pressure P-209	Ar Pressure P-210	Ar Pressure P-211	Ar Pressure P-212	Ar Pressure P-213	Ar Pressure P-214	Ar Pressure P-215	Ar Pressure P-216	Ar Pressure P-217	Ar Pressure P-218
0000	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0100	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0200	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0300	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0400	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0500	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0600	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0700	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0800	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
0900	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1000	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1100	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1200	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1300	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1400	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1500	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1600	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1700	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1800	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
1900	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
2000	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
2100	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
2200	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
2300	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5
2400	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5	71.5

MASS WOODMAN

0130 - END STACK  
TEST 2

STACK TEST #3 Begins  
at 1215 hrs

1715 - STACK TEST #3  
COMPLETE.

1730 - END T-5.

DEGIN COOL DOWN

7/31/89 Afterburner shot down @ 0130 hrs. Mayhem on site @ 0245 hrs to attempt a restart of T.O. system would NOT START.

- 0940, 7/31/89 - afterburner system running

15

Afterburner RE-LIT AT 910AM AFTER SHUTTING DOWN

DATA SHEET 2  
PAGE 4 OF 5

TEST NUMBER 15 (Cool Down)

Time	Main Panel										Proposed Test				Proposed Test				Afterburner Discharge			
	Ar Heater Fuel Control P-201	Ar Heater Fuel Air Flow P-202	Ar Heater Temperature T-204	10.0 Air Ar Temperature T-204	10.0 Air Ar Pressure P-201	10.0 Air Ar Pressure P-202	10.0 Air Ar Pressure P-203	10.0 Air Ar Pressure P-204	10.0 Air Ar Pressure P-205	10.0 Air Ar Pressure P-206	Ar Heater Discharge P-207	Ar Heater Discharge P-208	Ar Heater Discharge P-209	Ar Heater Discharge P-210	Flash Chamber Discharge P-211	Flash Chamber Discharge P-212	Flash Chamber Discharge P-213	Flash Chamber Discharge P-214	Ar Heater Discharge P-215	Ar Heater Discharge P-216	Ar Heater Discharge P-217	Ar Heater Discharge P-218
0000																						
0100																						
0200																						
0300																						
0400																						
0500																						
0600																						
0700																						
0800																						
0900																						
1000	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
1100	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
1200																						
1300																						
1400																						
1500	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
1600	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
1700	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
1800	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
1900	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
2000	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
2100	0.1	0.1	31	112	0.13	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11	0.11
2200																						
2300																						

100 T.O. at 5000 ft  
1000 ft at 3114 ft.

REC'D 920000  
PROP. 120000  
7/10/67

RECEIVED 170000  
830 PM  
1200 PM TO 11  
845 PM.



Time	Main Panel										Propane Tank				Afterburner Discharge			
	HC-21 Air Exhaust Test Discharge	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	HC-21 Air Exhaust Test Air Flow	Propane Tank Temp	Propane Tank Pressure	Propane Tank Level	Propane Tank Level	Flash Chamber Discharge THC	Flash Chamber Discharge THC	Flash Chamber Discharge THC	Flash Chamber Discharge THC
00:00																		
01:00																		
02:00																		
03:00																		
04:00																		
05:00																		
06:00																		
07:00																		
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23:00																		

Date 8/1/89 Test Number TS

TS

DATA SHEET 3

Page 1 of 4

27 July 84 Sub. by T-5 3005 / 20 1000

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030																														
0130																														
0230																														
0330																														
0430																														
0530																														
0630																														
0730																														
0830																														
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1430																														
1530																														
1630																														
1730																														
1830																														
1930																														
2030																														
2130																														
2230																														
2330																														

Key:

Powder  
Boxes - PB

Shell Support  
Rack - SSR

Clay Pipe  
- CP

Ship Mine  
- SM

Steam  
Heated  
Riser - SHR

Steel Pipe  
- SP

Aluminum  
Pipe  
- AP

Motor with  
Gear  
Reducer  
- M

Steam  
Heated  
Discharge  
Valve - SDV

Equip.		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
	PB																														
0030		571	572	573	574	575	576	577	578	579	580	581	582	583	584	585	586	587	588	589	590	591	592	593	594	595	596	597	598	599	600
0130		611	612	613	614	615	616	617	618	619	620	621	622	623	624	625	626	627	628	629	630	631	632	633	634	635	636	637	638	639	640
0230																															
0330		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
0430		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
0530		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
0630		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
0730		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
0830		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
0930		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
1030		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
1130		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
1230		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
1330		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139
1430		110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131								

**177 8576**

2/3/87 15

DATA SHEET 3  
Page 3 of 4

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
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0130																															
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1130																															
1230																															
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1430																															
1530	170	187	203	210	179	191	168	194	170	217	190	192	180	189	190	196	193	189	192	186											
1630	180	180	204	204	177	184	167	192	167	195	174	190	187	182	187	173	172	187	187	187											
1730	183	184	198	206	175	176	166	167	185	212	192	187	185	180	185	191	187	184	187	182											
1830	183	182	196	205	173	177	162	187	183	207	190	185	183	187	183	187	187	183	185	180											
1930	185	183	197	205	177	184	163	166	181	207	188	184	181	177	181	187	185	181	184	178											
2030	178	179	193	201	169	180	160	173	178	204	186	191	179	175	180	183	183	180	182	178											
2130																															
2230																															
2330																															

Key:	Powder Boxes - PB	Shell Support Rack - SSR	Clay Pipe - CP	Ship Mine - SM	Steam Heated Riser - SHR	Steel Pipe - SP	Aluminum Pipe - AP	Motor with Gear Reducer - M	Steam Heated Discharge Valve - SDV
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Key:

Powder Boxes - PB  
Shell Support Rack - SSR  
Clay Pipe - CP  
Ship Mine - SM  
Steam Heated Riser - SHR  
Steel Pipe - SP  
Aluminum Pipe - AP  
Motor with Gear Reducer - M  
Steam Heated Discharge Valve - SDV

		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Equip.	PB																														
0030																															
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1030		35	37	151	165	125	124	115	131	128	135	134	124	121	115	123	123	124	124	124	125	125									
1130		122	120	120	122	121	121	115	132	127	131	121	121	121	121	121	121	121	121	121	121	121									
1230																															
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2130																															
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2330																															

[illegible]

Test Run		T-1		T-2		T-3		T-4		T-5		T-6		T-7		T-8		T-9		T-10		T-11		T-12		T-13		T-14		T-15		T-16		T-17		T-18		T-19		T-20		T-21		T-22		T-23		T-24		T-25		T-26		T-27		T-28		T-29		T-30		T-31		T-32		T-33		T-34		T-35		T-36		T-37		T-38		T-39		T-40		T-41		T-42		T-43		T-44		T-45		T-46		T-47		T-48		T-49		T-50		T-51		T-52		T-53		T-54		T-55		T-56		T-57		T-58		T-59		T-60		T-61		T-62		T-63		T-64		T-65		T-66		T-67		T-68		T-69		T-70		T-71		T-72		T-73		T-74		T-75		T-76		T-77		T-78		T-79		T-80		T-81		T-82		T-83		T-84		T-85		T-86		T-87		T-88		T-89		T-90		T-91		T-92		T-93		T-94		T-95		T-96		T-97		T-98		T-99		T-100																																																																																																																																																																													
Test Run	Temperature	Pressure	Flow	Time	Location	Altitude	Latitude	Longitude	Speed	Direction	Wind	Wave	Current	Depth	Bottom	Soil	Vegetation	Animals	Plants	Minerals	Fossils	Geology	Hydrology	Climate	Ecology	History	Culture	Language	Religion	Government	Economy	Education	Health	Environment	Energy	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication	Science	Technology	Art	Literature	Music	Dance	Sports	Games	Religion	Philosophy	Law	Medicine	Agriculture	Industry	Commerce	Finance	Real Estate	Insurance	Banking	Transportation	Communication</

[illegible]



[illegible]

DATA SHEET 4  
PAGE 5 OF 7

[illegible]





July 1990  
Revision: Final

**TEST RUN 8**  
**400°F/36 HOURS**

1311R2

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DATA SHEET 1  
PAGE 1 OF 1

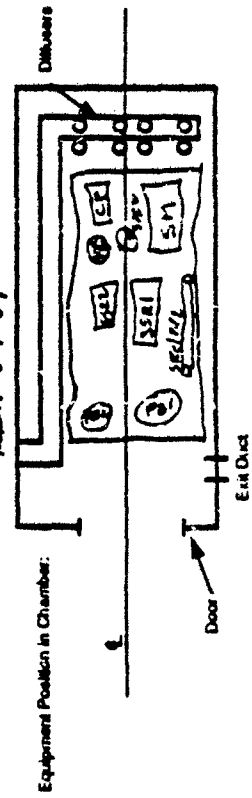
Test Run T-8 Date 8/3/89  
 Test Duration 36 Hrs Time \_\_\_\_\_  
 Heat Up Rate \_\_\_\_\_

Flash Chamber Temperature 400°F Flash Chamber Inlet \_\_\_\_\_

Equipment Type	Contaminant(s)	Dimensions L x W	Initial Wt (g)	Final Wt (g)	Sample Type	Equipment Supplier	Initial Contaminant Concentration	Final Contaminant Concentration	Thermocouple #	Observations Pre-Test	Observations Post-Test
1. SHR 1		9 1/4 x 7	11	11.5					10 (150)		
2. SHR 2		9 1/4 x 7	11.5	11.5							
3. PB 1		11 1/2 x 11 1/2	8	8.5					10		
4. PB 2		11 1/2 x 11 1/2	8.5	10.5					11		
5. SR 1		15 1/2 x 15 1/2	71	70.5							
6. SSF 2		15 1/2 x 15 1/2	85.0	85.0					6		
7. SHR 105		24 1/2 x 22	20.5	20.5					150 (140)		
8. SHR 106		23 1/2 x 21 1/2	719	719					20 (101)		
9. SHR 107		24 1/2 x 22	191	191							
10. SHR 108		24 1/2 x 22	191	191							
11. _____											
12. _____											
13. _____											
14. _____											
15. _____											

4 taken 8-9-89

NOTES: ① All equipment weighed on SCALE PROVIDED BY DEB  
 ② All SSR sized w/ 4" x 4" template



5  
204015  
204015  
204015

①

180

TEST

DATA SHEET 2  
PAGE 1 OF 6

Date 3 Aug 89 Test Number 18 400 F / 36 hrs

Time	Main Panel										Propellant Tank				Air				Flash Chamber Discharge				Afterburner Discharge				
	At 1000 F	At 1200 F	At 1400 F	At 1600 F	At 1800 F	At 2000 F	At 2200 F	At 2400 F	At 2600 F	At 2800 F	At 3000 F	At 3200 F	At 3400 F	At 3600 F	At 3800 F	At 4000 F	At 4200 F	At 4400 F	At 4600 F	At 4800 F	At 5000 F	At 5200 F	At 5400 F	At 5600 F	At 5800 F	At 6000 F	
0000																											
0100																											
0200																											
0300																											
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5600																											
5700																											
5800																											
5900																											
6000																											

2315 HRS - PRE HEAT  
STARTED (To Temp)  
AT 1800 F

DATA SHEET 2  
PAGE 2 OF 6

finded

4 AUG. 89 Test Number T-8 400°F/36hr

Time	Main Period										Propose Tank				Propose Tank				Afterburner Discharge			
	At Heater Inlet Temp	At Heater Outlet Temp	At Heater Inlet Press	At Heater Outlet Press	At Heater Inlet Flow	At Heater Outlet Flow	At Heater Inlet Temp	At Heater Outlet Temp	At Heater Inlet Press	At Heater Outlet Press	At Heater Inlet Flow	At Heater Outlet Flow	At Heater Inlet Temp	At Heater Outlet Temp	At Heater Inlet Press	At Heater Outlet Press	At Heater Inlet Flow	At Heater Outlet Flow	At Heater Inlet Temp	At Heater Outlet Temp	At Heater Inlet Press	At Heater Outlet Press
0000	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0100	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0200	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0300	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0400	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0500	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0600	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0700	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0800	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0900	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1000	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1100	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1200	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1300	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1400	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1500	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1600	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1700	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1800	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
1900	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
2000	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
2100	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
2200	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
2300	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120

S-50 AM  
STEADY STATE  
ACHIEVED.  
→ May 20/19/81  
Temperature 310  
1st. 2nd. 3rd. 4th.  
LP 1st. 2nd. 3rd. 4th.  
0.14 0.14 0.14  
0.14 0.14 0.14  
0.14 0.14 0.14

1000 - (bal) from tank  
Guns here to check tank  
78% full. Wants us to  
let him or his office know  
when we are running & shut  
in to don't have to come &

2059 hrs - in to check on system.  
running okay. High building  
press. clean going off but  
nothing shut down. Looks okay  
exit gas temp high - lowered



DATA SHEET 2  
PAGE 3 OF 6

(3)

2-230 City around with 2000-4000 ft. (1000-1500 ft.)  
Alt. in 2000 ft. 4000 ft. 2000 ft. 4000 ft. 2000 ft. 4000 ft.  
T.O. 1800° S.P. (750° S.P.)

Sub.

Date 5 Aug 89 Test Number T8 400°/564ms

Time	Main Panel										Propane Test			
	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	Alt. Heater	Alt. Heater	Alt. Heater	Alt. Heater
0000	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0100	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0200	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0300	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0400	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0500	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0600	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0700	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0800	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
0900	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1000	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1100	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1200	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1300	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1400	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1500	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1600	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1700	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1800	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
1900	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
2000	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
2100	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
2200	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300
2300	1000	1100	1200	1300	1400	1500	1600	1700	1800	1900	1000	1100	1200	1300

0830 AM  
City and 1000  
Altitude - 1000 ft.  
~ 400° @ 1000 ft.  
in Air Motion  
around 30 ft. 1000 ft.

Leaving 5100  
1200 ft. 1000 ft.  
Alt. 600 ft. 1000 ft.  
On-site 1755  
Alt. 600 ft. 1000 ft.  
On-site 1755  
Alt. 600 ft. 1000 ft.  
On-site 1755  
Alt. 600 ft. 1000 ft.

2030 Can from 5000 ft. 1000 ft.  
2050 Can from 5000 ft. 1000 ft.  
2100 Can from 5000 ft. 1000 ft.  
2150 Can from 5000 ft. 1000 ft.  
2200 Can from 5000 ft. 1000 ft.  
2250 Can from 5000 ft. 1000 ft.  
2300 Can from 5000 ft. 1000 ft.  
2350 Can from 5000 ft. 1000 ft.

4

DATA SHEET 2  
PAGE 4 OF 6

Sundul  
Date 6 Aug 1989 Test Number TB 400/36 hrs

Time	Main Period										After				Propane Tank				Propane Tank				Flash Chamber Discharge				Afterburner Discharge			
	Ar Water Temp °C	Ar Water Press PSIG	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C	Ar Water Temp °C
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1900																														
2000																														
2100																														
2200																														
2300																														
2400																														

09/15 high pH h  
ringing in gas  
line? Is this  
normal?  
- no TIC reading  
Paul Calibrating.

Monday  
AUG 39  
Tide Number 78  
400°/36 hrs

[illegible]

0500 - T.O. Temp. 24.6  
1815 - 1st. temp. 24.1  
2004 - Temp on 1812  
1st. moving up river

0139 - ~~Engine~~ ~~beater~~ went off - system down  
0203 - RT5 on-site. Flame failed. High building process. low temp.  
0206 - got T.O. burner going. T.O. Temp

0515 - ~~at~~<sup>while</sup> we were getting into the truck  
to leave I noticed the building lights go out. I thought it  
strange that the electric eyes would shut off so early (why)

6

DATA SHEET 2  
PAGE 6 OF 6

Tuesday  
Date 8 Aug 1989 Test Number T8 400/36 hrs.

Time	Main Period				Air Preheater	After Burner	Propane Tank			Propane Tank			
	HC-201 Air Heater Fuel Air Flow P-202	HC-201 Air Heater Temperature T-201	HC-201 T.O. Heat Air Temperature T-204	HC-201 Heat Flow P-201	HC-201 Heat Flow P-202	HC-201 Heat Flow P-203	HC-201 Heat Flow P-204	HC-201 Heat Flow P-205	HC-201 Heat Flow P-206	HC-201 Heat Flow P-207	HC-201 Heat Flow P-208	HC-201 Heat Flow P-209	HC-201 Heat Flow P-210
0000													
0100													
0200													
0300													
0400													
0500													
0600													
0700													
0800													
0900													
1000													
1100													
1200													
1300													
1400													
1500													
1600													
1700													
1800													
1900													
2000													
2100													
2200													
2300													

0600 SYSTEM TRIPPED DUE TO POWER SURGE  
0625 CITY AND P.S. ONSTAY ALL EQUIP.  $\angle 120^\circ$   
SO START SYSTEM (E.G. AND AMU) DOWN.

0715 - WATER FAILED IN REVERSE  
0930-1000 CITY AND P.S. OFFLINE FLASH CHAMBER  
REMOVED THEREAFTER

TX 8/3/89 Afterburner Ignition 12:05 PM

Key:																															
Powder Boxes - PB																															
Shell Support Rack - SSR																															
Clay Pipe - CP																															
Ship Mine - SM																															
Steam Heated Riser - SHR																															
Steel Pipe - SP																															
Aluminum Pipe - AP																															
Motor with Gear Reducer - M																															
Steam Heated Discharge Valve - SDV																															
Equip.	PB	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030																															
0130																															
0230																															
0330																															
0430																															
0530																															
0630																															
0730																															
0830																															
0930																															
1030																															
1130																															
1230		109	13	12	11	10	9	8	7	6	5	4	3	2	1																
1330																															
1430		110	115	123	128	107	108	126	101	110	106	108	112	108	107	102	83	111	103	107	105										
1530		111	115	124	128	108	107	126	102	111	107	108	112	110	108	105	87	112	106	105	103										
1630		112	114	124	128	109	108	126	102	111	108	109	112	112	110	108	89	112	109	107	106										
1730																															
1830																															
1930		113	115	124	129	110	108	126	103	112	109	110	112	113	111	110	92	113	110	108	109										
2030																															
2130																															
2230																															
2330		206	125	134	129	108	212	257	218	217	217	255	158	134	205	190	101	255	146	220	162										

Equip.		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
PB																															
0030	1	306	57	162	112	322	267	246	308	267	244	497	159	206	300	118	132	341	216	257	255										
0130	13	329	181	187	159	371	291	321	324	289	306	306	178	257	319	237	162	336	218	220	251										
0230	14	343	191	207	174	355	310	308	308	308	308	321	171	280	332	204	160	353	277	268	270										
0330	1	360	247	228	187	307	313	308	307	332	267	350	204	309	361	292	203	361	302	310	311										
0430	10	406	236	247	202	411	368	354	378	353	340	370	222	332	382	316	204	406	394	361	338										
0530	17	424	252	263	214	424	360	360	360	360	360	360	360	360	360	360	360	360	360	360	361										
0630	17	436	267	277	226	448	378	408	417	385	410	499	200	369	404	355	260	420	361	312	378										
0730	11	459	277	287	235	496	403	415	416	394	416	410	380	361	410	369	281	445	378	408	387										
0830		477	281	294	242	456	414	424	424	424	424	424	424	424	424	424	424	424	424	424	424										
0930	1	492	285	306	256	452	445	421	425	407	437	418	371	399	423	391	534	451	376	427	435										
1030	21																														
1130	2	447	302	311	262	458	422	427	428	409	438	421	281	400	424	394	494	453	398	426	428										
1230	23	450	304	314	266	455	419	424	424	410	438	416	384	402	420	376	483	452	399	421	423										
1330	24	444	307	317	270	452	418	422	422	412	436	418	287	403	424	397	471	453	400	425	421										
1430	25	456	311	321	274	460	419	424	424	415	437	420	270	405	426	391	459	453	402	427	423										
1530	1	460	315	325	278	460	419	424	424	415	437	420	270	405	426	391	459	453	402	427	423										
1630	1	460	315	325	278	460	419	424	424	415	437	420	270	405	426	391	459	453	402	427	423										
1730	1																														
1830	1	470	315	325	278	460	419	424	424	415	437	420	270	405	426	391	459	453	402	427	423										
1930	1	470	315	325	278	460	419	424	424	415	437	420	270	405	426	391	459	453	402	427	423										
2030	2045	465	332	343	278	472	435	438	448	432	453	434	311	477	435	417	444	469	420	447	437										
2130	205	490	345	355	285	470	430	430	430	430	430	430	430	430	430	430	430	430	430	430	430										
2230	203	490	345	355	285	470	430	430	430	430	430	430	430	430	430	430	430	430	430	430	430										
2330	211	490	345	355	285	470	430	430	430	430	430	430	430	430	430	430	430	430	430	430	430										



Equip.	PB	Key:																															
		1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30		
0030	51																																
0130	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50	50		
0230	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45	45		
0330																																	
0430	40	45	45	45	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40	40		
0530	35	35	40	40	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35	35		
0630	30																																
0730	25	25	25	42	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25		
0830	20	25	25	42	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25		
0930	0940	183	197	153	144	200	130	168	44	133	125	157	112	134	156	152	157	135	158														
1030	1	164	169	179	174	151	143	196	134	165	143	138	157	141	152	154	151	149	134	157													
1130																																	
1230	11	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25		
1330	12	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	
1430	13																																
1530	14	20	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	
1630	15	20	20	20	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	
1730	16																																
1830	17	20	20	20	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	
1930		25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	
2030	11																																
2130		25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	
2230	1	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	25	
2330																																	



400°/36 hrs

Test: T8

Date: Mon. 7 Aug 89

Key:																															
Powder Boxes - PB																															
Shell Support Rack - SSR																															
Clay Pipe - CP																															
Ship Mine - SM																															
Steam Heated Ricer - SHR																															
Steel Pipe - SP																															
Aluminum Pipe - AP																															
Motor with Gear Reducer - M																															
Steam Heated Discharge Valve - SDV																															
Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
0030	PB																														
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0330																															
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0506																															
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1930																															
2030																															
2130																															
2230																															
2330																															

Key:

Powder  
Boxes - PB

Shell Support  
Rack - SSR

Clay Pipe  
- CP

Ship Mole  
- SM

Steam  
Heated  
Riser - SHR

Steel Pipe  
- SP

Aluminum  
Pipe  
- AP

Motor with  
Gear  
Reducer  
- M

Steam  
Heated  
Discharge  
Valve - SDV

0 AUG 1967

700 136 143.

11/22/67

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Equip.	PB																													
0030																														
0130	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70
0230	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70
0330																														
0430	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70	70
0530																														
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1930																														
2030																														
2130																														
2230																														
2330																														

Key:

- Powder Boxes - PB
- Shell Support Rack - SSR
- Clay Pipe - CP
- Ship Mine - SM
- Steam Heated Riser - SHR
- Steel Pipe - SP
- Aluminum Pipe - AP
- Motor with Gear Reducer - M
- Steam Heated Discharge Valve - SDV

0715 MOLYBDENE FUEL IN POWER OUTAGE



[illegible]



[illegible]

[illegible]





[illegible]

July 1990  
Revision: Final

TEST RUN 13  
500°F/12 HOURS

1311R2

DATA SHEET 1  
PAGE 1 OF 1

1906 - 1350 Mashed & And  
Sifted up to do At-test  
Sampling.

Test 13  
500°/12 hrs

Test Run 500°/12 hrs  
Test Duration  
Heat-Up Rate

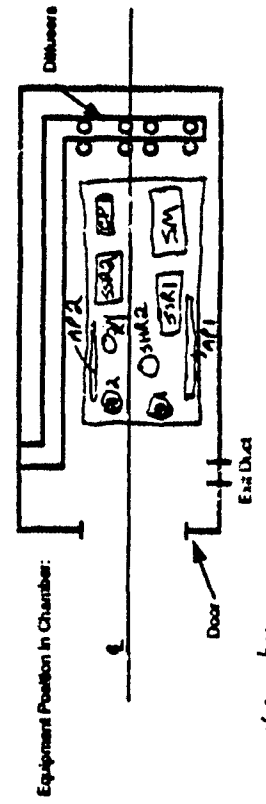
Date 8-7-89  
Time

Flash Chamber Temp 200 Flash Chamber Interior

Equipment Type	Contaminant(s)	Dimensions L H W	Initial Wt (lbs.)	Final Wt (lbs.)	Sample Type	Equipment Spiked	Initial Contaminant Concentration	Final Contaminant Concentration	Thermocouple #	Our Volume Pre-Test	Our Volume Post-Test
1. PBI	TNT	13 1/2" x 11 1/2"	8.5	8.5							
2. PBR	TNT	4 1/2" x 4 1/2"	7.5	8.5							
3. SHR 1	TNT	12" x 9"	11.5	12.0							
4. SHR 2	TNT	12" x 9"	11.5	12.0							
5. SSR 1	TNT	12" x 9"	11.5	12.0							
6. SSR 2	TNT	12" x 9"	11.5	12.0							
7. API	TNT	5 1/2" x 5 1/2"	5.5	5.5							
8. APR	TNT	5 1/2" x 5 1/2"	5.5	5.5							
9. CP	TNT	11 1/2" x 11 1/2"	7.2	6.5							
10. SM	TNT	11 1/2" x 11 1/2"	7.2	7.1							
11.											
12.											
13.											
14.											
15.											

← some c. irradiation  
→ small drop of ethylalcohol caught on ric. used extinguisher to put it out. some cleared spots look okay.

→ Pre-test sampling.  
Our readings w in control room, 20.70 in next to the sampling area.



10:15 AM 8-14-89 - open door on Chamber

At-test - 8-14-89 1:56 PM Chamber Temp 102°F D.C.

Post Test Sampling  
8-14-89 16:30 hrs -  
At-test

①

Test 113

Date 8/9/89 Test Number T13 500°F/12 hrs

Time	Main Panel				Air Treated	Air Inlet	Propane Tank				Air Heater Discharge		Flash Chamber Discharge		Aluminate Discharge			
	At Heater Tank Discharge HC-21	At Heater Tank Air Flow P-202	At Heater Temperature TC-204	At Heater Air Temperature TC-204			At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204	At Heater Temperature TC-204
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0100																		
0200																		
0300																		
0400																		
0500																		
0600																		
0700																		
0800																		
0900																		
1000																		
1100																		
1200																		
1300	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6	11.6
1400	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
1500	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
1600	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
1700	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
1800	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
1900	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
2000	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
2100	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
2200	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5
2300	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5	11.5

→ bugs!

NOTE: Pattern of the  
Molytek this test.  
Some of the  
thermocouples were  
bad & replaced  
with new ones (Chemi-  
#s 6, 16 & 18) (USE  
Channel 6 to monitor  
chamber temp since  
channel 8 - Exilgas  
doesn't seem to be  
reading correctly.

1233 - limits proved (T.O.) - fan running  
1235 - T.O. burner ignited - system running  
1300 - T.O. analysis set on yet due to low amt. of H<sub>2</sub>  
2014 - all power down for 1.5 sec.  
2020 - T.O. burner re-ignited & 40 sec

شکریہ

Date 10 May 54 Tax Number 773 520°/12 hrs

[illegible]

everybody says so: 10

06.10 DEWENT FLORENCE  
AUSTIN JAMES  
07.12 DEWENT FLORENCE  
AUSTIN JAMES  
DANGER

8:30 RAISED FUND  
FOR THE 6 OFFICES  
WARRANTED RAISED  
T. O. 2000

0900 PROPHET 34%  
Q. 1000 1000  
C. 1000 1000

1030 STANLEY STREET  
ACADIA V3D

1758 - count index - system down

1301 - T.O. up & running - Did not have had to bring  
306 - A.M. up & running - fuel valve below 30% to get limits proved

2133 - Cy & RJS on site on but everything even if counter hours as good. We will avg. the fast temp. - high building pres. alarm running. Mike Cosmes said temp below 500. the fast temp.

DATA SHEET 2  
PAGE 3 OF 5

Friday  
8/11/89

500°F / 12 hrs.

T13

Test Number

Time	Main Panel						Air Flashes	Alarm Buzzer	Propene Tank		Flash Chamber Discharge		Alcorturner Discharge	
	1000	1100	1200	1300	1400	1500			HC	CO	HC	CO	HC	CO
1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000
1100	1100	1100	1100	1100	1100	1100	1100	1100	1100	1100	1100	1100	1100	1100
1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200	1200
1300	1300	1300	1300	1300	1300	1300	1300	1300	1300	1300	1300	1300	1300	1300
1400	1400	1400	1400	1400	1400	1400	1400	1400	1400	1400	1400	1400	1400	1400
1500	1500	1500	1500	1500	1500	1500	1500	1500	1500	1500	1500	1500	1500	1500
1600	1600	1600	1600	1600	1600	1600	1600	1600	1600	1600	1600	1600	1600	1600
1700	1700	1700	1700	1700	1700	1700	1700	1700	1700	1700	1700	1700	1700	1700
1800	1800	1800	1800	1800	1800	1800	1800	1800	1800	1800	1800	1800	1800	1800
1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900	1900
2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000	2000
2100	2100	2100	2100	2100	2100	2100	2100	2100	2100	2100	2100	2100	2100	2100
2200	2200	2200	2200	2200	2200	2200	2200	2200	2200	2200	2200	2200	2200	2200
2300	2300	2300	2300	2300	2300	2300	2300	2300	2300	2300	2300	2300	2300	2300
2400	2400	2400	2400	2400	2400	2400	2400	2400	2400	2400	2400	2400	2400	2400

(Thurs. 8-10 2235 hrs  
(Started cool down)



5

83-74:5453 52-17772 1772=

5

DATA SHEET 2  
PAGE 5 OF 5

Sunday  
Date 8/13/89 Test Number T13 500/126

Time	Main Panel				Air				Alter.				Propose Tank				Propose Tank			
	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp	MC-201 Air Heater Exit Temp
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0200																				
0300																				
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0500																				
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0700																				
0800																				
0900																				
1000																				
1100																				
1200																				
1300																				
1400																				
1500																				
1600																				
1700																				
1800																				
1900																				
2000																				
2100																				
2200																				
2300																				

Monday 8/14 8:00 15 21 52 1045 1245  
8:14 8:40 S.A.T.S. SYSTEM DOWN



Equip.	TIME																													
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030																														
0130	232	234	534	416	247	527	417	214	159	83	106	120	109	411	744	186	151	165	203	150	174	114	135							
0230	304	924	114	153	210	510	318	210	210	153	152	155	157	170	57	27	27	219	308	219	215	158	214							
0330	367	231	165	164	575	573	374	316	310	450	223	228	261	253	106	315	384	304	425	22	215	219	204							
0430	328	165	25	115	377	54	44	371	365	366	468	522	305	22	134	315	265	363	457	317	357	314	335							
0530	411	182	220	210	410	675	424	377	381	511	275	311	328	28	65	41	414	141	23	312	367	319	357							
0630	457	210	453	416	412	510	469	410	410	410	310	310	310	310	191	453	467	467	502	307	307	404	404							
0730	450	210	207	277	462	711	410	410	410	410	410	410	410	410	211	453	465	465	465	465	465	465	465							
0830	493	265	207	277	462	711	410	410	410	410	410	410	410	410	211	453	465	465	465	465	465	465	465							
0930	(576)	314	319	271	272	412	412	412	412	412	412	412	412	412	211	453	465	465	465	465	465	465	465							
1030	516	216	316	316	316	316	316	316	316	316	316	316	316	316	211	453	465	465	465	465	465	465	465							
1130	552	410	313	324	511	715	510	510	510	510	510	510	510	510	211	453	465	465	465	465	465	465	465							
1230	551	381	378	377	511	715	510	510	510	510	510	510	510	510	211	453	465	465	465	465	465	465	465							
132645	415	323	315	515	515	515	515	515	515	515	515	515	515	515	211	453	465	465	465	465	465	465	465							
1430	422	307	364	350	513	714	511	410	317	455	475	475	475	475	211	453	465	465	465	465	465	465	465							
1530	418	285	371	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
1630	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
1730	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
1830	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
1930	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
2030	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
2130	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
2230	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							
2330	416	305	317	317	578	713	510	510	315	315	476	310	477	215	194	571	571	571	571	571	571	571	571							

1258 - powder outage.  
 1320 - A.H. back up & running  
 T.O. MUR T. meaning SIE at 1030 P.M. - SHUTDOWN  
 (2)

SW 1 / 12 hrs.

110

1001

1111

001101 1111

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Ke.	
Equip.	PB						V			H	H	H	V	V			V	V	V	V	V	V	V	V	V	V	V	V	V	V		
	Diffuser																															
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Equip.	Key:																													
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DATA SHEET 4  
PAGE 2- OF 8

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DATA SHEET 4  
PAGE 4 OF 8

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## DATA SHEET 4

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DATA SHEET 4  
PAGE 7 OF 8

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DATA SHEET 2  
PAGE 1 OF 4

ONE STARTED T.O.,  
FINDING PROBLEM

Tues. Date 8-15-89 Test Number T14 400°F / 12 hrs.

Time	Main Panel						Air Pressure PSIG	Air Temp F	Air Flow CFM	Air Pressure PSIG	Air Temp F	Propane Tank			Air Hose Discharge RHC	Flash Chamber Discharge RHC	Alcuburner Discharge																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																			
	MC-201	MC-202	MC-203	MC-204	MC-205	MC-206						MC-207	MC-208	MC-209			MC-210	MC-211	MC-212	MC-213	MC-214	MC-215	MC-216	MC-217	MC-218																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																																											
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23:40 PROBLEM ELEMENT, CONTINUED.

23:40 PROBLEM ELEMENT, CONTINUED. PROBLEM, RETURNED PRESSURE BY CLOSING GAS VALVE & PRESSURE RETURNED.

23:40 PROBLEM ELEMENT, CONTINUED. PROBLEM, RETURNED PRESSURE BY CLOSING GAS VALVE & PRESSURE RETURNED. AFTER RETURNED PROBLEM STILL OCCURRING - RETURNED PRESSURE & SYSTEM BEGAN OPERATING NORMALLY - SET PROBLEM GAS VALVE TO 70%.



1850

76 53 33 9 34 27 79 1 55 0 15 75 2

Pass 1405 hrs. - major wind storm came through - ~70 mph winds  
high building press. alarm



FROM  
Date 12 AUG 89 Test Number T14 400 F / 12 hrs.

Time	Main Panel						Propose Test		Afterburner Discharge			
	NO. 11 Air Motor Fuel Air Flow PSI	NO. 12 Air Motor Fuel Air Flow PSI	NO. 13 Air Motor Fuel Air Flow PSI	NO. 14 Air Motor Fuel Air Flow PSI	NO. 15 Air Motor Fuel Air Flow PSI	NO. 16 Air Motor Fuel Air Flow PSI	NO. 17 Air Motor Fuel Air Flow PSI	NO. 18 Air Motor Fuel Air Flow PSI	Flame Chamber Pressure	THC	CO	HC
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9900												
10000												

0445 - system shutdown for end of Test T14  
005 - noted that photo on SSR was left on during test. Photo melted. Mike Cosmos advised to take 4 test tubes as used. I will discuss course of action.

DATE : 8-15-89 TUES.

TEST : T14

400°F / 12 hrs.

DATA SHEET 3  
Page 1 of 4

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Exptl.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030																														
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Key:

Powder Boxes - PB  
Shell Support Rack - SSR  
Clay Pipe - CP  
Ship Mine - SM  
Steam Heated Riser - SHR  
Steel Pipe - SP  
Aluminum Pipe - AP  
Motor with Gear Reducer - M  
Steam Heated Discharge Valve - SDV

also got high building press. alarm at about the same time.

Equbo.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
0030	374	374	180	367	447	370	352	301	375	237	270	281	267	242	220	354	307	245	276	177											
0130	406	407	205	331	478	341	380	371	404	357	349	341	304	281	260	380	337	366	334	248											
0230	447	449	341	361	435	333	400	413	417	363	345	330	340	309	283	400	357	335	363	298											
0330	488	491	265	207	441	371	425	445	445	285	373	358	377	352	336	445	378	364	383	333											
0430	466	309	286	346	418	410	436	451	477	308	335	341	393	377	347	448	368	394	408	287											
0530	472	300	300	346	506	414	467	465	471	304	316	410	445	345	346	443	423	412	449	245											
0630 (on line out)	480	333	311	335	517	432	468	467	473	320	424	425	426	400	377	468	431	423	445	471											
0730	408	244	247	332	450	305	430	417	446	331	400	135	437	413	384	413	437	420	444	424											
0830	441	321	312	331	460	347	469	433	444	300	400	424	413	335	331	340	410	412	447	715											
0930	451	333	346	342	403	377	467	458	445	300	411	410	410	400	377	442	413	413	423	445											
1030	458	338	349	346	473	362	423	434	440	304	410	404	412	379	346	467	411	412	418	411											
1130	444	334	321	345	418	375	422	440	441	317	408	417	409	358	336	439	410	411	417	412											
1230	440	337	321	346	465	341	447	424	434	306	400	404	406	360	325	435	407	408	414	409											
1330	444	338	323	336	463	340	455	447	443	304	405	409	404	395	375	435	407	407	414	410											
1430	331	203	303	346	314	308	330	264	338	155	153	167	173	137	133	357	330	372	349	383											
1530	260			260			260	110	305	210	220	300	260	260	260	160	270			260											
1630																															
1730	250			250			240	140	260	110	240	250	250	250	240	250			240												
1830																															
1930	210			210	180						210	210	210	210	210	210															
2030	190			190	160						160	190	190	190	190	190															
2130																															
2230	175	190	165								185	210	170	115	180	165	150	170	180	180	180										
2330	160	180	155								200	155	160	140	170	155	165	165	170	160	160	160									

Key:  
 Powder Boxes - PB  
 Shell Support Rack - SSR  
 Clay Pipe - CP  
 Slip Mine - SM  
 Steam Heated Riser - S.H.R.  
 Steel Pipe - SP  
 Aluminum Pipe - AP  
 Motor with Gear Reducer - M  
 Steam Heated Discharge Valve - SDV

0200 - Reached "Steady State" - Exit Gas Temp 410°F  
 1400 - 1410 410 117 m - saw some problems

③

18 AUG 1989 T14 400°/12ms

TANSON

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Equip.	PB																													
0630 (08:30)	135	135	144	133	116	126	132	116	141	133	129	127	133	126	136	136	132	131	129	125										
0130			155	170					140	150	150	155	160	155	150	150	160	160	160	150										
0230			150	165	155			140	180	155		155		155		155	150		150											
0330																														
0430			140	150	140	140			170	135	140	150	140		140	140			140	145										
0530									105	130	120	120	135	135	130	130	130	130	130	120										
0630																														
0730			125	150				115	160	120	125		125		120	120	120	120		110										
0830			125	125	119	119	126	126	126	126	125	127	130	126	126	126	126	126	126	125										
0930			125	124	118	118	126	126	126	126	126	127	134	125	125	125	125	125	125	125										
1030			134	125	117	115	126	125	116	158	134	124	127	133	126	134	135	130	129	125										
1130			114	125	114	126	131	117	155	132	129	127	132	126	134	134	131	131	129	125										
1230			133	134	125	133	119	117	153	120	128	127	130	126	134	132	130	130	129	125										
1330			132	125	115	124	117	125	116	152	131	127	130	126	134	131	129	130	128	125										
1430			129	124	114	131	116	115	150	128	126	126	127	124	124	123	126	128	126	124										
1530																														
1630																														
1730																														
1830			120	120	120	120	140	120	120	120	120	120	110	110	120	120	120	120	120	120										
1930			115	115	115			115	115	115	115	115	115	115	115	115	115	115	115	115										
2030																														
2130			120	110	130	110		110	110	110	110	110	110	110	110	110	110	110	110	110										
2230																														
2330			108	108	125	108		108	108	115	108	108	109	108	108	108	108	108	108	108										

Equip.	Key:																													
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030	PB	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105
0130																														
0230		100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100	100
0330		95	95	115	95		95	95	115	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95
0430																														
0530																														
0630		95	95	115	95		95	95	115	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95	95
0730																														
0830		109	105	123	109	96	103	105	97	125	111	104	103	107	101	108	108	107	106	104	100									
093025		110	109	123	110	97	104	107	98	125	111	105	107	106	103	110	108	106	105	103										
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July 1990  
Revision: Final

TEST RUN 15  
600°F/12 HOURS

1311R2

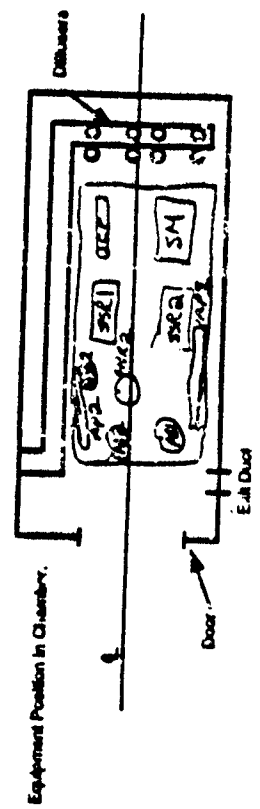
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Test Sub Data Tues.  
Date 8/22/89  
Time

Test Run T15  
Test Duration 19 hrs. - Study Shute  
Heat-Up Rate

Flash Chamber Temperature 600°F  
Flash Chamber Inlet

Equipment Type	Concentration(s)	Dimensions L x H x W	Initial Wt (lbs)	Final Wt (lbs)	Sample Type	Equipment Applied	Inlet Concentration	Final Concentration	Thermocouple #	Pre Test	Observations Post Test
1. PBI	Explosive	16" x 16" x 16"	10.5	10.5							Large crack in the side of the chamber
2. PBI		16" x 16" x 16"	10.5	10.5							Small crack in the side of the chamber
3. SHB1		78" x 78" x 78"	11.5	11.5							Small crack in the side of the chamber
4. SHB2		78" x 78" x 78"	11.5	11.5							Small crack in the side of the chamber
5. SSR1		24" x 24" x 24"	15.5	15.5							Small crack in the side of the chamber
6. SSR2		24" x 24" x 24"	15.5	15.5							Small crack in the side of the chamber
7. API		24" x 24" x 24"	15.5	15.5							Small crack in the side of the chamber
8. API		24" x 24" x 24"	15.5	15.5							Small crack in the side of the chamber
9. CP		24" x 24" x 24"	15.5	15.5							Small crack in the side of the chamber
10. SM		24" x 24" x 24"	15.5	15.5							Small crack in the side of the chamber



8/21/89 1210 - Pre Test Sampling  
1410 - Initial equipment  
8/22/89 0930 - Chamber loaded & thermal-  
cycling wired to equipment.  
CEM not calibrated yet - need  
at hr. more.  
9/27/89 Flash Chamber was sampled  
at the right hand wall,  
west of the...

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DATA SHEET 2  
PAGE 1 OF 3

Tuesday  
Date 8/22/89 Test Number T15 600° F / 12 hrs.

NOTE: S.C. Subid  
the Chamber door  
if fiberglass. Sur  
to be cut before  
can hold 814. pos  
more negative &  
still get the temp.  
we need.

Time	Main Panel										Air		Propane Tank		Flash Chamber Discharge		Aeroburner Discharge	
	177-200	177-200	177-200	177-200	177-200	177-200	177-200	177-200	177-200	177-200	Pressure	Temp	Pressure	Temp	Pressure	Temp	Pressure	Temp
0000	✓																	
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0200																		
0300																		
0400																		
0500																		
0600																		
0700																		
0800																		
0900																		
1000																		
1100																		
1200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1500	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1600	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1700	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1800	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
1900	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2000	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2100	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2200	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2300	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0
2400	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0	1.0

1100 - T.O. burner ignited  
12:00 - 3000 BTU - 1000 BTU  
15:00 - 3000 BTU - 1000 BTU

Wednesday

Test Number T15

$$600^\circ \text{F} / 12 \text{ hrs.}$$

1255 hrs - Flamm and the Pre-Header (high temp at 145°F)  
1257 hrs - Sustaining Burn, and

251110000 24115 14115 - 05111

W<sup>0</sup>F sale

DATA SHEET 2  
PAGE 3 OF 3

Date 8/14/89 Test Number T-15 600°F/12 hr.

Time	Main Panel										Projector Tank				Afterburner Discharge			
	At Exhaust Exit Discharge NO-87	At Exhaust Exit Air Flow P-302	At Exhaust Temperature TIC-304	T.O. Wet Air Temperature THER	Eng. Temp PC-271	Exhaust Air Valve Position NO-82	T.O. Temperature TIC-301	Exhaust (Constant and Variable Components) NO-81	At Exhaust P-301	At Exhaust P-302	At Exhaust P-303	CO <sub>2</sub>	CO	HC	Flash Chamber Discharge	NO	CO	HC
8000																		
8100																		
8200	17.1	1.0	1123	541	20.5	0	1172	57/42	152/47	160/50	162	19	50	35.6	41.7	2.5	7.2	0.5
8300																		
8400																		
8500																		
8600																		
8700																		
8800																		
8900	11.3	0.7	1010	185	20.5	0	1114	12/51	12/51	12/51	60	12	110	0	1.1	2.5	7.2	0.5
9000																		
9100																		
9200	12.3	0.7	1020	149	20.5	0	1114		10.0	10.0	62	13	114	0.6		0.5	7.1	0.2
9300																		
9400																		
9500																		
9600																		
9700																		
9800																		
9900																		
1000																		
1100																		
1200																		
1300																		
1400																		
1500																		
1600																		
1700																		
1800																		
1900																		
2000																		
2100																		
2200																		
2300																		
2400																		

17/400



Date: 8-22-84 TEST: 115 600 F / 12 hrs.

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
PB																														
Diffusion																														
0030																														
0130																														
0230																														
0330																														
0430																														
0530																														
0630																														
0730																														
0830																														
0930																														
1030																														
1120/10																														
1230																														
1330																														
1430																														
1530																														
1630																														
1730																														
1830																														
1930																														
2030																														
2130																														
2230																														
2330																														

Date: 8/23/89

Test: T15 600°F/12 hrs.

Key:	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	
Equip.	PB																														
	Diffuser																														
0030		505	120	264	208	330	348	350	323	361	321	359	217	235	277	222	247	274	162	208	291										
0130		425	345	219	270	461	385	392	418	426	297	336	287	312	357	277	419	450	246	298	343										
0230		416	266	263	319	447	421	429	397	461	350	376	341	305	373	337	462	499	323	465	411										
0330		501	300	249	256	532	63	415	371	441	555	415	382	403	417	367	418	519	477	437	413										
0430		535	368	329	373	566	488	486	424	527	430	452	422	446	447	406	420	557	444	487	477										
0530		570	407	241	410	402	371	514	412	517	473	441	431	400	415	443	547	543	419	504	511										
0630		509	415	597	449	421	536	533	440	551	504	505	488	506	489	466	570	611	507	557	535										
0730		600	455	445	448	428	465	546	508	585	523	521	506	524	486	481	590	617	505	550	544										
0830		614	476	427	471	415	574	560	523	510	545	540	525	518	505	501	603	636	599	567	546										
0930		624	448	441	524	444	581	562	571	602	553	549	536	581	572	512	608	612	563	577	575										
1030		632	504	453	517	451	510	571	553	607	566	558	573	566	525	523	625	650	572	587	584										
1130		645	544	446	624	640	600	584	603	648	560	569	557	574	534	634	658	509	602	572											
1230		640	570	440	521	671	609	572	575	588	584	574	565	581	537	559	633	640	592	602	592										
1330		650	523	480	541	656	609	573	564	574	576	574	566	582	570	539	613	627	600	606	597										
1430		657	534	491	551	669	617	602	576	632	596	584	574	573	549	570	641	675	607	615	608										
1530		660	555	503	584	684	645	603	640	640	640	640		555	546		640	620	620	620											
1630		670	510	505	565	670				640				560	540		620	610	600	640											
1730		670	510	505	565	670				640				560	540		620	610	600	640											
1830		680	510	505	565	670				640				560	540		620	610	600	640											
1930																															
2030		690	510	505	565	670				640				560	540		620	610	600	640											
2130		690	510	505	565	670				640				560	540		620	610	600	640											
2230																															
2330		725	436	540		625				640				603	630		620	610	600	640											

Key:

Powder  
Boxes - PB  
Shell Support  
Rack - SSR  
Clay Pipe  
- CP  
Ship Mine  
- SM  
Steam  
Heated  
Riser - SHR  
Steel Pipe  
- SP  
Aluminum  
Pipe  
- AP  
Motor with  
Gear  
Reducer  
- M  
Clean  
Heated  
Discharge  
Valve - SDV

DATE 8/24/89 1521 1-13 6:00 P/12 hr.

Page 3 of 2

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030																														
0130	335	335	335	335	335																									
0230	713	50	605	611	617	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618	618
0330																														
0430	201	44			430				340	340		504		716	503	60			550	510	500									
0530																														
0630																														
0730																														
0830	110	110			320		340		315	324		310		215	326	210			310	310	310									
0930	343	144	315	253	210	311	363	314	314	311	317	310	311	240	324	25	704	330	310	310	310									
1030																														
1130																														
1230																														
1330	150	110	110						145	108	310	310	310	310	310	310	310	310	310	310	310									
1430																														
1530																														
1630																														
1730																														
1830	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110									
1930																														
2030																														
2130																														
2230	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110									
2330																														

177 857c  
142.00 Eng Steam Spoke 2.9, T-15  
T-15 Pool Down Complete @ 0730 hrs 8/27/89

DATA SHEET 4  
PAGE 1 OF 7

[illegible]



DATA SHEET 4  
PAGE 3 OF 7

[illegible]



DATA SHEET 4  
PAGE 5 OF 7

[illegible]



[illegible]

[illegible]

July 1990  
Revision: Final

TEST RUN 16  
600°F/6 HOURS

1311R2

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DATA SHEET 1  
PAGE 1 OF 1

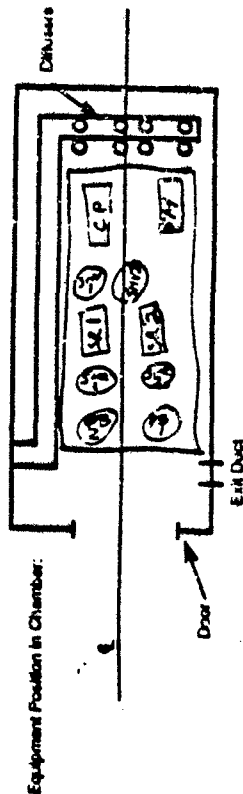
Test Run T-11a  
Test Duration 10:00/10:00  
Heat Up Rate \_\_\_\_\_  
Date 21 AUG 89  
Time \_\_\_\_\_

Flash Chamber Temperature \_\_\_\_\_ Flash Chamber Interior \_\_\_\_\_

Equipment Type	Container(s)	Dimensions (L x H x W)	Initial Wt (g)	Final Wt (g)	Sample Type	Equipment Spilled	Initial Concentration	Final Concentration	Thermocouple #	Observations Pre-Test	Post-Test
1. SSR 1	UPR 10010E	34x41x11	24.5	20.5	7L						
2. SSR 2		33x41x11	24.5	20.5	7L						
3. PD 1		15x15x11	7.5	7.5	8.5						
4. PD 2		15x15x11	7.5	7.5	8.5						
5. SHR 1		4x2x9	7.5	7.5	7.5						
6. SHR 2		4x2x9	7.5	7.5	7.5						
7. CP		4x2x11	147.0	12.5	12.5						
8. SHV 1		33x41x11	24.5	20.5	20.5						
9. SHV 2		33x41x11	24.5	20.5	20.5						
10. SHV 3		33x41x11	24.5	20.5	20.5						
11.											
12.											
13.											
14.											
15.											

Pre-Test Notes:

- \* PBI + PBI tested with ethylenediamine; No color changes observed
- \* Color change noted in bottom of SSR 2, and SSR 1. No color changes observed on the tops.
- \* Color change observed in liner of SHR 1
- \* CP - Price M. off of Flanged end.



- \* SHV 1 - heat exchanger
- \* SHV 2 - No heat exchanger

CP - Price M.



Date 8/28/89 (Mon) Test Number \_\_\_\_\_

Order 117

- PROPANE LEAK FOUND AT PREHEATER IGNITOR. (SEALED WITH DUCT TAPE).

12-Tile Creek, Owl River District,

0067  
7189

TEST: T16

600°F / 6 hrs.

DATA SHEET 3  
Page 1 of 2

②

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
	PB																													
0030	←	Di	60	30	↑	60	30	60	30	60	30	60	30	60	30	60	30	60	30	60	30	60	30	60	30	60	30	60	30	60
0130																														
0230																														
0330																														
0430																														
0530																														
0630																														
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1530																														
1630																														
1730																														
1830																														
1930																														
2030																														
2130																														
2230																														
2330	212	138	106	184	303	211	290	253	221	240	149	204	203	204	211	280	115	204	209	253										

8/28/89 Mon.

Test: 116 600 r 10 hr.

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
PB																														
0030	312	116	112	115	122	125	128	130	132	134	136	138	140	142	144	146	148	150	152	154	156	158	160	162	164	166	168	170	172	174
0130	334	210	214	218	222	226	230	234	238	242	246	250	254	258	262	266	270	274	278	282	286	290	294	298	302	306	310	314	318	322
0230	366	252	256	260	264	268	272	276	280	284	288	292	296	300	304	308	312	316	320	324	328	332	336	340	344	348	352	356	360	364
0330	418	316	320	324	328	332	336	340	344	348	352	356	360	364	368	372	376	380	384	388	392	396	400	404	408	412	416	420	424	428
0430	516	414	418	422	426	430	434	438	442	446	450	454	458	462	466	470	474	478	482	486	490	494	498	502	506	510	514	518	522	526
0530	568	466	470	474	478	482	486	490	494	498	502	506	510	514	518	522	526	530	534	538	542	546	550	554	558	562	566	570	574	578
0630	618	516	520	524	528	532	536	540	544	548	552	556	560	564	568	572	576	580	584	588	592	596	600	604	608	612	616	620	624	628
0730	668	566	570	574	578	582	586	590	594	598	602	606	610	614	618	622	626	630	634	638	642	646	650	654	658	662	666	670	674	678
0830	718	616	620	624	628	632	636	640	644	648	652	656	660	664	668	672	676	680	684	688	692	696	700	704	708	712	716	720	724	728
0930	768	666	670	674	678	682	686	690	694	698	702	706	710	714	718	722	726	730	734	738	742	746	750	754	758	762	766	770	774	778
1030	818	716	720	724	728	732	736	740	744	748	752	756	760	764	768	772	776	780	784	788	792	796	800	804	808	812	816	820	824	828
1130	868	766	770	774	778	782	786	790	794	798	802	806	810	814	818	822	826	830	834	838	842	846	850	854	858	862	866	870	874	878
1230	918	816	820	824	828	832	836	840	844	848	852	856	860	864	868	872	876	880	884	888	892	896	900	904	908	912	916	920	924	928
1330	968	866	870	874	878	882	886	890	894	898	902	906	910	914	918	922	926	930	934	938	942	946	950	954	958	962	966	970	974	978
1430	1018	916	920	924	928	932	936	940	944	948	952	956	960	964	968	972	976	980	984	988	992	996	1000	1004	1008	1012	1016	1020	1024	1028
1530	1068	966	970	974	978	982	986	990	994	998	1002	1006	1010	1014	1018	1022	1026	1030	1034	1038	1042	1046	1050	1054	1058	1062	1066	1070	1074	1078
1630	1118	1016	1020	1024	1028	1032	1036	1040	1044	1048	1052	1056	1060	1064	1068	1072	1076	1080	1084	1088	1092	1096	1100	1104	1108	1112	1116	1120	1124	1128
1730	1168	1066	1070	1074	1078	1082	1086	1090	1094	1098	1102	1106	1110	1114	1118	1122	1126	1130	1134	1138	1142	1146	1150	1154	1158	1162	1166	1170	1174	1178
1830	1218	1116	1120	1124	1128	1132	1136	1140	1144	1148	1152	1156	1160	1164	1168	1172	1176	1180	1184	1188	1192	1196	1200	1204	1208	1212	1216	1220	1224	1228
1930	1268	1166	1170	1174	1178	1182	1186	1190	1194	1198	1202	1206	1210	1214	1218	1222	1226	1230	1234	1238	1242	1246	1250	1254	1258	1262	1266	1270	1274	1278
2030	1318	1216	1220	1224	1228	1232	1236	1240	1244	1248	1252	1256	1260	1264	1268	1272	1276	1280	1284	1288	1292	1296	1300	1304	1308	1312	1316	1320	1324	1328
2130	1368	1266	1270	1274	1278	1282	1286	1290	1294	1298	1302	1306	1310	1314	1318	1322	1326	1330	1334	1338	1342	1346	1350	1354	1358	1362	1366	1370	1374	1378
2230	1418	1316	1320	1324	1328	1332	1336	1340	1344	1348	1352	1356	1360	1364	1368	1372	1376	1380	1384	1388	1392	1396	1400	1404	1408	1412	1416	1420	1424	1428
2330	1468	1366	1370	1374	1378	1382	1386	1390	1394	1398	1402	1406	1410	1414	1418	1422	1426	1430	1434	1438	1442	1446	1450	1454	1458	1462	1466	1470	1474	1478

POWER OUT TO MOTOR + CEM

\* Lost power to the flywheel due to a bad pump in line (532)



[illegible]





[illegible]



[illegible]

July 1990  
Revision: Final

TEST RUN 17  
600°F/48 HOURS

1311R2

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Date 8/29/82  
Time

Test Run T-17  
Test Duration 600°/48 hr AMH P.C.ATE

Heat Up Rate

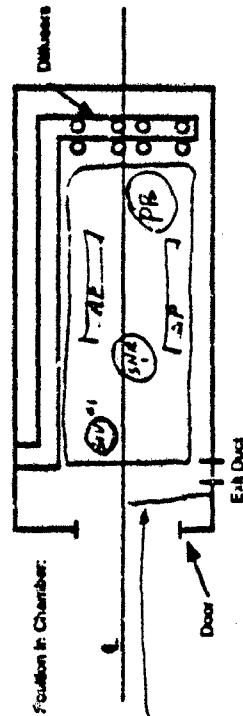
Flash Chamber Temperature

Flash Chamber Insides

Equipment Type	Container(s)	Dimensions L x W	Initial Wt (lbs.)	Final Wt (lbs.)	Sample Type	Equip. and Spilled	Liquid Contaminant Concentration	Final Contaminant Concentration	Thermocouple #	Pre-Test Observations	Post-Test Observations
1. PBI	AMH. PC.	11" x 11"	8.0	8.0						0.11 3.4.3	0.11 3.4.3
2. PBI		11" x 11"	8.0	X						0.11 3.4.3	0.11 3.4.3
3. PBI		11" x 11"	10.0	X						0.11 3.4.3	0.11 3.4.3
4. APC		11" x 11"	13.5	14.0						0.11 3.4.3	0.11 3.4.3
5. APC		11" x 11"	13.5	X						0.11 3.4.3	0.11 3.4.3
6. SP 1		11" x 11"	20.5	20.5						0.11 3.4.3	0.11 3.4.3
7. SP 2		11" x 11"	20.5	X						0.11 3.4.3	0.11 3.4.3
8. SHV 1		11" x 11"	25.5	25.5						0.11 3.4.3	0.11 3.4.3
9. SHV 2		11" x 11"	25.5	25.5						0.11 3.4.3	0.11 3.4.3
10. SHR 1		11" x 11"	7.5	7.5						0.11 3.4.3	0.11 3.4.3
11. SHR 2		11" x 11"	7.5	X						0.11 3.4.3	0.11 3.4.3

1/8 O.D. 0.530 O.D. 0.530

Test Notes: Equipment Location in Chamber:



NOTE: ALL EQUIPMENT WAS PRE RINSED WITH ACN & MDC WATER.

\* All pipe supplied by HWAAP

Post Notes: From. Low. CAR on floor, assembly at door. CEAS HERE IN PLON - 1 meter in from door. Wires of transfer walls are used. Also normal. But in appearance.





Key:

Powder Boxes - PB

Shell Support Hack - SSH

Clay Pipe - CP

Ship Mine - SM

Steam Heated Riser - SHR

Steel Pipe - SP

Aluminum Pipe - AP

Motor with Gear Reducer - M

Steam Heated Discharge Valve - SDV

	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
Equip.																														
D	P	F	U	S	O	R	S																							
0030	280	113	151	119	309	201	280	182	281	215	207	212	179	215																
0130	309	145	177	205	429	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230	230
0230	305	103	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128	128
0330	357	249	125	235	577	277	340	300	329	412	307	411	406	538	24															
0430	146	210	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120	120
0530	323	340	34	440	534	300	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401	401
0630	347	145	309	457	578	421	38	406	500	527	402	501	459	826	461															
0730	303	457	313	436	67	452	533	506	536	550	515	515	460	490																
0830	395	432	412	515	127	467	440	536	549	672	537	500	482	483	511															
0930	210	440	435	530	34	490	561	215	570	510	532	571	419	469	570															
1030	621	471	453	54	50	507	575	440	584	609	570	532	543	425	546															
1130	335	505	120	346	605	570	584	513	518	616	513	504	545	216	561															
1230	340	349	180	335	271	336	571	596	706	320	584	416	550	335	572															
1330	350	325	501	511	571	446	600	595	615	635	605	574	565	370	586															
1430	340	351	512	576	505	557	605	605	622	645	644	631	591	414	513															
1530	341	557	521	533	630	570	602	612	624	657	620	634	573	449	600															
1630	340	557	525	605	640	565	605	620	626	650	620	634	558	448	600															
1730	346	561	531	601	611	571	651	630	651	623	620	570	443	605																
1830	375	509	541	603	603	616	601	603	603	603	603	603	603	603	603															
1930	372	574	540	608	600	580	600	600	600	600	600	600	600	600	600															
2030	694	511	551	614	710	593	636	621	641	645	642	558	578	452	625															
2130	341	600	543	620	75	609	639	657	642	650	645	585	434	632																
2230																														
2330																														

9/3/89

48 hrs @ 600°F (cont.)

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
PB																														
DIFFUSERS																														
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Key:	Powder Boxes - PB	Shell Support Rack - SSR	Clay Pipe - CP	Strip Mine - SM	Steam Heated Riser - SHR	Steel Pipe - SP	Aluminum Pipe - AP	Motor with Gear Reducer - M	Steam Heated Discharge Valve - SDV
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Subtotal Flameouts Occurred on Preheaters between 1800 & 0830 hrs on 9/3/89

Eq. No.	Loc. No.																													
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030																														
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Key:

- Powder Boxes - PB
- Shell Support Rack - SSR
- Clay Pipe - CP
- Ship Mine - SM
- Steam Heated Riser - SHR
- Steel Pipe - SP
- Aluminum Pipe - AP
- Motor with Gear Reducer - M
- Steam Heated Discharge Valve - SDV

[illegible]

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Test Number		Run 7		Run 8		Run 9		Run 10		Run 11		Run 12		Run 13		Run 14		Run 15		Run 16		Run 17		Run 18		Run 19		Run 20		Run 21		Run 22		Run 23		Run 24		Run 25		Run 26		Run 27		Run 28		Run 29		Run 30		Run 31		Run 32		Run 33		Run 34		Run 35		Run 36		Run 37		Run 38		Run 39		Run 40		Run 41		Run 42		Run 43		Run 44		Run 45		Run 46		Run 47		Run 48		Run 49		Run 50		Run 51		Run 52		Run 53		Run 54		Run 55		Run 56		Run 57		Run 58		Run 59		Run 60		Run 61		Run 62		Run 63		Run 64		Run 65		Run 66		Run 67		Run 68		Run 69		Run 70		Run 71		Run 72		Run 73		Run 74		Run 75		Run 76		Run 77		Run 78		Run 79		Run 80		Run 81		Run 82		Run 83		Run 84		Run 85		Run 86		Run 87		Run 88		Run 89		Run 90		Run 91		Run 92		Run 93		Run 94		Run 95		Run 96		Run 97		Run 98		Run 99		Run 100		Run 101		Run 102		Run 103		Run 104		Run 105		Run 106		Run 107		Run 108		Run 109		Run 110		Run 111		Run 112		Run 113		Run 114		Run 115		Run 116		Run 117		Run 118		Run 119		Run 120		Run 121		Run 122		Run 123		Run 124		Run 125		Run 126		Run 127		Run 128		Run 129		Run 130		Run 131		Run 132		Run 133		Run 134		Run 135		Run 136		Run 137		Run 138		Run 139		Run 140		Run 141		Run 142		Run 143		Run 144		Run 145		Run 146		Run 147		Run 148		Run 149		Run 150		Run 151		Run 152		Run 153		Run 154		Run 155		Run 156		Run 157		Run 158		Run 159		Run 160		Run 161		Run 162		Run 163		Run 164		Run 165		Run 166		Run 167		Run 168		Run 169		Run 170		Run 171		Run 172		Run 173		Run 174		Run 175		Run 176		Run 177		Run 178		Run 179		Run 180		Run 181		Run 182		Run 183		Run 184		Run 185		Run 186		Run 187		Run 188		Run 189		Run 190		Run 191		Run 192		Run 193		Run 194		Run 195		Run 196		Run 197		Run 198		Run 199		Run 200		Run 201		Run 202		Run 203		Run 204		Run 205		Run 206		Run 207		Run 208		Run 209		Run 210		Run 211		Run 212		Run 213		Run 214		Run 215		Run 216		Run 217		Run 218		Run 219		Run 220		Run 221		Run 222		Run 223		Run 224		Run 225		Run 226		Run 227		Run 228		Run 229		Run 230		Run 231		Run 232		Run 233		Run 234		Run 235		Run 236		Run 237		Run 238		Run 239		Run 240		Run 241		Run 242		Run 243		Run 244		Run 245		Run 246		Run 247		Run 248		Run 249		Run 250		Run 251		Run 252		Run 253		Run 254		Run 255		Run 256		Run 257		Run 258		Run 259		Run 260		Run 261		Run 262		Run 263		Run 264		Run 265		Run 266		Run 267		Run 268		Run 269		Run 270		Run 271		Run 272		Run 273		Run 274		Run 275		Run 276		Run 277		Run 278		Run 279		Run 280		Run 281		Run 282		Run 283		Run 284		Run 285		Run 286		Run 287		Run 288		Run 289		Run 290		Run 291		Run 292		Run 293		Run 294		Run 295		Run 296		Run 297		Run 298		Run 299		Run 300		Run 301		Run 302		Run 303		Run 304</	
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July 1990  
Revision: Final

TEST RUN 18  
500°F/6 HOURS

1311R2

Test Run T-18  
Test Duration 6 hrs 2  
Heat-Up Rate \_\_\_\_\_  
Flash Chamber Temperature 500°F  
Flash Chamber Interior \_\_\_\_\_

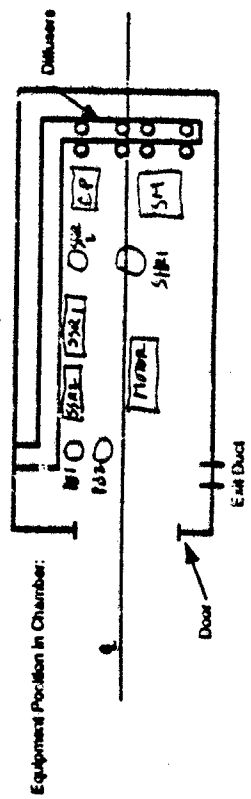
Date 9/13/89  
Time \_\_\_\_\_  
Sheet UP 0825

Equipment Type	Contaminant(s)	Dimensions L x H x W	Initial Wt (lbs.)	Final Wt (lbs.)	Sample Type	Equipment Speed	Initial Contaminant Concentration	Final Contaminant Concentration	Thermocouple #	Pie Test	Observations Post Test
1. SSR 1		35 1/2" x 18 1/2"	72.5	72.5							
2. SSR 2		35 1/2" x 18 1/2"	85.5	85.5							
3. PB 1		35 1/2" x 18 1/2"	8.5	8.5							
4. PB 2		35 1/2" x 18 1/2"	8.0	8.0							
5. SHR 1		7 1/4" x 9"	11.5	11.5							
6. SHR 2		7 1/4" x 9"	5.5	5.5							
7. CP		36"	126.5	126.5							
8. SM			769.5	769.5							
9. Motor			946.5	946.5							
10.											
11.											
12.											
13.											
14.											
15.											

Notes: Ethylene diamine applied to equipment, TAP  
A.T. on following: SSR 1  
SSR 1

SHIP MINE - End Able removed from P Test

MOTOR: LUBRIC OIL STAIN ON CYLINDER REDUCER.  
MOTOR STAND: removed from base of Motor &  
CYLINDER REDUCER, BUT, was still tested.



①

DATA SHEET 2  
PAGE 1 OF 5

232

Date 7/13/89 Test Number T-18 520°/6445.

Time	Main Panel							Air Temperature	Air Pressure	Aberr. Buttle	Propane Tank				Propane Tank				Aberturner Discharge																																																																																																																																																																																																																																																																																																																																																																															
	At Heater With Air Flow HC-201	At Heater With Air Flow P-202	Air Heater Temperature TC-204	T. Inlet Air Temperature TC-204	Bag Pressure PIC-221	Blow Air Valve Position HC-22	T.O. Temperature TC-204				Ambient Temperature Dry Bulb Temperature Wet Bulb Temperature and Humidity Control	Gas Pressure P-200	Flame Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200	Gas Pressure P-200

0815  
START T.O  
0825  
START  
12:30 AND 1:45  
1:50-2:00

\* sheet  
+ 4.4-10

9/15 0820 - AFTERBURNER DOWN.  
0800 - AFTERBURNER STARTED  
NOTE: Several attempts were made to ignite the preheated fuel without success.  
@ 0200 hrs. Nozzle loaded site. T.O. was left running + operation on 0210  
01:20 - PRE HEATER STARTED

2

DATA SHEET 2  
PAGE 2 OF 5

Date 9/14/89 Test Number T-18 500°F/6hr.

Time	Main Panel										Propane Tank			Propane Tank			Flash Chamber Discharge			Afterburner Discharge		
	At Heater Inlet Pressure (PSIA)	At Heater Inlet Temp (°F)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)	At Heater Outlet Temp (°F)	At Heater Outlet Pressure (PSIA)
00:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
01:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
02:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
03:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
04:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
05:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
06:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
07:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
08:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
09:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
10:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
11:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
12:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
13:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
14:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
15:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
16:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
17:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
18:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
19:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
20:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
21:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
22:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0
23:00	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0	55.0

- Pre heater started @ 1015 hrs this date.
- Received 8000 gallons of propane the date @ ~ 0700 hrs.
- 2000 lbs (9/18/89) steady state condition 80°F. Reached.

445 - A.A.  
Rising pressure  
/ time in sample



3

DATA SHEET 2  
PAGE 3 OF 5

Date 9/5/87 Test Number T-18 500F/6hr

Time	Main Panel						Propose Tank				Propose Tank				Atmospheric Discharge			
	Atmospheric Discharge MC-501	Atmospheric Discharge P-20	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10	Atmospheric Discharge T-10
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1900																		
2000																		
2100																		
2200																		
2300																		

T-18 Complete @ 0200 hrs. Cooledown begins

④

100-1000

9/2/59

Time	Main Panel				Air Pressure	Air Temperature	T.C. 201	T.C. 202	T.C. 203	T.C. 204	T.C. 205	T.C. 206	T.C. 207	T.C. 208	T.C. 209	T.C. 210	T.C. 211	T.C. 212	T.C. 213	T.C. 214	T.C. 215	T.C. 216	T.C. 217	T.C. 218	T.C. 219	T.C. 220	T.C. 221	T.C. 222	T.C. 223	T.C. 224	T.C. 225	T.C. 226	T.C. 227	T.C. 228	T.C. 229	T.C. 230	T.C. 231	T.C. 232	T.C. 233	T.C. 234	T.C. 235	T.C. 236	T.C. 237	T.C. 238	T.C. 239	T.C. 240	T.C. 241	T.C. 242	T.C. 243	T.C. 244	T.C. 245	T.C. 246	T.C. 247	T.C. 248	T.C. 249	T.C. 250	T.C. 251	T.C. 252	T.C. 253	T.C. 254	T.C. 255	T.C. 256	T.C. 257	T.C. 258	T.C. 259	T.C. 260	T.C. 261	T.C. 262	T.C. 263	T.C. 264	T.C. 265	T.C. 266	T.C. 267	T.C. 268	T.C. 269	T.C. 270	T.C. 271	T.C. 272	T.C. 273	T.C. 274	T.C. 275	T.C. 276	T.C. 277	T.C. 278	T.C. 279	T.C. 280	T.C. 281	T.C. 282	T.C. 283	T.C. 284	T.C. 285	T.C. 286	T.C. 287	T.C. 288	T.C. 289	T.C. 290	T.C. 291	T.C. 292	T.C. 293	T.C. 294	T.C. 295	T.C. 296	T.C. 297	T.C. 298	T.C. 299	T.C. 300	T.C. 301	T.C. 302	T.C. 303	T.C. 304	T.C. 305	T.C. 306	T.C. 307	T.C. 308	T.C. 309	T.C. 310	T.C. 311	T.C. 312	T.C. 313	T.C. 314	T.C. 315	T.C. 316	T.C. 317	T.C. 318	T.C. 319	T.C. 320	T.C. 321	T.C. 322	T.C. 323	T.C. 324	T.C. 325	T.C. 326	T.C. 327	T.C. 328	T.C. 329	T.C. 330	T.C. 331	T.C. 332	T.C. 333	T.C. 334	T.C. 335	T.C. 336	T.C. 337	T.C. 338	T.C. 339	T.C. 340	T.C. 341	T.C. 342	T.C. 343	T.C. 344	T.C. 345	T.C. 346	T.C. 347	T.C. 348	T.C. 349	T.C. 350	T.C. 351	T.C. 352	T.C. 353	T.C. 354	T.C. 355	T.C. 356	T.C. 357	T.C. 358	T.C. 359	T.C. 360	T.C. 361	T.C. 362	T.C. 363	T.C. 364	T.C. 365	T.C. 366	T.C. 367	T.C. 368	T.C. 369	T.C. 370	T.C. 371	T.C. 372	T.C. 373	T.C. 374	T.C. 375	T.C. 376	T.C. 377	T.C. 378	T.C. 379	T.C. 380	T.C. 381	T.C. 382	T.C. 383	T.C. 384	T.C. 385	T.C. 386	T.C. 387	T.C. 388	T.C. 389	T.C. 390	T.C. 391	T.C. 392	T.C. 393	T.C. 394	T.C. 395	T.C. 396	T.C. 397	T.C. 398	T.C. 399	T.C. 400	T.C. 401	T.C. 402	T.C. 403	T.C. 404	T.C. 405	T.C. 406	T.C. 407	T.C. 408	T.C. 409	T.C. 410	T.C. 411	T.C. 412	T.C. 413	T.C. 414	T.C. 415	T.C. 416	T.C. 417	T.C. 418	T.C. 419	T.C. 420	T.C. 421	T.C. 422	T.C. 423	T.C. 424	T.C. 425	T.C. 426	T.C. 427	T.C. 428	T.C. 429	T.C. 430	T.C. 431	T.C. 432	T.C. 433	T.C. 434	T.C. 435	T.C. 436	T.C. 437	T.C. 438	T.C. 439	T.C. 440	T.C. 441	T.C. 442	T.C. 443	T.C. 444	T.C. 445	T.C. 446	T.C. 447	T.C. 448	T.C. 449	T.C. 450	T.C. 451	T.C. 452	T.C.
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Date: 9/17/89 Test Number: T18 5000/6443

Time	Main Panel										Propane Tank				Propane Tank			
	Air Heater Fuel Discharge MC-201	Air Heater Fuel Air Flow PC-202	Air Heater Temperature TC-204	T.O. Inlet Air Temperature TC-204	Bag Pressure PC-221	Bag Air Valve Position MC-22	T.O. Temperature TC-204	Propane Tank Pressure PS-203	Propane Tank Temperature TC-203	Propane Tank Pressure PS-210	Propane Tank Pressure PS-212	Propane Tank Pressure PS-214	Propane Tank Pressure PS-216	Propane Tank Pressure PS-218	Propane Tank Pressure PS-220	Propane Tank Pressure PS-222	Propane Tank Pressure PS-224	Propane Tank Pressure PS-226
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0530 can from security system trip due to electrical system  
0530 can from security system trip due to electrical system  
0530 can from security system trip due to electrical system

56

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	Ref.
	PB																														
0030																															
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Powder Boxes - PB  
 Shell Support Rack - SSR  
 Clay Pipe - CP  
 Ship Mine - SM  
 Steam Heated Riser - SHR  
 Steel Pipe - SP  
 Aluminum Pipe - AP  
 Motor with Gear Reducer - M  
 Steam Heated Discharge Valve - SDV

0015  
STRA  
T-O.

177 857c

No TEMPS recorded DIFFICULTY NOTING PREPARED

9/14/89 778 500°/60ms. AIR-HOTTER STARTED 1015

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
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Key:

Powder Boxes - PB  
Shell Support Rack - SSR  
Clay Pipe - CP  
Ship Mine - SM  
Steam Heated Riser - SHR  
Steel Pipe - SP  
Aluminum Pipe - AP  
Motor with Gear Reducer - M  
Steam Heated Discharge Valve - SDV

11/2/07

11/13/07

3

Equip.	Key:																													
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
PB																														
0030	555	140	140	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160	160
0130																														
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0530	265	260	150	25	120	35	210	200	155	135	110	190	85	20	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
0630																														
0730																														
0830	242	160	202	171	171	171	181	181	177	201	220	238	203	241	224	198	219	219	219	219	219	219	219	219	219	219	219	219	219	219
0930	205	162	162	170	167	163	160	170	170	177	177	202	204	241	207	192	210	208	210	210	210	210	210	210	210	210	210	210	210	210
1030	190	160	200	165	165	165	190	195	170	230	185	160	190	205	190	180	195	195	195	195	195	195	195	195	195	195	195	195	195	195
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1430	172	140	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125
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1830																														
1930	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155	155
2030																														
2130																														
2230																														
2330	125	125	115	125	125	125	125	125	125	125	125	150	150	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125	125

9/16/89 718 500°/6445

④

Equip.	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030	115	110	120	120	120	120	120	110	120	140	140	140	140	140	120	120	120	120	120	120	120									
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0530	115	115	115	115	115	115	115	115	115	115	115	115	135	115	115	115	115	115	115	115	115									
0630																														
0730																														
0830	115	115	115	115	115	115	115	115	115	115	115	115	131	115	115	115	115	115	115	115	115									
0930																														
1030																														
1130																														
1230																														
1330	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110									
1430																														
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1830	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110	110									
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2030																														
2130																														
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2330	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105	105									

11/10/89

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Key:																															
Powder Boxes - PB																															
Shell Support Rack - SSR																															
Clay Pipe - CP																															
Ship Mine - SM																															
Steam Heated Riser - SHR																															
Steel Pipe - SP																															
Aluminum Pipe - AP																															
Motor with Gear Reducer - M																															
Steam Heated Discharge Valve - SDV																															
Equip.	PB	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30
0030		100	100	100	100	100	100	100	100	100	100	100	120				100	100	100	100	100	100									
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0630	9/12/67	98	57	10	98	93	105	101	98	0	95	76	77	102	78	98	98	103	101	102											
0730																															
0830	9/18/67	74	56	104	72	92	86	95	63		80	65	67	96	88	97	72	97	100												
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77-6576

Key:

Powder

Boxes - PB

Shell Support

Rack - SSR

Clay Pipe

- CP

Ship Mine

- SM

Steam

Heated

Riser - SHR

Steel Pipe

- SP

Aluminum

Pipe

- AP

Motor with

Gear

Reducer

- M

Steam

Heated

Discharge

Valve - SDV



Test Machine	P-10	End P		Back-up Start	10	Temperature	100 Deg P	Back-up Start	10	Steady State Start	15	Steady State Stop	30	Steady State Stop	35	Steady State Stop	40	Steady State Stop	45	Steady State Stop	50	Steady State Stop	55	Steady State Stop	60	Steady State Stop	65	Steady State Stop	70	Steady State Stop	75	Steady State Stop	80	Steady State Stop	85	Steady State Stop	90	Steady State Stop	95	Steady State Stop	100	Steady State Stop	105	Steady State Stop	110	Steady State Stop	115	Steady State Stop	120	Steady State Stop	125	Steady State Stop	130	Steady State Stop	135	Steady State Stop	140	Steady State Stop	145	Steady State Stop	150	Steady State Stop	155	Steady State Stop	160	Steady State Stop	165	Steady State Stop	170	Steady State Stop	175	Steady State Stop	180	Steady State Stop	185	Steady State Stop	190	Steady State Stop	195	Steady State Stop	200	Steady State Stop	205	Steady State Stop	210	Steady State Stop	215	Steady State Stop	220	Steady State Stop	225	Steady State Stop	230	Steady State Stop	235	Steady State Stop	240	Steady State Stop	245	Steady State Stop	250	Steady State Stop	255	Steady State Stop	260	Steady State Stop	265	Steady State Stop	270	Steady State Stop	275	Steady State Stop	280	Steady State Stop	285	Steady State Stop	290	Steady State Stop	295	Steady State Stop	300	Steady State Stop	305	Steady State Stop	310	Steady State Stop	315	Steady State Stop	320	Steady State Stop	325	Steady State Stop	330	Steady State Stop	335	Steady State Stop	340	Steady State Stop	345	Steady State Stop	350	Steady State Stop	355	Steady State Stop	360	Steady State Stop	365	Steady State Stop	370	Steady State Stop	375	Steady State Stop	380	Steady State Stop	385	Steady State Stop	390	Steady State Stop	395	Steady State Stop	400	Steady State Stop	405	Steady State Stop	410	Steady State Stop	415	Steady State Stop	420	Steady State Stop	425	Steady State Stop	430	Steady State Stop	435	Steady State Stop	440	Steady State Stop	445	Steady State Stop	450	Steady State Stop	455	Steady State Stop	460	Steady State Stop	465	Steady State Stop	470	Steady State Stop	475	Steady State Stop	480	Steady State Stop	485	Steady State Stop	490	Steady State Stop	495	Steady State Stop	500	Steady State Stop	505	Steady State Stop	510	Steady State Stop	515	Steady State Stop	520	Steady State Stop	525	Steady State Stop	530	Steady State Stop	535	Steady State Stop	540	Steady State Stop	545	Steady State Stop	550	Steady State Stop	555	Steady State Stop	560	Steady State Stop	565	Steady State Stop	570	Steady State Stop	575	Steady State Stop	580	Steady State Stop	585	Steady State Stop	590	Steady State Stop	595	Steady State Stop	600	Steady State Stop	605	Steady State Stop	610	Steady State Stop	615	Steady State Stop	620	Steady State Stop	625	Steady State Stop	630	Steady State Stop	635	Steady State Stop	640	Steady State Stop	645	Steady State Stop	650	Steady State Stop	655	Steady State Stop	660	Steady State Stop	665	Steady State Stop	670	Steady State Stop	675	Steady State Stop	680	Steady State Stop	685	Steady State Stop	690	Steady State Stop	695	Steady State Stop	700	Steady State Stop	705	Steady State Stop	710	Steady State Stop	715	Steady State Stop	720	Steady State Stop	725	Steady State Stop	730	Steady State Stop	735	Steady State Stop	740	Steady State Stop	745	Steady State Stop	750	Steady State Stop	755	Steady State Stop	760	Steady State Stop	765	Steady State Stop	770	Steady State Stop	775	Steady State Stop	780	Steady State Stop	785	Steady State Stop
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Track Number	Y-15	Row 7		500 deg F	Heat-up Start	Row 7	17	Temperature	Time	Steady State Start	25	Range 15 425-431	Steady State Stop	31	Range 15 417-431	Test End	66	Range 15 417-466	Bilfinger Bear	Bear	Floor	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Support Floor	Wall	Side	Right	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub	Middle	Ship	Clap	Near	Ship	Stash	Bilfinger	Exit	Row	Powder	Bulge	Floor	Hub
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July 1990  
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**APPENDIX E**  
**HOURLY AVERAGES FOR CEM SYSTEM DATA**

Appendix E provides hourly averages of data collected by the continuous emissions monitoring (CEM) system. The following information is provided:

- Afterburner Outlet
  - Oxygen (O<sub>2</sub>) concentration
  - Carbon Monoxide (CO) concentration
  - Nitrous Oxides (NO<sub>x</sub>) concentration
  - Total Hydrocarbons (THC) concentration
  - Carbon Dioxide (CO<sub>2</sub>) concentration
- Flash Chamber Inlet
  - Total Hydrocarbons (THC)
- Flash Chamber Outlet
  - Total Hydrocarbons (THC)

Two hydrocarbon analyzers were used to monitor total hydrocarbons: one analyzer continuously monitored emissions from the afterburner outlet; the other analyzer intermittently monitored emissions from the flash chamber inlet and outlet on a time sharing basis.

Several data gaps exist for various time periods in the CEM data presented in this Appendix. These data gaps are a result of power failures (usually from lightning events in the Hawthorne area) to the data logger system used to continuously record instrument readings. The data for these time periods were, however, recorded on a strip chart recorder. A review of the strip chart printout indicated that the data for these time periods are consistent with those presented herein.



July 1990  
Revision: Final

TEST RUN 2  
400°F/24 HOURS

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/25/69

Test #: 2

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:11-00:59	11.2	5.4	50.8	<0.1	6.2	<0.1	<0.1	2.1
01:00-01:59	11.2	5.7	49.3	<0.1	6.2	<0.1	<0.1	2.1
02:00-02:59	11.2	5.6	49.1	<0.1	6.2	<0.1	<0.1	2.1
03:00-03:59	11.2	5.7	50.4	<0.1	6.2	<0.1	<0.1	2.1
04:00-04:59	11.2	5.4	51.2	<0.1	6.1	<0.1	<0.1	2.0
05:00-05:59	11.2	5.4	51.4	<0.1	6.2	<0.1	<0.1	2.0
06:00-06:59	11.2	5.3	51.2	<0.1	6.1	<0.1	<0.1	2.0
07:00-07:59	11.3	6.0	51.8	<0.1	6.1	<0.1	<0.1	2.0
08:00-08:40	11.3	6.8	52.7	<0.1	6.1	<0.1	<0.1	24.5

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/26/89

Test #: 2

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
15:37-15:59	12.3	6.5	72.6	1.0	5.4	1.0	2.1	2.1
16:00-16:59	12.0	6.4	74.0	0.6	5.6	1.3	2.3	2.3
17:00-17:59	12.2	6.4	69.6	0.2	5.5	1.0	2.3	2.3
18:00-18:59	12.2	6.2	66.0	0.1	5.4	0.6	2.3	2.3
19:00-19:59	12.3	5.9	63.7	<0.1	5.4	0.9	1.7	1.7
20:00-20:59	12.4	5.5	64.7	<0.1	5.4	0.6	1.6	1.6
21:00-21:59	12.5	5.6	63.8	<0.1	5.3	0.7	1.5	1.5
22:00-22:59	12.6	5.8	60.6	<0.1	5.2	0.5	1.7	1.7
23:00-23:59	12.7	6.0	59.6	<0.1	5.1	0.7	1.4	1.4

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/27/89

Test #: 2

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	12.7	6.0	58.8	<0.1	5.1	0.6	1.5	1.5
01:00-01:59	12.7	6.1	57.0	<0.1	5.1	0.6	1.4	1.4
02:00-02:59	12.9	6.3	55.6	<0.1	5.0	0.5	1.5	1.5
03:00-03:59	13.0	6.6	54.2	<0.1	4.9	0.3	1.7	1.7
04:00-04:59	13.1	6.8	55.7	<0.1	4.8	0.7	1.1	1.1
05:00-05:59	13.1	6.7	54.9	<0.1	4.8	0.5	1.4	1.4
06:00-06:59	13.2	6.8	54.3	<0.1	4.8	0.3	1.5	1.5
07:00-07:59	13.3	7.6	53.3	<0.1	4.7	0.6	1.4	1.4
08:00-08:59	13.4	8.9	52.5	0.2	4.6	0.8	2.1	2.1
09:00-09:28	13.4	9.1	52.6	0.2	4.6	0.5	2.6	2.6
10:37-10:59	13.3	9.1	52.4	0.6	4.5	1.0	2.6	2.6
11:00-11:59	13.4	8.8	53.1	0.4	4.5	0.8	2.9	2.9
12:00-12:59	13.4	8.7	53.8	0.3	4.5	0.6	2.3	2.3
13:00-13:59	13.4	8.7	53.7	0.2	4.4	0.8	2.6	2.6
14:00-14:59	13.4	8.7	54.1	0.2	4.4	1.0	2.4	2.4
15:00-15:59	13.4	8.6	54.0	0.2	4.5	0.5	2.6	2.6
16:00-16:59	13.3	8.4	53.7	0.1	4.5	1.1	2.1	2.1
17:00-17:59	12.9	7.8	55.5	0.1	4.8	0.8	2.2	2.2
18:00-18:59	12.9	7.6	55.1	<0.1	4.8	0.9	2.0	2.0
19:00-19:59	13.2	7.9	52.5	<0.1	4.6	0.6	2.0	2.0
20:00-20:59	13.0	7.4	51.7	<0.1	4.7	0.4	1.8	1.8
21:00-21:59	13.3	7.8	49.1	<0.1	4.5	0.7	1.5	1.5
22:00-22:59	13.3	7.8	51.9	<0.1	4.5	0.4	1.5	1.5
23:00-23:59	13.4	7.7	51.4	<0.1	4.4	0.6	1.4	1.4

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/28/89

Test #: 2

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	13.4	7.6	49.4	<0.1	4.4	0.5	1.6	1.6
01:00-01:59	13.4	7.7	48.8	<0.1	4.4	0.3	1.7	1.7
02:00-02:59	13.4	7.6	48.7	<0.1	4.4	0.6	1.4	1.4
03:00-03:59	13.4	7.4	49.3	<0.1	4.4	0.4	1.5	1.5
04:00-04:59	13.5	7.6	50.0	<0.1	4.4	0.6	1.4	1.4
05:00-05:59	13.5	7.7	50.2	<0.1	4.4	0.4	1.2	1.2
06:00-06:59	13.5	7.5	49.8	<0.1	4.4	0.2	1.2	1.2
07:00-07:44	13.5	7.7	50.3	<0.1	4.4	0.3	1.2	1.2
08:51-08:59	19.6	6.6	0.3	1.5	0.1	<0.1	1.9	1.9
09:00-09:59	19.6	6.9	0.3	1.6	<0.1	1.1	3.1	3.1
10:00-10:59	19.6	6.7	0.3	1.3	<0.1	0.7	3.0	3.0
11:00-11:59	19.6	6.7	0.2	1.3	<0.1	1.1	2.5	2.5
12:00-12:59	19.6	6.6	0.3	1.2	<0.1	1.1	2.4	2.4
13:00-13:59	19.6	6.7	0.3	1.2	<0.1	0.7	2.8	2.8
14:00-14:59	19.6	6.7	0.2	1.3	<0.1	1.1	2.4	2.4
15:00-15:59	19.6	6.5	0.2	1.3	<0.1	0.9	2.4	2.4
16:00-16:59	19.6	6.4	0.2	1.2	<0.1	1.0	2.2	2.2
17:00-17:59	19.7	6.4	0.2	1.5	<0.1	0.8	2.2	2.2
18:00-18:59	19.6	6.3	0.3	17.0	<0.1	0.6	2.5	2.5
19:00-19:59	19.1	17.1	3.2	1.7	0.5	0.9	2.1	2.1
20:00-20:59	18.2	22.1	8.3	1.1	1.2	0.5	2.0	2.0
21:00-21:59	18.0	22.8	9.2	1.0	1.3	0.8	1.6	1.6
22:00-22:59	18.0	22.9	9.0	1.1	1.3	0.7	1.7	1.7
23:00-23:59	18.0	22.7	8.9	1.0	1.3	0.8	1.6	1.6

July 1990  
Revision: Final

TEST RUN 3  
500°F/36 HOURS

1311R2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/19/89

Test #: 3

Test Time	Afterburner Outlet				Flash		Flash Chamber Outlet THC (ppm)
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	Chamber Inlet THC (ppm)	
00:00-00:59	12.0	5.8	64.9	<0.1	5.9	0.4	<0.1
01:00-01:59	12.4	6.1	59.6	<0.1	5.6	0.3	<0.1
02:00-02:59	12.5	6.3	58.8	<0.1	5.6	0.2	<0.1
03:00-03:59	12.6	6.1	58.4	<0.1	5.6	0.2	<0.1
04:00-04:59	12.5	5.8	58.4	<0.1	5.7	0.1	<0.1
05:00-05:59	12.4	5.5	57.9	<0.1	5.7	<0.1	<0.1
06:00-06:59	12.5	5.6	56.4	<0.1	5.7	<0.1	<0.1
07:00-07:59	17.8	17.4	12.0	0.8	1.3	0.1	<0.1
08:00-08:59	13.5	9.9	50.4	0.1	5.0	0.2	<0.1
09:00-09:59	13.0	7.8	60.6	0.2	5.3	0.8	8.4
10:00-10:59	12.8	7.7	63.6	0.1	5.5	0.3	3.5
11:00-11:59	12.4	7.6	67.8	<0.1	5.8	0.9	2.1
12:00-12:59	11.7	7.8	75.8	<0.1	6.5	0.4	3.2
13:00-13:59	9.0	17.6	98.5	4.1	4.8	13.5	11.9
14:00-14:59	11.2	8.4	78.1	0.5	6.2	0.9	3.8
15:00-15:59	11.3	8.1	78.6	0.2	6.4	0.6	3.6
16:00-16:59	11.4	7.6	77.7	<0.1	6.5	1.1	2.7
17:00-17:59	11.4	7.5	78.8	<0.1	6.5	0.8	2.3
18:00-18:59	11.3	7.4	79.9	<0.1	6.6	0.5	3.0
19:00-19:59	11.2	6.8	76.4	<0.1	6.6	1.2	2.1

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/23/89

Test #:

3

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
20:49-20:59	17.5	24.7	11.6	1.2	1.6	1.6	6.1	6.1
21:00-21:59	17.6	24.1	11.1	0.8	1.5	1.2	2.3	2.3
22:00-22:59	17.5	24.0	11.0	0.7	1.5	0.8	2.1	2.1
23:00-23:59	17.1	24.7	13.2	0.7	1.8	1.2	1.7	1.7



HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/24/89

Test #: 3

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	16.3	24.4	17.0	0.4	2.3	0.8	1.9	1.9
01:00-01:59	15.4	20.3	22.0	<0.1	3.0	0.9	1.5	1.5
02:00-02:59	14.5	13.5	28.5	<0.1	3.7	0.9	1.4	1.4
03:00-03:59	13.4	8.2	38.3	<0.1	4.5	0.7	1.6	1.6
04:00-04:59	12.2	6.3	51.4	<0.1	5.4	0.8	1.4	1.4
05:00-05:59	11.1	5.5	64.0	<0.1	6.1	0.7	1.5	1.5
06:00-06:59	10.0	5.4	78.6	<0.1	7.0	0.7	1.5	1.5
07:00-06:59	5.7	5.4	83.9	<0.1	7.2	<0.1	1.2	1.2

July 1990  
Revision: Final

TEST RUN 5  
500°F/24 HOURS

1311R2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/29/89

Test #:

5

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	17.6	23.4	11.0	1.1	1.5	0.5	1.7	1.7
01:00-01:59	16.9	24.3	14.1	1.3	1.9	0.4	1.6	1.6
02:00-02:59	16.2	24.4	16.9	1.1	2.5	0.7	1.4	1.4
03:00-03:59	15.3	23.2	19.2	0.8	2.7	0.7	1.5	1.5
04:00-04:59	14.9	16.5	27.2	0.3	3.4	0.6	1.5	1.5
05:00-05:59	14.1	11.7	35.3	0.1	4.0	0.4	1.7	1.7
06:00-06:59	13.2	8.1	46.6	<0.1	4.7	0.7	1.5	1.5
07:00-07:59	12.2	6.1	63.4	<0.1	5.4	0.6	1.7	1.7
08:00-08:29	11.4	6.1	76.3	0.1	5.9	0.5	2.2	2.2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/30/89

Test #: 5

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
18:18-18:59	12.4	8.8	75.3	0.4	5.3	1.0	2.1	2.1
19:00-19:59	12.3	5.7	74.3	0.1	5.4	0.6	2.3	2.3
20:00-20:59	12.2	5.5	72.2	<0.1	5.4	0.9	1.7	1.7
21:00-21:59	12.3	5.4	66.9	<0.1	5.3	0.9	1.5	1.5
22:00-22:59	12.4	5.4	62.8	<0.1	5.2	0.6	1.6	1.6
23:00-23:59	12.5	5.7	59.8	<0.1	5.2	0.4	1.7	1.7

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 07/31/89

Test #:

5

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:25	12.5	6.6	58.5	<0.1	5.2	1.3	1.3	1.3
16:32-16:59	16.3	22.6	18.0	1.2	2.5	2.6	3.7	3.7
17:00-17:59	15.7	19.7	22.1	0.7	3.0	0.5	2.1	2.1
18:00-18:59	14.9	14.0	29.7	0.2	3.5	0.9	1.7	1.7
19:00-19:59	14.0	8.5	41.8	<0.1	4.1	0.9	1.5	1.5
20:00-20:59	12.7	5.4	59.3	<0.1	5.1	0.6	1.5	1.5
21:00-21:59	13.5	5.8	58.8	<0.1	4.5	0.4	1.4	1.4
22:00-22:59	13.5	5.8	57.4	<0.1	4.5	0.6	1.2	1.2
23:00-23:59	13.4	5.7	57.4	<0.1	4.6	0.4	1.4	1.4

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/01/89  
Test #:

5

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	13.4	5.6	56.1	<0.1	4.6	0.5		1.2
01:00-01:59	13.5	5.6	55.5	<0.1	4.5	0.3		1.3
02:00-02:59	13.4	5.6	55.6	<0.1	4.6	0.6		1.1
03:00-03:59	13.5	5.7	55.0	<0.1	4.5	0.4		1.2
04:00-04:59	13.5	6.0	55.4	<0.1	4.5	0.5		1.2
05:00-05:59	13.5	6.1	55.3	<0.1	4.5	0.4		1.3
06:00-06:52	13.5	5.9	55.4	<0.1	4.5	0.3		1.1
09:03-09:59	19.3	9.4	2.1	6.7	0.3	0.9		1.9
10:00-10:59	18.3	20.1	8.1	1.0	1.0	0.7		2.0
11:00-11:59	18.1	21.0	9.2	0.9	1.1	0.9		2.0
12:00-12:59	18.1	21.2	9.1	1.0	1.1	0.6		2.3
13:00-13:59	18.1	21.0	9.0	1.2	1.1	1.1		2.0
14:00-14:59	17.9	21.7	10.3	1.2	1.3	1.0		1.5
15:00-15:35	13.3	24.5	60.6	2.6	2.4	1.5		11.9
08:39-08:59	13.6	7.7	33.4	0.1	4.5	0.4		3.1
09:00-09:59	13.6	7.4	0.2	0.1	4.5	0.8		1.7
10:00-10:59	13.0	9.7	22.5	0.2	4.6	0.5		1.9
11:00-11:59	12.1	10.3	80.9	0.6	4.0	1.8		3.4
12:00-12:59	13.7	8.6	53.5	0.4	4.4	1.0		2.2
13:00-13:22	13.7	8.2	53.8	0.3	4.4	0.5		3.2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/02/89

Test #:

5

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
08:44-08:59	19.6	5.7	0.2	1.3	0.2	0.6	1.7	
09:00-09:59	13.4	12.9	71.5	4.0	1.5	1.4	9.6	
10:00-10:59	19.6	5.4	0.3	<0.1	0.2	10.7	<0.1	
11:00-11:59	19.6	5.6	0.3	<0.1	0.2	<0.1	<0.1	
12:00-12:59	19.6	5.7	0.3	<0.1	0.3	<0.1	<0.1	
13:00-13:59	19.6	5.6	0.3	<0.1	0.2	<0.1	<0.1	
14:00-14:59	19.6	5.4	0.3	<0.1	0.2	<0.1	<0.1	
15:00-15:52	19.2	5.5	0.3	<0.1	0.2	<0.1	<0.1	
16:29-16:59	19.6	5.3	0.3	<0.1	0.2	<0.1	<0.1	
17:00-17:59	19.6	5.2	0.4	<0.1	0.2	<0.1	<0.1	
18:00-18:59	19.6	5.2	0.3	<0.1	0.2	<0.1	<0.1	
19:00-19:59	19.6	5.0	0.3	<0.1	0.2	<0.1	<0.1	
20:00-20:59	19.6	4.7	0.3	<0.1	0.2	<0.1	<0.1	
21:00-21:59	19.6	4.6	0.2	<0.1	0.2	<0.1	<0.1	
22:00-22:59	19.6	4.5	0.2	<0.1	0.2	<0.1	<0.1	
23:00-23:59	19.6	4.3	0.2	<0.1	0.2	<0.1	<0.1	

July 1990  
Revision: Final

TEST RUN 8  
400°F/36 HOURS

1311R2



HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/03/69

Test #:

8

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	19.6	4.4	0.2	<0.1	0.2	<0.1	<0.1	<0.1
01:00-01:59	19.6	4.4	0.2	<0.1	0.2	<0.1	<0.1	<0.1
02:00-02:59	19.6	4.3	0.2	<0.1	0.2	<0.1	<0.1	<0.1
03:00-03:59	19.6	4.5	0.2	<0.1	0.2	<0.1	<0.1	<0.1
04:00-04:59	19.6	4.3	0.2	<0.1	0.2	<0.1	<0.1	<0.1
05:00-05:59	19.6	4.3	0.1	<0.1	0.2	<0.1	<0.1	<0.1
06:00-06:59	19.6	4.3	<0.1	<0.1	0.2	<0.1	<0.1	<0.1
07:00-07:59	19.6	4.4	<0.1	<0.1	0.2	<0.1	<0.1	<0.1
08:11-08:59	10.5	19.1	102.2	8.5	3.0	<0.1	<0.1	5.0
09:00-09:59	19.1	7.5	0.3	1.2	0.5	17.8	17.8	12.0
10:00-10:59	19.6	5.2	0.3	1.1	0.2	0.9	0.9	2.1
11:00-11:59	19.6	5.4	0.2	9.2	0.2	0.7	0.7	3.4
12:00-12:59	18.3	21.3	7.1	3.2	1.1	1.0	1.0	2.7
13:00-13:59	18.0	23.4	2.1	1.4	1.3	0.8	0.8	2.3
14:00-14:59	18.0	23.2	9.1	1.3	1.3	0.9	0.9	2.1
15:00-15:59	18.0	22.8	9.0	1.2	1.3	0.6	0.6	2.2
16:00-16:59	17.8	23.2	10.1	1.3	1.4	0.9	0.9	1.4
17:00-17:59	17.2	24.9	12.8	1.8	1.8	0.7	0.7	1.9
18:00-18:59	16.4	26.2	15.3	1.8	2.3	0.5	0.5	1.8
19:00-19:59	15.6	23.8	19.4	0.9	2.9	0.7	0.7	1.5
20:00-20:59	14.9	16.7	26.9	0.3	3.5	0.7	0.7	1.4
21:00-21:59	13.8	9.4	39.1	<0.1	4.2	0.5	0.5	1.4
22:00-22:59	12.6	6.1	57.9	<0.1	5.0	0.7	0.7	1.3
23:00-23:59	11.0	4.6	54.4	<0.1	6.2	21.4	21.4	12.7

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/04/89

Test #:

8

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.0	4.5	57.0	<0.1	6.8	32.8	26.8	
01:00-01:59	9.9	4.7	57.0	<0.1	6.9	35.7	28.9	
02:00-02:59	10.0	4.8	56.9	<0.1	6.8	38.2	35.6	
03:00-03:59	10.0	5.0	58.0	<0.1	6.8	62.1	48.2	
04:00-04:59	10.9	5.1	54.0	<0.1	6.2	59.6	43.5	
05:00-05:59	11.3	5.1	53.3	<0.1	6.0	61.2	43.5	
06:00-06:59	10.5	4.8	59.0	<0.1	6.5	59.8	45.0	
07:00-07:59	10.5	5.1	59.8	<0.1	6.5	58.1	44.1	
08:00-08:59	10.6	5.8	72.8	<0.1	6.5	55.3	45.3	
09:00-09:59	9.8	11.5	86.6	3.4	5.6	49.9	39.5	
10:00-10:59	10.8	6.2	55.6	0.2	6.4	48.6	38.8	
11:00-11:59	10.8	6.0	55.8	0.1	6.4	47.9	36.6	
12:00-12:59	10.9	6.1	55.9	0.1	6.3	46.7	35.8	
13:00-13:59	10.9	6.1	55.7	0.1	6.3	45.5	35.3	
14:00-14:59	10.9	6.2	56.7	0.1	6.2	44.8	34.2	
15:00-15:59	10.9	6.1	57.0	0.1	6.3	43.6	34.0	
16:00-16:59	10.9	5.9	56.8	<0.1	6.2	43.9	33.5	
17:00-17:59	10.8	5.7	57.0	<0.1	6.3	44.0	34.3	
18:00-18:59	10.7	5.8	56.9	<0.1	6.3	45.7	34.7	
19:00-19:59	10.7	5.7	56.5	<0.1	6.4	47.2	35.5	
20:00-20:59	10.7	5.1	54.7	<0.1	6.4	50.5	38.5	
21:00-21:59	10.7	5.0	56.0	<0.1	6.4	51.0	39.0	
22:00-22:59	10.6	5.4	56.3	<0.1	6.5	50.0	38.8	
23:00-23:59	10.6	5.1	56.1	<0.1	6.4	50.0	38.8	

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 06/05/89

Test #:

8

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.6	5.0	55.7	<0.1	6.5	51.5	40.4	40.4
01:00-01:59	10.5	5.1	54.8	<0.1	6.5	54.6	43.3	43.3
02:00-02:59	10.5	5.3	54.3	<0.1	6.5	56.2	44.3	44.3
03:00-03:59	10.5	5.3	55.6	<0.1	6.5	56.5	44.7	44.7
04:00-04:59	10.5	5.3	56.5	<0.1	6.6	55.4	44.5	44.5
05:00-05:59	10.5	5.2	56.1	<0.1	6.6	55.8	44.3	44.3
06:00-06:59	10.4	5.0	56.3	<0.1	6.6	56.8	44.8	44.8
07:00-07:59	10.5	5.2	56.3	<0.1	6.6	56.3	43.7	43.7
08:00-08:59	10.6	5.6	56.9	<0.1	6.5	48.3	37.5	37.5
09:00-09:59	9.8	10.9	96.1	3.6	5.2	51.5	40.8	40.8
10:00-10:59	11.2	5.2	58.0	<0.1	6.2	45.4	36.5	36.5
11:00-11:59	11.2	5.3	58.7	<0.1	6.2	44.0	34.8	34.8
12:00-12:59	11.2	5.4	59.5	<0.1	6.2	43.3	33.5	33.5
13:00-13:59	11.2	5.5	59.1	<0.1	6.1	42.1	33.1	33.1
14:00-14:59	11.2	5.7	59.4	0.1	6.1	42.2	32.1	32.1
15:00-15:59	11.2	5.6	59.9	<0.1	6.1	40.6	32.2	32.2
16:00-16:59	11.3	5.2	58.8	<0.1	6.1	41.8	32.0	32.0
17:00-17:59	11.3	5.0	59.2	<0.1	6.0	40.0	31.2	31.2
18:00-18:59	13.5	6.1	63.2	0.2	4.5	1.2	2.1	2.1
19:00-19:59	12.4	5.2	67.0	<0.1	5.3	0.9	1.6	1.6
20:00-20:04	12.5	5.2	62.1	<0.1	5.2	0.5	6.0	6.0

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/06/89

Test #:

8

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
09:32-09:59	13.2	6.2	58.9	0.2	4.8	10.0	23.6	
10:00-10:59	11.0	10.1	90.3	4.4	4.1	0.7	2.6	
11:00-11:19	13.1	5.9	59.0	<0.1	4.8	0.6	1.5	
14:30-14:59	13.3	5.6	47.4	<0.1	4.8	0.9	1.0	
15:00-15:59	13.3	5.6	48.1	<0.1	4.8	0.6	1.4	
16:00-16:59	13.0	5.0	50.4	<0.1	5.0	0.5	1.3	
17:00-17:59	12.2	3.7	58.2	<0.1	5.6	0.6	1.1	
18:00-18:59	12.2	3.8	56.1	<0.1	5.6	0.5	1.2	
19:00-19:59	12.3	4.0	55.6	<0.1	5.5	0.7	1.1	
20:00-20:59	12.3	4.0	56.5	<0.1	5.5	0.5	1.1	
21:00-21:59	12.3	4.1	56.2	0.1	5.5	0.4	1.0	
22:00-22:59	12.2	4.4	58.5	0.5	5.5	0.6	1.0	
23:00-23:59	12.3	4.5	55.4	0.2	5.5	0.7	1.2	

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/07/89

Test #:

8

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	12.3	4.4	53.6	<0.1	5.5	0.5		1.2
01:00-01:59	12.2	4.3	54.3	<0.1	5.6	0.6		1.3
02:00-02:59	12.1	4.3	54.5	<0.1	5.6	0.6		1.2
03:00-03:59	12.2	4.3	54.5	<0.1	5.6	0.5		1.3
04:00-04:59	12.2	4.4	54.5	<0.1	5.5	0.4		1.4
05:00-05:59	13.3	4.4	46.1	0.2	4.7	0.7		1.2
06:00-06:21	19.6	4.2	<0.1	1.1	0.3	0.7		1.3
09:51-09:53	11.8	4.9	70.0	0.1	5.8	<0.1		7.7
13:58-13:59	11.5	3.4	64.2	0.1	6.2	<0.1		0.8
14:05-14:22	12.1	3.8	60.7	<0.1	5.7	0.8		1.2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/08/89

Test #:

8

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
09:37-08:59	19.9	4.4	5.2	5.2	0.4	0.7	2.5	
09:00-09:15	17.0	5.0	2.3	23.4	0.4	<0.1	26.5	
12:33-12:59	18.1	19.4	5.1	1.0	0.9	<0.1	<0.1	
13:00-13:48	17.5	21.3	8.7	0.6	1.3	<0.1	<0.1	

July 1990  
Revision: Final

TEST RUN 13  
500°F/12 HOURS

1311R2

HANTHORNE ARMY AMMUNITION PLANT  
HANTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/09/89

Test #:

13

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
20:26-20:59	14.5	18.2	24.4	<0.1	3.4	<0.1	<0.1	<0.1
21:00-21:59	14.1	13.5	30.4	<0.1	3.7	<0.1	<0.1	<0.1
22:00-22:59	13.0	7.9	45.2	<0.1	4.5	<0.1	<0.1	<0.1
23:00-23:59	11.7	4.2	64.2	<0.1	5.3	<0.1	<0.1	<0.1



HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - DAILY AVERAGE

Test Date: 08/10/89

Test #:

13

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.0	3.8	73.6	<0.1	6.5	4.7	7.9	7.9
01:00-01:59	9.3	3.7	52.8	<0.1	7.0	28.4	26.5	26.5
02:00-02:59	9.0	3.7	52.9	<0.1	7.2	49.4	35.1	35.1
03:00-03:59	7.8	3.6	55.5	<0.1	8.0	71.8	50.8	50.8
04:00-04:59	7.2	3.5	62.2	<0.1	8.5	59.2	42.1	42.1
05:00-05:59	7.1	3.6	55.4	<0.1	8.5	46.0	31.0	31.0
06:00-06:59	7.3	3.8	65.3	<0.1	8.4	44.6	31.5	31.5
07:00-07:59	7.7	4.0	56.6	<0.1	8.1	33.9	24.4	24.4
08:00-08:59	7.5	4.2	52.5	<0.1	8.3	47.0	24.2	24.2
09:00-09:59	8.0	4.7	49.1	<0.1	7.9	53.1	31.9	31.9
10:00-10:59	8.4	4.7	49.0	<0.1	7.6	51.9	26.8	26.8
11:00-11:40	8.0	9.9	72.8	1.5	6.7	43.9	26.2	26.2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/11/89

Test #:

13

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	TAC (ppm)
09:59-11:40	9.8	6.6	101.6	38.9	6.6	<0.1		46.5
10:00-11:59	8.6	18.8	119.6	8.1	6.6	<0.1		8.8
11:00-11:59	9.1	4.6	142.2	3.0	5.9	11.7		9.2
12:00-12:59	9.6	3.8	101.8	<0.1	7.2	0.9		2.0
13:00-13:59	9.6	3.9	102.3	<0.1	7.2	1.1		1.8
14:00-14:59	9.6	3.7	104.1	<0.1	7.2	1.1		1.8
15:00-15:59	9.5	3.7	105.7	<0.1	7.2	0.9		1.9
16:00-16:59	9.5	3.7	105.0	<0.1	7.2	0.7		1.6
17:00-17:59	9.5	3.7	105.9	<0.1	7.2	0.9		1.8
18:00-18:59	9.5	3.6	107.4	<0.1	7.2	0.6		1.7
19:00-19:59	9.4	3.3	108.0	<0.1	7.3	0.9		1.4
20:00-20:59	9.4	2.9	108.4	<0.1	7.3	0.5		1.4
21:00-21:59	9.4	2.8	109.3	<0.1	7.3	0.5		1.3
22:00-22:59	9.4	2.9	107.8	<0.1	7.3	0.5		1.3
23:00-23:59	9.4	3.0	104.3	<0.1	7.3	0.5		1.2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/12/89

Test #: 13

Test Time	Afterburner Outlet			Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	HC <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)
00:00-00:59	9.4	2.9	102.0	<0.1	7.3	0.6	1.1
01:00-01:59	9.5	2.9	101.8	<0.1	7.3	0.5	1.2
02:00-02:59	9.5	2.9	102.2	<0.1	7.2	0.7	1.1
03:00-03:59	9.5	3.0	100.6	<0.1	7.2	0.5	1.2
04:00-04:59	9.5	3.0	101.7	<0.1	7.2	0.5	1.2
05:00-05:59	9.6	2.9	101.8	<0.1	7.2	0.4	1.3
06:00-06:59	9.6	2.8	101.0	<0.1	7.1	0.4	1.2
07:00-07:59	9.7	3.1	100.8	<0.1	7.1	0.5	1.2
08:00-08:59	9.9	3.6	100.6	<0.1	7.0	0.4	1.5
09:00-09:59	10.0	4.6	99.4	<0.1	6.9	0.7	1.6
10:00-10:59	9.7	8.5	107.5	4.4	5.8	8.1	8.3
11:00-11:59	10.0	3.7	98.7	<0.1	7.0	0.6	1.8
12:00-12:51	10.0	3.8	101.1	<0.1	6.9	0.5	1.6

July 1990  
Revision: Final

TEST RUN 14  
400°F/12 HOURS

1311R2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/15/89

Test #:

14

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
07:58-07:59	19.3	4.2	<0.1	<0.1	0.2	<0.1	<0.1	<0.1
08:00-08:59	13.1	20.6	106.0	7.8	3.6	4.9	5.2	5.2
09:00-09:59	19.4	5.3	1.4	7.4	0.4	0.7	2.0	2.0
10:00-10:59	18.5	20.7	5.9	2.6	1.0	10.9	11.0	11.0
11:00-11:59	18.0	21.9	5.3	2.2	1.3	0.5	3.4	3.4
12:00-12:59	18.1	21.5	8.2	1.7	1.3	0.4	2.3	2.3
13:00-13:59	18.1	21.3	8.1	1.4	1.3	0.4	2.0	2.0
14:00-14:59	17.9	22.1	9.4	1.6	1.4	0.4	1.9	1.9
15:00-15:59	17.3	24.1	12.0	2.4	1.8	0.4	1.6	1.6
16:00-16:59	16.5	25.6	14.1	2.4	2.3	0.4	1.9	1.9
17:00-17:59	15.8	22.5	19.4	1.6	2.8	0.5	1.9	1.9
18:00-18:59	15.0	16.8	27.8	0.9	3.4	0.5	1.8	1.8
19:00-19:59	13.9	10.0	41.9	0.3	4.2	0.5	1.4	1.4
20:00-20:59	12.7	5.3	53.5	<0.1	5.1	0.4	1.2	1.2
21:00-21:59	11.1	3.4	92.9	<0.1	6.2	4.2	1.1	1.1
22:00-22:59	10.5	3.7	53.5	<0.1	6.5	10.5	10.3	10.3
23:00-23:59	10.2	3.6	57.0	<0.1	6.8	23.5	23.6	23.6

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/16/89

Test #:

14

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	9.1	3.3	57.4	<0.1	7.6	35.4	35.4	26.4
01:00-01:59	8.7	3.4	63.2	<0.1	7.9	38.2	38.2	28.7
02:00-02:59	8.8	3.4	68.9	<0.1	7.8	42.3	42.3	29.2
03:00-03:59	10.8	3.3	62.1	<0.1	6.4	57.7	57.7	44.2
04:00-04:59	10.8	3.1	63.1	<0.1	6.3	60.0	60.0	42.9
05:00-05:59	10.4	3.1	69.5	<0.1	6.6	59.9	59.9	43.1
06:00-06:59	10.4	3.3	53.2	<0.1	6.6	62.4	62.4	44.2
07:00-07:59	11.0	3.2	54.2	<0.1	6.3	51.3	51.3	37.1
08:00-08:59	11.2	9.6	77.7	6.0	5.4	43.4	43.4	35.6
09:00-09:59	9.5	3.9	63.2	<0.1	7.3	33.5	33.5	30.7
10:00-10:59	9.2	3.9	65.7	<0.1	7.5	31.8	31.8	26.2
11:00-11:59	9.2	3.9	67.6	<0.1	7.5	28.8	28.8	23.6
12:00-12:59	9.4	4.0	59.1	<0.1	7.4	26.0	26.0	21.1
13:00-13:59	9.4	4.2	70.7	<0.1	7.3	23.1	23.1	20.6
14:00-14:59	11.7	5.1	104.1	<0.1	5.7	1.4	1.4	2.1
15:00-15:59	12.1	4.2	89.4	<0.1	5.4	1.1	1.1	1.8
16:00-16:59	12.4	4.2	82.4	<0.1	5.2	0.7	0.7	2.0
17:00-17:59	12.4	4.1	76.4	<0.1	5.2	0.9	0.9	1.6
18:00-18:59	12.4	4.0	73.7	<0.1	5.2	0.8	0.8	1.5
19:00-19:59	12.5	3.7	70.4	<0.1	5.1	0.5	0.5	1.5
20:00-20:59	12.5	3.5	69.2	<0.1	5.1	0.4	0.4	1.4
21:00-21:59	12.6	3.5	67.7	<0.1	5.1	0.5	0.5	1.2
22:00-22:59	12.7	3.5	67.4	<0.1	5.0	0.6	0.6	1.1
23:00-23:59	12.7	3.8	66.8	<0.1	5.0	0.4	0.4	1.4

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/17/89

Test #:

14

Test Time	Afterburner Outlet			Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)
00:00-00:59	12.7	4.0	65.4	<0.1	5.0	0.4	1.4
01:00-01:59	12.8	3.8	62.8	<0.1	4.9	0.5	1.2
02:00-02:59	12.8	4.1	62.2	<0.1	4.9	0.6	1.1
03:00-03:59	12.9	3.9	63.1	<0.1	4.8	0.4	1.2
04:00-04:59	13.0	3.9	61.5	<0.1	4.8	0.3	1.1
05:00-05:59	13.0	4.1	61.4	<0.1	4.8	0.5	1.0
06:00-06:59	13.0	3.9	61.0	<0.1	4.8	0.3	1.1
07:00-07:59	13.1	4.2	59.9	<0.1	4.7	0.4	1.0
08:00-08:59	11.5	4.3	78.1	<0.1	5.8	0.4	1.5
09:00-09:59	12.1	11.8	67.9	6.4	6.1	18.6	10.2
10:00-10:59	9.8	7.3	135.3	10.9	4.8	0.6	1.6
11:00-11:59	10.1	4.2	104.6	0.2	6.8	0.5	1.6
12:00-12:59	10.3	3.7	99.3	0.2	6.7	0.7	1.3
13:00-13:59	10.1	3.4	100.9	0.2	6.7	0.4	1.3
14:00-14:59	11.7	3.5	79.6	0.2	5.7	0.4	1.2
15:00-15:59	10.2	3.9	102.6	0.3	6.7	0.6	1.5
16:00-16:59	10.2	3.8	103.0	0.2	6.7	0.7	1.5
17:00-17:59	10.1	3.5	103.0	0.2	6.8	0.4	1.4
18:00-18:59	9.9	3.2	103.3	0.1	6.9	0.4	1.2
19:00-19:59	9.9	3.0	102.7	0.1	6.9	0.4	1.0
20:00-20:59	9.9	2.9	102.2	0.1	6.9	0.5	0.9
21:00-21:59	10.0	2.9	100.7	0.1	6.9	0.3	1.0
22:00-22:59	10.1	2.9	99.6	0.1	6.8	0.3	1.0
23:00-23:59	10.1	3.2	99.9	0.2	6.8	0.5	1.0

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/13/89

Test #:

14

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.1	3.2	98.9	0.2	6.8	0.3	1.1	1.1
01:00-01:59	10.1	3.1	98.0	0.2	6.8	0.4	1.0	1.0
02:00-02:59	10.2	3.1	97.6	0.2	6.8	0.3	0.9	0.9
03:00-03:59	10.2	2.9	96.2	0.1	6.8	0.4	0.8	0.8
04:00-04:59	10.2	2.8	95.7	0.1	6.8	0.3	0.9	0.9
05:00-05:59	10.2	2.8	94.7	0.1	6.8	0.3	0.9	0.9
06:00-06:59	10.3	2.9	94.2	0.1	6.7	0.4	0.9	0.9
07:00-07:59	10.3	2.9	93.2	0.1	6.7	0.3	1.0	1.0
08:00-08:59	10.4	3.4	91.5	0.2	6.6	7.7	1.1	1.1
09:00-09:59	13.6	10.5	75.2	10.1	2.7	2.4	10.5	10.5
10:00-10:29	19.6	4.6	0.2	1.1	0.2	0.7	1.0	1.0



July 1990  
Revision: Final

TEST RUN 15  
600°F/12 HOURS

1311R2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/22/89

Test #: 15

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
08:49-08:59	19.9	3.5	<0.1	<0.1	0.2	<0.1	<0.1	<0.1
09:00-09:59	15.6	8.0	40.2	6.0	1.1	0.9	9.6	9.6
10:00-10:54	14.2	9.4	75.5	3.7	1.3	12.3	12.1	12.1
11:13-11:59	17.9	20.0	7.9	1.0	1.2	0.7	2.4	2.4
12:00-12:59	17.6	20.8	9.0	0.9	1.3	0.9	1.8	1.8
13:00-13:59	17.6	20.6	9.1	0.8	1.3	0.8	1.6	1.6
14:00-14:59	17.6	20.5	9.0	0.8	1.3	0.6	1.6	1.6
15:00-15:59	17.3	21.7	10.3	1.1	1.4	0.9	1.6	1.6
16:00-16:59	17.0	23.3	12.1	1.6	1.7	0.6	1.7	1.7
17:00-17:59	16.3	24.9	14.2	1.9	2.1	0.5	1.8	1.8
18:00-18:59	15.4	22.6	19.7	0.9	2.8	0.5	1.6	1.6
19:00-19:59	14.5	15.6	31.2	0.1	3.5	0.6	1.2	1.2
20:00-20:59	13.4	10.5	44.9	<0.1	4.2	0.6	1.1	1.1
21:00-21:59	12.2	5.8	65.5	<0.1	5.1	0.5	1.2	1.2
22:00-22:59	10.8	3.7	88.9	<0.1	6.1	0.5	1.2	1.2
23:00-23:59	9.6	3.0	75.9	<0.1	6.9	18.7	20.4	20.4

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/23/89

Test #:

15

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	8.8	3.0	56.9	<0.1	7.5	45.0	39.7	39.7
01:00-01:59	7.6	3.0	73.3	<0.1	8.4	50.9	43.0	43.0
02:00-02:59	7.1	3.0	95.1	<0.1	8.7	54.5	59.1	59.1
03:00-03:59	6.8	2.8	82.9	<0.1	8.9	54.4	41.1	41.1
04:00-04:59	6.1	3.0	64.0	<0.1	9.4	49.3	32.3	32.3
05:00-05:59	6.2	3.2	62.4	<0.1	9.3	37.1	22.2	22.2
06:00-06:59	6.7	3.1	63.1	<0.1	9.1	42.1	23.1	23.1
07:00-07:59	6.6	3.2	63.3	<0.1	9.1	42.3	23.1	23.1
08:00-08:59	6.7	3.1	62.5	<0.1	9.0	39.5	21.5	21.5
09:00-09:59	8.1	8.5	90.5	8.9	5.4	34.6	23.1	23.1
10:00-10:59	5.4	3.1	109.3	0.9	7.1	36.1	18.6	18.6
11:00-11:59	7.0	3.1	56.0	0.3	6.8	34.8	18.7	18.7
12:00-12:59	7.5	3.0	57.4	0.3	8.5	32.2	15.7	15.7
13:00-13:59	6.9	3.2	58.7	0.5	8.9	34.7	17.0	17.0
14:00-14:59	7.1	3.2	57.5	0.4	8.8	34.1	15.7	15.7
15:00-15:59	7.0	3.0	58.7	0.4	8.8	34.8	17.1	17.1
16:00-16:59	6.9	2.8	58.4	0.3	8.9	37.7	16.7	16.7
17:00-17:59	6.8	2.7	58.0	0.3	8.9	39.0	17.8	17.8
18:00-18:59	6.8	2.6	57.8	0.3	9.0	40.3	17.6	17.6
19:00-19:24	6.8	2.6	56.3	0.4	9.0	46.3	17.9	17.9

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/24/89

Test #: 15

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	HC <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
09:14-09:59	11.2	2.6	87.2	0.5	5.9	0.5	1.5	
10:00-10:59	10.8	2.8	92.3	0.5	6.2	0.7	1.3	
11:00-11:59	9.4	2.9	104.4	0.5	7.2	0.7	1.4	
12:00-12:59	9.3	3.2	106.5	0.5	7.2	0.6	1.6	
13:00-13:59	9.4	3.4	106.0	0.5	7.1	0.8	1.5	
14:00-14:59	9.5	3.3	104.6	0.5	7.1	0.7	1.5	
15:00-15:59	9.4	3.3	108.2	0.5	7.1	0.5	1.6	
16:00-16:59	9.4	3.2	106.7	0.5	7.1	0.7	1.2	
17:00-17:59	9.4	3.0	106.7	0.5	7.1	0.5	1.4	
18:00-18:59	9.4	2.8	106.3	0.4	7.1	0.7	1.2	
19:00-19:59	9.3	2.6	107.4	0.4	7.1	0.6	1.0	
20:00-20:59	9.4	2.6	107.2	0.4	7.1	0.5	1.1	
21:00-21:59	9.4	2.6	105.7	0.4	7.1	0.5	1.1	
22:00-22:59	9.3	2.5	107.5	0.4	7.2	0.5	1.0	
23:00-23:59	9.3	2.6	106.5	0.4	7.2	0.6	0.9	

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/25/89

Test #:

15

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	9.3	2.6	107.4	0.4	7.2	0.5	1.6	1.6
01:00-01:59	9.4	2.7	105.8	0.4	7.1	0.5	1.1	1.1
02:00-02:59	9.4	2.5	104.5	0.4	7.1	0.5	0.9	0.9
03:00-03:59	9.3	2.5	103.2	0.4	7.2	0.5	0.9	0.9
04:00-04:59	9.4	2.4	103.7	0.4	7.1	0.4	1.0	1.0
05:00-05:59	9.4	2.4	103.3	0.4	7.1	0.4	0.9	0.9
06:00-06:59	9.4	2.5	102.3	0.4	7.1	0.5	0.9	0.9
07:00-07:59	9.5	2.5	95.4	0.4	7.0	0.5	0.9	0.9
08:00-08:59	10.2	3.1	87.4	3.4	6.2	6.9	8.0	8.0
09:00-09:59	8.0	9.7	190.5	1.9	2.5	0.7	2.1	2.1
10:00-10:59	10.7	3.0	98.9	0.6	6.3	0.6	1.3	1.3
11:00-11:59	10.7	3.0	99.5	0.5	6.2	0.5	1.4	1.4
12:00-12:59	10.7	3.1	99.4	0.5	6.2	0.6	1.3	1.3
13:00-13:59	10.7	3.2	100.0	0.5	6.2	0.5	1.2	1.2
14:00-14:59	10.7	3.2	100.2	0.5	6.2	0.4	1.4	1.4
15:00-15:59	10.3	3.0	100.5	0.5	6.4	0.5	1.3	1.3
16:00-16:59	9.6	3.0	105.5	0.5	6.9	0.4	1.3	1.3
17:00-17:59	9.5	3.0	105.2	0.5	6.9	0.5	1.2	1.2
18:00-18:59	9.5	2.9	103.6	0.5	7.0	0.5	1.1	1.1
19:00-19:59	9.5	2.7	101.4	0.4	7.0	0.4	1.1	1.1
20:00-20:59	9.4	2.6	103.0	0.4	7.1	0.5	0.9	0.9
21:00-21:59	9.5	2.6	102.5	0.4	7.0	0.4	1.0	1.0
22:00-22:59	9.5	2.7	104.3	0.4	7.0	0.4	1.0	1.0
23:00-23:59	9.5	2.6	103.3	0.4	7.0	0.3	1.0	1.0

HAUTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/26/89

Test #:

15

Test Time	Afterburner Outlet				Flash Chamber Inlet	Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)		THC (ppm)	THC (ppm)
00:00-00:59	9.5	2.6	102.7	0.4	0.5	0.5	0.9
01:00-01:59	9.5	2.6	104.4	0.4	0.3	0.3	0.9
02:00-02:59	9.5	2.6	103.2	0.4	0.4	0.4	0.9
03:00-03:59	9.6	2.6	102.3	0.4	0.3	0.3	0.9
04:00-04:59	9.6	2.5	102.0	0.4	0.4	0.4	0.8
05:00-05:59	9.6	2.5	102.6	0.4	0.3	0.3	0.9
06:00-06:59	9.6	2.6	101.9	0.4	0.4	0.4	0.8
07:00-07:59	9.5	6.6	106.6	3.6	4.7	4.7	9.3
08:00-08:59	9.9	3.0	96.5	0.5	0.4	0.4	1.3
09:00-09:59	9.9	3.1	94.4	0.5	0.5	0.5	1.4
10:00-10:59	9.9	3.2	97.0	0.5	0.5	0.5	1.5
11:00-11:59	9.9	3.2	98.6	0.5	0.6	0.6	1.5
12:00-12:59	9.9	3.2	99.4	0.5	0.5	0.5	1.5
13:00-13:59	9.9	3.3	100.2	0.5	0.7	0.7	1.4
14:00-14:59	9.9	3.4	101.1	0.5	0.7	0.7	1.4
15:00-15:59	9.9	3.3	102.3	0.5	0.5	0.5	1.5
16:00-16:59	9.8	3.2	101.5	0.5	0.7	0.7	1.3
17:00-17:59	9.7	3.1	101.3	0.5	0.6	0.6	1.3
18:00-18:59	9.7	3.0	98.9	0.4	0.4	0.4	1.3
19:00-19:59	9.6	2.8	97.0	0.4	0.5	0.5	1.1
20:00-20:59	9.6	2.7	96.7	0.4	0.5	0.5	1.0
21:00-21:59	9.6	2.7	96.0	0.4	0.4	0.4	1.1
22:00-22:59	9.7	2.7	97.1	0.4	0.5	0.5	0.9
23:00-23:59	9.7	2.6	99.4	0.4	0.4	0.4	1.0

July 1990  
Revision: Final

TEST RUN 16  
600°F/6 HOURS

1311R2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/27/89

Test #: 16

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	9.7	2.6	96.6	0.4	6.9	0.5	0.9	0.9
01:00-01:59	9.7	2.7	95.4	0.4	6.9	0.4	1.0	1.0
02:00-02:59	9.7	2.7	96.9	0.4	6.9	0.4	1.0	1.0
03:00-03:59	9.7	2.7	97.2	0.4	6.9	0.4	1.0	1.0
04:00-04:59	9.7	2.6	97.2	0.4	6.9	0.5	0.9	0.9
05:00-05:59	9.8	2.8	96.1	0.4	6.9	0.3	1.0	1.0
06:00-06:59	9.8	2.5	95.6	0.4	6.9	0.3	3.0	3.0
07:00-07:59	11.4	2.8	79.4	0.6	5.7	3.9	41.2	41.2
08:00-08:59	11.4	13.1	81.3	9.6	2.1	6.5	9.3	9.3
09:00-09:59	9.7	8.3	145.1	3.8	1.0	7.9	5.7	5.7
10:35-10:59	18.5	16.5	3.8	3.2	0.8	1.0	3.9	3.9
11:00-11:59	17.8	22.4	7.7	2.4	1.3	1.1	2.6	2.6
12:00-12:59	17.8	22.3	8.1	2.3	1.3	1.1	2.1	2.1
13:00-13:59	17.8	21.4	8.1	1.9	1.3	1.0	2.1	2.1
14:00-14:59	17.7	22.0	8.8	1.8	1.4	0.9	1.9	1.9
15:00-15:59	17.4	22.8	9.9	1.9	1.6	1.2	1.9	1.9
16:00-16:59	16.7	24.9	12.5	2.4	2.0	1.0	1.9	1.9
17:00-17:59	15.9	24.2	15.6	1.8	2.6	0.9	1.9	1.9
18:00-18:59	15.2	19.7	22.4	1.1	3.1	1.1	1.7	1.7
19:00-19:59	14.3	12.5	33.1	0.6	3.8	1.0	1.8	1.8
20:00-20:59	12.9	8.2	52.8	0.3	4.9	1.0	1.7	1.7
21:00-21:59	11.4	3.3	76.8	0.3	5.9	1.1	1.7	1.7
22:00-22:05	10.7	2.8	86.8	0.2	6.5	<0.1	1.4	1.4



HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/29/89

Test #:

16

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
08:27-08:59	10.1	3.5	11.2	<0.1	6.7	1.0	1.3	1.3
09:00-09:59	10.7	3.3	3.6	<0.1	6.3	0.4	1.2	1.2
10:00-10:59	10.8	3.3	0.6	<0.1	6.3	0.3	1.3	1.3
11:00-11:59	10.7	3.4	0.7	<0.1	6.3	0.5	1.2	1.2
12:00-12:59	10.8	3.5	0.5	<0.1	6.2	0.4	1.4	1.4
13:00-13:59	10.8	3.6	56.4	<0.1	6.2	0.4	1.3	1.3
14:00-14:59	10.8	4.1	8.2	<0.1	6.2	0.7	1.3	1.3
15:00-15:59	11.1	7.5	<0.1	1.7	5.9	5.0	10.6	10.6
16:00-16:59	10.9	3.6	50.0	<0.1	6.2	1.5	3.7	3.7
17:00-17:59	10.8	3.6	105.6	<0.1	6.2	0.9	1.8	1.8
18:00-18:59	10.8	3.3	104.1	<0.1	6.2	1.3	1.9	1.9
19:00-19:59	10.8	3.1	105.1	<0.1	6.2	0.5	1.4	1.4
20:00-20:59	10.8	3.2	103.3	<0.1	6.2	0.6	1.3	1.3
21:00-21:59	10.8	3.0	101.0	<0.1	6.2	0.5	1.2	1.2
22:00-22:59	10.7	3.1	103.9	<0.1	6.2	0.5	1.1	1.1
23:00-23:59	10.8	3.2	103.3	<0.1	6.2	0.5	0.9	0.9

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 08/30/19  
Test #:

16

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.8	3.0	100.9	<0.1	6.2	0.3	0.9	0.9
01:00-01:59	10.8	2.8	101.8	<0.1	6.2	0.4	1.0	1.0
02:00-02:59	10.8	2.8	103.1	<0.1	6.2	0.5	0.9	0.9
03:00-03:59	10.8	2.8	103.0	<0.1	6.2	0.3	0.9	0.9
04:00-04:59	10.7	2.9	105.1	<0.1	6.3	0.2	0.8	0.8
05:00-05:59	10.7	2.9	104.8	<0.1	6.3	0.4	0.7	0.7
06:00-06:59	10.6	3.0	103.9	<0.1	6.2	0.2	0.9	0.9
07:00-07:59	10.7	2.9	103.7	<0.1	6.2	0.2	0.9	0.9
08:00-08:59	10.8	2.9	99.9	<0.1	6.2	0.3	0.7	0.7
09:00-09:25	15.0	3.3	52.3	0.1	3.2	0.6	0.7	0.7

July 1990  
Revision: Final

TEST RUN 17  
600°F/48 HOURS

1311R2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/01/89

Test #: 17

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
10:20-10:59	19.3	2.9	0.4	8.0	0.2	0.7	11.9	
11:00-11:59	18.9	8.5	1.9	6.8	0.4	0.7	10.3	
12:00-12:59	17.8	22.3	8.8	5.9	1.2	1.0	7.0	
13:00-13:59	17.5	22.8	9.4	4.3	1.3	0.7	6.9	
14:00-14:59	17.7	22.4	9.2	3.7	1.3	1.0	5.8	
15:00-15:59	17.6	25.2	9.7	5.0	1.4	0.7	11.5	
16:00-16:59	17.2	28.3	12.3	7.5	1.6	1.0	12.4	
17:00-17:59	16.6	30.7	15.2	5.2	2.0	0.6	8.5	
18:00-18:59	15.8	30.8	18.9	2.8	2.6	0.9	6.2	
19:00-19:59	15.1	24.3	24.2	1.2	3.1	0.8	4.9	
20:00-20:59	14.0	14.6	38.2	0.3	3.9	0.5	3.8	
21:00-21:59	12.9	6.8	56.8	<0.1	4.7	0.7	2.6	
22:00-22:59	11.6	3.5	79.8	<0.1	5.7	0.6	2.2	
23:00-23:59	10.9	3.0	71.2	<0.1	6.3	19.4	20.8	

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/02/89

Test #:

17

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.9	2.6	48.1	<0.1	6.3	39.7	51.7	51.7
01:00-01:59	10.5	2.5	52.0	<0.1	6.5	44.2	59.7	59.7
02:00-02:59	10.1	2.4	53.7	<0.1	6.8	54.7	53.7	53.7
03:00-03:59	9.5	2.3	55.0	<0.1	7.4	50.4	47.6	47.6
04:00-04:59	7.9	2.4	54.6	<0.1	8.6	71.2	57.6	57.6
05:00-05:59	6.9	2.5	53.6	<0.1	9.3	66.0	50.5	50.5
06:00-06:59	6.1	2.5	54.6	<0.1	9.8	45.8	30.2	30.2
07:00-07:59	6.6	2.6	56.2	<0.1	9.5	40.3	26.1	26.1
08:00-08:59	6.2	3.1	57.9	<0.1	9.8	33.2	21.4	21.4
09:00-09:59	8.2	9.6	124.7	9.3	7.1	30.0	21.3	21.3
10:00-10:59	6.0	3.4	93.4	2.4	8.8	29.4	19.3	19.3
11:00-11:59	6.1	3.1	57.8	0.1	9.9	29.6	18.5	18.5
12:00-12:59	6.1	3.2	58.6	0.1	9.9	28.7	17.9	17.9
13:00-13:59	6.2	3.3	59.1	0.1	9.8	25.4	16.4	16.4
14:00-14:59	6.5	3.2	59.4	0.1	9.5	25.6	16.4	16.4
15:00-15:59	6.5	3.2	61.5	0.1	9.5	32.1	17.6	17.6
16:00-16:59	6.5	3.2	60.7	0.1	9.5	38.3	19.1	19.1
17:00-17:59	6.4	3.1	59.8	0.1	9.6	39.5	19.1	19.1
18:00-18:59	6.8	3.2	58.3	<0.1	9.3	45.5	19.7	19.7
19:00-19:59	7.1	2.7	56.9	<0.1	9.1	49.1	22.6	22.6
20:00-20:59	6.9	2.7	56.2	<0.1	9.3	48.9	21.3	21.3
21:00-21:59	7.0	2.7	56.6	<0.1	9.2	58.5	22.7	22.7
22:00-22:59	7.0	2.8	58.3	<0.1	9.2	54.1	22.4	22.4
23:00-23:59	6.9	2.8	57.9	<0.1	9.3	51.3	22.2	22.2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/03/89

Test #: 17

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	6.9	2.9	59.1	<0.1	9.3	54.5	23.1	23.1
01:00-01:59	6.9	2.7	59.5	<0.1	9.3	54.5	23.3	23.3
02:00-02:59	6.8	2.6	59.2	<0.1	9.4	53.7	22.2	22.2
03:00-03:59	6.8	2.7	59.2	0.1	9.4	58.6	24.0	24.0
04:00-04:59	6.8	2.9	58.7	<0.1	9.4	53.9	25.2	25.2
05:00-05:59	6.6	2.7	58.1	0.1	9.5	55.4	21.6	21.6
06:00-06:59	6.6	2.6	57.8	0.1	9.6	55.3	24.1	24.1
07:00-07:59	6.7	2.8	58.7	<0.1	9.5	60.0	25.0	25.0
08:00-08:59	7.3	7.4	123.8	4.1	6.9	49.9	20.9	20.9
09:00-09:59	7.9	3.0	70.1	0.1	8.6	52.6	41.1	41.1
10:00-10:59	7.1	2.9	63.4	<0.1	9.3	54.1	43.3	43.3
11:00-11:59	6.9	3.1	63.3	0.1	9.3	53.5	39.7	39.7
12:00-12:59	7.3	3.1	63.6	0.1	9.1	52.4	38.5	38.5
13:00-13:59	7.1	3.1	64.5	0.1	9.1	49.9	33.7	33.7
14:00-14:59	7.3	3.2	65.1	0.1	9.0	48.2	34.8	34.8
15:00-15:59	7.4	3.2	64.9	0.1	9.0	47.3	32.4	32.4
16:00-16:59	7.4	3.1	64.6	0.1	9.0	45.8	31.5	31.5
17:00-17:59	7.3	3.1	64.8	0.1	9.0	47.2	34.3	34.3
18:00-18:59	7.3	2.9	62.5	<0.1	9.1	55.5	40.1	40.1
19:00-19:59	8.3	2.8	81.4	<0.1	8.3	40.5	31.5	31.5
20:00-20:59	7.2	2.7	60.3	<0.1	9.1	69.2	48.5	48.5
21:00-21:59	7.3	2.8	60.8	<0.1	9.1	69.7	50.4	50.4
22:00-22:59	8.2	2.8	76.3	<0.1	8.4	55.1	39.4	39.4
23:00-23:59	6.8	3.0	59.3	<0.1	9.4	68.9	39.9	39.9

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/04/89

Test #:

17

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	6.9	2.8	60.5	<0.1	9.4	69.8	46.3	46.3
01:00-01:59	6.8	2.6	60.4	<0.1	9.4	72.9	45.5	45.5
02:00-02:59	8.0	2.8	81.3	<0.1	8.5	64.7	29.9	29.9
03:00-03:59	7.4	2.6	60.1	<0.1	9.0	76.3	52.3	52.3
04:00-04:59	7.9	2.7	62.0	<0.1	8.7	82.4	61.5	61.5
05:00-05:59	8.1	2.8	62.4	<0.1	8.5	83.7	63.9	63.9
06:00-06:59	8.4	2.5	63.1	<0.1	8.4	85.2	65.0	65.0
07:00-07:59	10.0	2.6	78.2	0.1	7.2	53.4	52.0	52.0
08:00-08:59	7.4	3.2	62.0	<0.1	9.1	77.3	66.0	66.0
09:00-09:59	8.0	7.8	68.3	2.9	8.2	59.3	52.0	52.0
10:00-10:59	7.6	3.3	64.5	0.2	8.9	63.6	53.1	53.1
11:00-11:59	7.7	3.3	65.6	0.2	8.8	61.1	50.5	50.5
12:00-12:59	7.7	3.3	65.8	0.2	8.8	58.7	47.6	47.6
13:00-13:59	7.7	3.4	67.2	0.2	8.8	56.1	44.8	44.8
14:00-14:59	7.7	3.5	66.9	0.2	8.8	54.1	43.5	43.5
15:00-15:59	7.6	3.6	66.6	0.3	8.8	53.3	42.8	42.8
16:00-16:59	7.6	3.5	66.6	0.2	8.8	52.5	41.0	41.0
17:00-17:59	7.6	3.4	66.5	0.2	8.9	53.7	41.6	41.6
18:00-18:59	7.5	3.2	66.1	0.2	8.9	54.5	43.4	43.4
19:00-19:59	7.4	3.0	62.0	0.1	9.0	67.0	58.1	58.1
20:00-20:59	8.1	2.9	73.0	<0.1	8.5	71.1	37.3	37.3
21:00-21:59	11.8	3.0	103.4	0.1	5.8	1.3	2.9	2.9
22:00-22:59	12.0	2.7	101.9	0.2	5.6	0.9	1.9	1.9
23:00-23:59	12.0	3.0	96.4	0.1	5.6	0.9	1.8	1.8

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/05/89

Test #:

17

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	12.0	2.9	96.9	0.2	5.6	0.8	1.8	1.8
01:00-01:59	12.2	2.9	92.2	0.2	5.5	0.8	1.7	1.7
02:00-02:59	12.4	2.6	84.5	0.2	5.3	0.8	1.4	1.4
03:00-03:59	12.6	2.5	79.0	0.2	5.1	0.7	1.5	1.5
04:00-04:59	12.8	2.8	74.5	0.2	5.0	0.7	1.4	1.4
05:00-05:59	13.0	2.6	69.6	0.2	4.9	0.6	1.5	1.5
06:00-06:59	13.2	2.7	64.5	0.1	4.7	0.6	1.4	1.4
07:00-07:59	13.3	2.9	62.0	0.2	4.6	0.8	1.3	1.3
08:00-08:59	11.8	3.2	87.7	0.2	5.7	0.7	1.4	1.4
09:00-09:59	9.8	4.3	109.5	2.8	6.7	4.9	7.2	7.2
10:00-10:59	10.5	7.1	130.6	5.7	6.1	1.1	2.7	2.7
11:00-11:59	9.5	3.4	122.6	0.3	7.5	0.9	2.0	2.0
12:00-12:59	9.6	3.4	123.7	0.3	7.4	1.0	1.8	1.8
13:00-13:59	9.6	3.5	122.3	0.3	7.4	0.9	1.9	1.9
14:00-14:59	9.6	3.6	124.3	0.3	7.4	0.9	2.0	2.0
15:00-15:59	9.6	3.7	125.7	0.3	7.4	1.0	2.1	2.1
16:00-16:59	9.6	3.6	125.0	0.3	7.3	1.2	1.8	1.8
17:00-17:59	9.6	3.6	124.9	0.3	7.4	1.1	1.6	1.6
18:00-18:59	9.6	3.7	125.9	0.3	7.4	0.8	1.9	1.9
19:00-19:59	9.6	3.0	119.3	0.2	7.3	0.9	1.5	1.5
20:00-20:59	9.5	2.7	120.4	0.1	7.4	0.7	1.4	1.4
21:00-21:59	9.6	2.9	122.0	0.1	7.3	0.8	1.3	1.3
22:00-22:59	9.6	2.9	120.9	0.1	7.3	0.6	1.4	1.4
23:00-23:59	9.6	2.8	119.5	<0.1	7.3	0.6	1.3	1.3



HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/06/89

Test #:

17

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	9.6	2.9	117.2	<0.1	7.3	0.7	1.2	
01:00-01:42	9.7	2.8	114.1	<0.1	7.2	0.6	1.5	
20:09-20:59	9.8	3.0	127.8	0.2	6.9	1.4	1.3	
21:00-21:59	10.0	2.7	112.6	<0.1	6.9	0.5	1.1	
22:00-22:59	10.1	2.5	111.0	<0.1	6.9	0.6	0.9	
23:00-23:11	10.1	2.4	109.4	0.2	6.8	<0.1	0.8	

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/08/89

Test #:

17

Test Time	Afterburner Outlet			Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)

10:25-23:11	19.5	3.2	<0.1	<0.1	9.2	<0.1	<0.1
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July 1990  
Revision: Final

TEST RUN 18  
500°F/6 HOURS

1311R2

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/13/99

Test #:

18

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
08:50-08:59	17.4	13.5	22.5	<0.1	0.6	<0.1	<0.1	<0.1
09:00-09:59	11.9	31.6	0.5	<0.1	6.6	<0.1	<0.1	<0.1
10:00-10:59	11.7	18.2	162.8	<0.1	2.5	<0.1	<0.1	<0.1
11:00-11:59	17.3	27.1	8.8	<0.1	1.2	2.1	15.3	15.3
12:00-12:59	13.3	24.5	49.7	<0.1	2.8	8.4	10.7	10.7
13:00-13:59	17.2	27.7	10.5	10.0	1.5	15.9	5.7	5.7
14:00-14:59	16.4	34.2	14.0	1.8	2.0	1.9	1.9	1.9
15:00-15:59	13.1	29.9	8.7	3.6	3.4	11.3	5.0	5.0
16:00-16:59	15.8	8.3	59.8	1.1	0.9	30.9	18.3	18.3
17:00-17:59	17.3	5.9	11.7	4.4	0.5	0.9	1.9	1.9
18:00-18:59	18.8	5.4	4.2	0.4	0.5	0.9	1.5	1.5
19:00-19:59	18.6	4.3	6.0	0.3	0.6	0.9	1.5	1.5
20:00-20:59	18.5	5.9	7.1	0.3	0.7	20.4	4.3	4.3
21:00-21:59	18.6	8.8	5.3	0.5	0.7	29.8	13.9	13.9
22:00-22:59	12.9	5.3	61.9	0.3	4.9	6.1	9.4	9.4
23:00-23:59	11.0	6.2	61.6	0.2	6.3	24.4	24.8	24.8

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/14/89

Test #:

18

Test Time	Afterburner Outlet				Flash Chamber Inlet	Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)		THC (ppm)	THC (ppm)
00:00-00:59	17.7	7.3	15.4	20.4	0.9	1.4	1.4
01:00-01:59	10.2	8.7	101.5	0.4	19.2	2.9	2.9
02:00-02:59	9.8	5.3	127.0	0.1	1.4	1.1	1.1
03:00-03:59	9.9	5.1	124.7	0.1	0.3	1.0	1.0
04:00-04:59	9.9	5.5	123.9	0.1	0.8	1.0	1.0
05:00-05:59	9.9	5.5	124.0	0.1	0.8	0.9	0.9
06:00-06:59	9.9	5.1	121.7	0.1	0.7	1.0	1.0
07:00-07:59	9.9	5.7	123.2	0.1	0.7	1.0	1.0
08:00-08:59	9.6	6.4	116.4	0.1	10.7	7.7	7.7
09:00-09:59	9.8	6.5	124.9	0.2	10.1	2.6	2.6
10:00-10:59	10.5	6.6	65.3	0.2	17.6	16.3	16.3
11:00-11:59	11.1	7.6	51.6	0.2	26.2	23.9	23.9
12:00-12:59	11.1	7.1	55.1	0.2	20.8	23.3	23.3
13:00-13:59	10.1	7.0	56.7	0.2	26.1	24.4	24.4
14:00-14:59	8.4	11.9	110.3	3.4	31.7	32.0	32.0
15:00-15:59	7.6	8.5	224.8	0.2	39.2	74.3	74.3
16:00-16:59	7.2	6.6	64.0	0.1	30.2	28.9	28.9
17:00-17:59	7.0	6.7	64.9	0.1	29.2	26.3	26.3
18:00-18:59	6.7	6.7	64.0	0.1	32.7	26.9	26.9
19:00-19:59	6.3	6.8	63.2	<0.1	35.5	27.6	27.6
20:00-20:59	6.2	7.1	64.6	<0.1	36.5	25.8	25.8
21:00-21:59	7.2	6.8	72.4	0.1	32.1	26.4	26.4
22:00-22:59	7.2	6.4	71.3	<0.1	31.9	27.0	27.0
23:00-23:59	7.2	6.3	71.5	<0.1	32.1	27.1	27.1

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 05/15/89

Test #:

18

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	7.2	6.4	70.9	<0.1	9.3	33.1	27.8	
01:00-01:59	7.4	6.5	76.9	<0.1	9.1	32.9	24.0	
02:00-02:59	11.7	5.3	116.8	<0.1	5.9	1.2	4.0	
03:00-03:59	12.1	5.2	93.1	<0.1	5.5	1.1	3.1	
04:00-04:59	12.4	5.1	81.0	<0.1	5.3	0.9	3.0	
05:00-05:59	12.5	5.2	75.9	<0.1	5.2	0.9	4.6	
06:00-06:59	12.6	5.2	72.1	<0.1	5.1	1.0	5.2	
07:00-07:59	12.7	5.3	68.8	<0.1	5.1	0.9	3.6	
08:00-08:59	11.7	11.5	100.0	2.8	4.5	6.6	9.2	
09:00-09:59	11.5	5.5	121.4	0.3	4.7	0.9	1.7	
10:00-10:59	9.7	6.0	112.8	0.2	7.4	1.0	1.7	
11:00-11:59	9.8	6.0	115.5	0.2	7.3	0.8	1.9	
12:00-12:59	9.8	6.1	115.9	0.2	7.3	0.8	1.8	
13:00-13:59	9.8	5.8	115.2	0.2	7.2	0.9	1.6	
14:00-14:59	9.9	5.8	112.2	0.2	7.2	0.7	1.7	
15:00-15:59	9.9	6.0	111.9	0.2	7.1	0.9	1.6	
16:00-16:59	9.9	6.6	109.8	0.2	7.1	0.7	1.9	
17:00-17:59	9.9	6.4	111.4	0.2	7.1	0.7	1.7	
18:00-18:59	9.8	5.8	108.8	0.1	7.2	0.8	1.4	
19:00-19:59	9.8	6.8	106.7	0.1	7.2	0.7	1.4	
20:00-20:59	9.8	5.8	108.8	<0.1	7.2	0.6	1.4	
21:00-21:59	9.9	5.9	108.1	<0.1	7.1	0.7	1.1	
22:00-22:59	10.0	5.4	106.3	<0.1	7.1	0.6	1.2	
23:00-23:59	10.0	5.3	104.5	<0.1	7.0	0.6	1.2	

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/16/89

Test #:

18

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.1	5.3	103.4	<0.1	7.0	0.6	1.2	1.2
01:00-01:59	10.1	5.3	102.2	<0.1	7.0	0.5	1.2	1.2
02:00-02:59	10.1	5.1	99.5	<0.1	7.0	0.7	1.0	1.0
03:00-03:59	10.2	5.1	99.1	<0.1	6.9	0.6	1.0	1.0
04:00-04:59	10.2	5.3	97.4	<0.1	6.9	0.6	1.0	1.0
05:00-05:59	10.2	5.3	96.0	<0.1	6.9	0.5	0.9	0.9
06:00-06:59	10.2	5.8	95.0	<0.1	6.9	0.5	1.0	1.0
07:00-07:59	10.3	5.2	93.8	<0.1	6.8	0.5	1.0	1.0
08:00-08:59	11.1	8.9	89.3	7.2	3.6	29.1	16.5	16.5
09:00-09:59	10.5	5.9	92.7	5.0	6.7	6.8	10.9	10.9
10:00-10:59	10.5	6.2	92.8	0.2	6.6	1.0	1.7	1.7
11:00-11:59	10.6	5.9	93.3	0.2	6.6	0.8	2.0	2.0
12:00-12:59	10.6	5.9	92.5	0.2	6.6	0.8	1.6	1.6
13:00-13:59	10.6	5.6	94.5	0.2	6.6	0.9	1.6	1.6
14:00-14:59	10.5	5.3	95.0	<0.1	6.6	0.7	1.4	1.4
15:00-15:59	10.5	5.4	94.7	<0.1	6.6	0.7	1.4	1.4
16:00-16:59	10.4	5.3	94.9	<0.1	6.6	0.9	1.4	1.4
17:00-17:59	10.3	5.4	92.7	<0.1	6.7	1.3	1.7	1.7
18:00-18:59	10.3	5.7	91.4	<0.1	6.7	1.2	1.6	1.6
19:00-19:59	10.3	5.3	89.4	<0.1	6.7	1.0	1.3	1.3
20:00-20:59	10.3	5.7	87.6	<0.1	6.7	0.8	1.4	1.4
21:00-21:59	10.2	5.8	82.8	<0.1	6.8	0.7	1.3	1.3
22:00-22:59	10.2	5.1	76.1	<0.1	6.8	0.7	1.3	1.3
23:00-23:59	10.2	5.3	75.4	<0.1	6.8	0.8	1.1	1.1

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

SUMMARY OF CONTINUOUS EMISSIONS  
MONITORING DATA - HOURLY AVERAGES

Test Date: 09/17/89

Test #:

18

Test Time	Afterburner Outlet				Flash Chamber Inlet		Flash Chamber Outlet	
	O <sub>2</sub> (%)	CO (ppm)	NO <sub>x</sub> (ppm)	THC (ppm)	CO <sub>2</sub> (%)	THC (ppm)	THC (ppm)	THC (ppm)
00:00-00:59	10.2	5.1	75.4	<0.1	6.8	0.7	1.2	1.2
01:00-01:59	10.1	4.9	75.0	<0.1	6.8	0.6	1.2	1.2
02:00-02:59	10.1	5.2	74.2	<0.1	6.8	0.6	1.1	1.1
03:00-03:59	10.1	4.8	73.2	<0.1	6.8	0.7	1.0	1.0
04:00-04:59	10.1	4.7	72.8	<0.1	6.8	0.7	1.0	1.0
05:00-05:59	14.7	5.0	38.9	0.4	3.5	0.6	1.0	1.0



July 1990  
Revision: Final

**APPENDIX F**  
**RAW ANALYTICAL DATA SHEETS FOR TEST ITEMS**

The following information is provided in Appendix F:

- Chain of custody forms (Custody Transfer Record/Lab Work Request).
- Data summaries from onsite analytical laboratory (WESTON Analytics-Explosives).
- Data summaries from offsite analytical laboratories.

Test data are presented for pre-test and post-test sampling events. The onsite laboratory conducted analyses for explosive compounds. The offsite analytical laboratory (WESTON Analytics Division, Lionville, PA) conducted the following analyses:

- Duplicate samples for explosive compounds (to verify analytical procedures of field laboratory).
- Samples collected from test items for smokeless powder.
- Samples collected from test items for ammonium picrate.
- Sample of gear oil from motor for explosives.

Analytical data summaries from the onsite laboratory provide the following information:

- Test Name (Pre-Test 2).
- Sample Matrix (wipe, rinsate, solid).
- Lab Identification Number.
- Sample Description.
- Dilution Factor.
- Sample Volume.
- Units of Reported Contamination.
- Reported Level of Contaminant.

Sample results for wipe samples are reported as total microgram (ug); rinsate samples are reported as microgram per milliliter (ug/mL); solid samples are reported as microgram per gram (ug/g). If the analysis indicated that the compound was present below the method detection limit, the detection limit is provided and is preceded with a less than sign (<).

The detection limits vary based on the sample type (wipe, rinsate or solid) and the dilution factor. For TNT, the following detection limits generally apply:

- Wipe samples - 19.2 mg.
- Rinsate samples - 0.96 mg/mL (concentrations corrected to 1,000 mL sample).
- Solid samples - 1.92 ug/g.

These detection limits are consistent with the limits outlined in the Test Plan (Section 5).

For the remaining analytes, however, some of the detection limits varied, due to high concentrations of TNT and required dilutions. The following example is provided for tetryl:

- The detection limit for tetryl in a rinsate sample was 2.5 ug/mL.
- Due to high concentrations of TNT in the rinsate sample, the sample is diluted by a factor of 1,000 to quantify the concentration of TNT.
- The detection limit of tetryl inadvertently increased to 2,500 ug/mL (2.5 ug/mL x 1,000 mL).

The mass or concentration of some contaminants is reported as a "J Value" (i.e., 3.36J). This indicates that the compound was determined to be present but below the detection level. The mass of contaminant is estimated.

The offsite laboratory data summaries include:

- Inorganic narrative (explosives narrative presented, where applicable).
- Glossary of terms.
- Inorganics data summary report.
- Inorganics quality assurance/quality control (QA/QC) report.

The inorganic narrative is generally a summary of the quality control results and a description of any problems encountered during the analysis of the samples. The glossary of terms defines the data qualifiers used in the report, abbreviations, and a laboratory chronology and holdtime report.

The inorganics data summary presents the actual results of the analysis. In addition, the lab sample number, site ID, analyte tested, result in appropriate units, and the reporting limit are provided.

The inorganics QA/QC report includes the analysis of a method blank, inorganics accuracy report, and an inorganics duplicate spike report.

---

July 1930  
Revision: Final

TEST RUN 2  
400°F/24 HOURS

1311R2

1

WESTON Analytica Use Only
8907HW006

# Custody Transfer Record/Lab Work Request



Client USATHAMIA/HUAAAP  
 Work Order 2231-08-02  
 Date Rec'd. 08/02/22  
 RFW Contact Nancy Johnson  
 Client Contact Phone 72

Weston Analytica Use Only		Client ID/Description		Analyses Requested		Matrix		Data Collected		Retention		Reanalysis		Resolved by		Date		Time	
001	Wash	01	Flush IL	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
002	Wash	02	Flush IL	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
003	Wash	03	Pre-wipe B1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
004	Wash	04	" B2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
005	Wash	05	" B3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
006	Wash	06	" B4	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
007	Wash	07	" B5	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
008	Wash	08	SR1 deion Pre-wipe	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
009	Wash	09	SR3 Pre-wipe B1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
010	Wash	10	" B2	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
011	Wash	11	" B3	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
012	Wash	12	" B4	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
013	Wash	13	" B5	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
014	Wash	14	SR2 deion Pre-wipe	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	
015	Wash	15	Moisture Pre-wipe	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	

Matrix: W - Wash, D - Deion, S - Solid, L - Liquid, A - Air, F - Flush, X - Other  
 Specific Instructions: Combine PATIENTS FROM SR1 Pre-wipe 11/13/15  
 27/42 g/L of 200 analyzed as SR1. Combined PATIENTS FROM SR2  
 27/42 g/L of 200 analyzed as SR2. Combined PATIENTS FROM SR2  
 27/42 g/L of 200 analyzed as SR2.



# Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only

8901HW007

Client USATHAMA/HIVAAP

Work Order 2201-03-02

Date Rec'd. 2201-03-02

Ref W Contact Nancy Johnson

Client Contact/Phone 12

Client ID/Description

001 SR1 drum APP1

002 SR2 drum APP1

Matrix: W - Water DS - Drum Solids Special Instructions:

S - Soil O - Oil CL - Drum Liquids

SE - Sediment A - Air F - Fish

SO - Solid X - Other

WESTON Analytica Use Only	
Samples Were:	
1 Shipped or Hand-Delivered	
NOTES:	
2 Ambient or Chilled	
NOTES:	
3 Received Broken/Leaking (Improperly Sealed)	
Y N	
NOTES:	
4 Properly Preserved	
Y N	
NOTES:	
5 Received Within Holding Times	
Y N	
NOTES:	
COC Tape Was:	
1 Present on Outer Package	
Y N	
2 Unbroken on Outer Package	
Y N	
3 Present on Sample	
Y N	
4 Unbroken on Sample	
Y N	
NOTES:	
COC Record Was:	
1 Present Upon Receipt of Samples	
Y N	
Discrepancies Between Sample Labels and COC Record?	
Y N	
NOTES:	

RFW 21-21-001/A-5/56

7-115

## DATA SUMMARY

Units ANALYST - WJL DATE - 10-10-68  
Analyst Sam Jones  
Reviewed \_\_\_\_\_

**NOTE: Data is corrected for dilution, :**

Comment: T2 PLE Test

[illegible]

3907HW014

Client USADIANA/NAHIAWork Order 2281-08-02Date Rec'd. 2/28/2008RFW Contact MAZELON, Peter S. N. BlainClient Contact/Phone 215-430-3117

NA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	ANALYSES REQUESTED	Refrigerator #	SI Type Container	Containers/Volume	Preservative
014-001	T2-SHR RI	AR	7/28	X				
002	2	↓	↓	X				
003	3	↓	↓	X				
004	4	↓	↓	X				
014-021	T2-SHR1 NIPPLE WIPE	WIPE	7/28	X				

Matrix: W - Water DS - Drum Solids  
 S - Soil O - Oil DL - Drum Liquids  
 SE - Sediment A - Air F - Fish  
 SO - Solid X - Other

Special Instructions:

T-2 TEST SAMPLES

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

RIFW 21-21-001/A-5/88

## Custody Transfer Record/Lab Work Request

WESTON

7-115



## Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only
99074W0014

Client WESTON/1411AAR  
 Work Order 22-B1-03-02  
 Date Rec'd. MAZE/04/11/17  
 RFW Contact MAZE/04/11/17  
 Client Contact/Phone 215-430-3117

Lab ID	Client ID/Description	Matrix	Date Collected	ANALYSES REQUESTED
014-005	T2 SHV RINSE 1	AB	7/28	X
006	2	↓	↓	X
007	3	↓	↓	X
008	4	↓	↓	X
009	FLASH CHMD WALL W1	WIPE	7/28	X
010	STEEL PIPE W1 T2	WIPE	7/28	X
011	T2 SM W1	WIPE	7/28	X
012	T2 SSR 1 W1 TOP	WIPE	7/28	X
013	2	↓	↓	X
014	3	↓	↓	X
015	4	↓	↓	X

Matrix: W - Water DS - Drum Solids  
S - Soil O - Oil DL - Drum Liquids  
SE - Sediment A - Air F - Fish  
SO - Solid X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

RFW 21-21-0011A-5/88

7-115

WESTON Analytica Use Only
Samples Were: 1 Shipped or Hand-Delivered NOTES:
2 Ambient or Chilled NOTES:
3 Received Broken/Leaking (Improperly Sealed) Y N NOTES:
4 Properly Preserved Y N NOTES:
5 Received Within Holding Times Y N NOTES:
COC Type Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:
COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:

EX - EXPLOSIVES  
 POST T-2 SAMPLES

# Custody Transfer Record/Lab Work Request



WESTON Analytics Use Only	
9207W0014	1015

Client USATH/MA/HRW/AP

Work Order 22-81-08-02

Date Rec'd. \_\_\_\_\_ Date Due \_\_\_\_\_

HRW Contact MAZEL/CO/MIC/N. JACSON

Client Contact/Phone 215-430-3117

MA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	ANALYSES REQUESTED	Preservative	Type Container	Vol	Temp	Relinquished by	Received by	Date	Time
014-016	T2 5521 W151 Bottom	W151	7/28	X								
-017	2	↓		X								
-018	3	↓		X								
-019	4	↓		X								
-020	T2-CP S1	Solid	7/28									
015-01	T2 PB1 K1											
002	2											
003	3											
004	4											
-005	T2 WIPE BLANK	W151										
006	T2 Beaker Rinse	AQ										

Special Instructions: EXP-EXPLOSIVES

T-2 POST TEST SAMPLES

Matrix:  
 W - Water DS - Drum Solids  
 S - Soil G - Oil DL - Drum Liquids  
 SE - Sediment A - Air F - Fish  
 SO - Solid X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

<b>WESTON Analytics Use Only</b> Samples Were: 1 Shipped or Hand-Delivered NOTES: 2 Ambient or Chilled NOTES: 3 Received Broken/Leaking (Improperly Sealed) Y N NOTES: 4 Properly Preserved Y N NOTES: 5 Received Within Holding Times Y N NOTES:	<b>COC Tape Was:</b> 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:	<b>COC Record Was:</b> 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:
---	--	---

## DATA SUMMARY

RFN Batch 290702141015  
Installation NAME: HCN  
Matrix: RINATE WIFE & SON

Analytical Lot  
Date Prepared  
Date Analyzed

Units &  
Analyst  
Reviewed

**Note: Data is corrected for dilution.**

**Comment: TA POST TEST**

[illegible]

I - present below detection limit.

# WESTON ANALYTICS EXPLOSIVES DATA SUMMARY

RFM Batch 9901W2010105  
 Installation KAMMINGS  
 Matrix: GUNITE WIFE 5 SEW  
 Analytical Lot \_\_\_\_\_  
 Date Prepared \_\_\_\_\_  
 Date Analyzed 7/25/89  
 Units GUNITE-WIFE 5 SEW - 1000000  
 Analyst SPW  
 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution,

Comments: 12 PMSI TEST

LAB ID #	W												B
	014-	014-	014-	014-	014-	014-	014-	014-	014-	014-	014-	014-	
	017	013	014	014	015	016	017	018	019	020	021	022	
SAMPLE DESCRIPTION	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	12 SRI TOP WIFE 5 SEW	
Dilution	1	1	1	1	1	1	1	1	1	1	1	1	1
SAMPLE VOLUME	-	-	-	-	-	-	-	-	-	-	-	-	1000
HMX	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<0.635
RDX	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<9.80	<9.80	<9.80	<9.80	<9.80	<9.80	<9.80	<9.80	<9.80	<9.80	<9.80	<9.80	<0.490
1,3,5-TNB	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<1.05
1,3-DNB	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<0.295
NB	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	13.3	8.4	17.8	15.1	9.43	20.1	17.9	15.9	15.9	15.9	15.9	15.9	<0.210
Tetryl	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0
2,4,6-TNT	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<19.2	<19.2	<19.2	<19.2	<19.2	<19.2	<19.2	<19.2	<19.2	<19.2	<19.2	<19.2	<0.960
2,6-DNT	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<4.00	<0.200
2,4-DNT	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20	<0.210

calac 0000  
 1126 7126 7126 7126 7126 7126 7126 7126 7126 7126 7126 7126 7126

RFW Batch 6807H0001015  
Installation 6807H0001015  
Matrix: 6807H0001015  
Analytical Lot  
Date Prepared  
Date Analyzed 7/12/08

Comment: T3 POST TEST

[illegible]

DATE	DESCRIPTION	AMOUNT
1957		

**WESTON**

ROY P. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16,19,27, 8-1,5,10,16,20,22,29, 9-2,11,20

RFW #: 8907L058,059,154 8908L203,258,315,398,462,524,534,595

8909L595,679,804

W.O. #: 2281-08-C2

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

7/24/90  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- NICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\* CO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L20

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	POST TS-FLSK CHMB WA	NITRATED ESTERS	5.0 u	UG	5
-002	POST T2-SHIP MINE	NITRATED ESTERS	5.0 u	UG	5
-003	PRE T5-SHIP MINE	NITRATED ESTERS	5.0 u	UG	5
-005	PRE T5-BLANK WIPE	NITRATED ESTERS	5.0 u	UG	5



ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
 WCRK ORDER: 2381-08-02-0000

WESTON BATCH #: 8908L203

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-----	-----	-----	-----	-----	-----
BLANK10	89LNC008-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC008-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
WORK ORDER: 2281-08-02-C000

WESTON BATCH #: 8908L21

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%REC
BLANK10	89LNC008-MB1	NITRATED ESTERS	10.8	2.5 u	10.0	108
BLANK20	89LNC008-MB2	NITRATED ESTERS	49.6	2.5 u	50.0	99
		NITRATED ESTERS	49.5	2.5 u	50.0	99

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L203

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC008-MB2	NITRATED ESTERS	99.3	99.0	0.20

July 1990  
Revision: Final

**TEST RUN 3**  
**500°F/36 HOURS**

**1311R2**

# Custody Transfer Reco.d/Lab Work Request

WESTON Analytische Use Only  
8907HW00Z

USATIAMA

2291-08-02

68/11/1

NEW Contract. David Johnson

**Client Contact Phone:**

WA Use Only	Client ID/Description
Lab ID	
001	T3 SR1 Pre-wire #1
002	T3 SR1 Pre-wire #2
003	T3 SR1 Pre-wire #3
004	T3 SR1 Pre-wire #4
005	T3 SR1 Pre-wire #5
006	T3 SR1 down pre-wire
007	T3 SR2 Pre-wire #1
008	T3 SR2 Pre-wire #2
009	T3 SR2 Pre-wire #3
010	T3 SR2 Pre-wire #4
011	T3 SR2 Pre-wire #5
012	T3 SR3 down pre-wire
013	T3 PB1 Flush
014	T3 PB2 Flush

015-05-27/15/99

Media:	W - Water	DG - Drum S: M60	Special instructions:
Media:			

DL - Drum Liquids

20. **Food**  
 21. **Other**  
 22. **Other**  
 23. **Other**  
 24. **Other**  
 25. **Other**  
 26. **Other**  
 27. **Other**  
 28. **Other**  
 29. **Other**  
 30. **Other**  
 31. **Other**  
 32. **Other**  
 33. **Other**  
 34. **Other**  
 35. **Other**  
 36. **Other**  
 37. **Other**  
 38. **Other**  
 39. **Other**  
 40. **Other**  
 41. **Other**  
 42. **Other**  
 43. **Other**  
 44. **Other**  
 45. **Other**  
 46. **Other**  
 47. **Other**  
 48. **Other**  
 49. **Other**  
 50. **Other**  
 51. **Other**  
 52. **Other**  
 53. **Other**  
 54. **Other**  
 55. **Other**  
 56. **Other**  
 57. **Other**  
 58. **Other**  
 59. **Other**  
 60. **Other**  
 61. **Other**  
 62. **Other**  
 63. **Other**  
 64. **Other**  
 65. **Other**  
 66. **Other**  
 67. **Other**  
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 83. **Other**  
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 85. **Other**  
 86. **Other**  
 87. **Other**  
 88. **Other**  
 89. **Other**  
 90. **Other**  
 91. **Other**  
 92. **Other**  
 93. **Other**  
 94. **Other**  
 95. **Other**  
 96. **Other**  
 97. **Other**  
 98. **Other**  
 99. **Other**  
 100. **Other**

1000

[illegible]

**RFW 21-21-001/A-5/88**

72

WESTON Analytcs Use Only

8907 HW 002

# Custody Transfer Record/Lab Work Request



Client USAID/ANAN  
 Work Order 7731-03-01  
 Date Rec'd 7/14/03 Date Due  
 RFW Contact Navy  
 Client Contact/Phone

Refill/Replenish	ANALYSES REQUESTED	Matrix	Date Collected	Client ID/Description	Matrix	Date	Time	Received by	Date	Time
1 Type Container				015 T3 SR1 down area	110	7/14/03				
Container Volume				016 T3 SR2 down area	110					
Preservative				017 T3 SR1 Flush B1						
				018 T3 SR2 Flush B1						
				019 T3 SR1 Flush #2						
				020 T3 SR2 Flush #2						
				021 T3 SR2 Flush #3						
				022 T3 SR1 Flush						
				023 T3 SR2 Flush						
				024 T3 CP PI-200g's	SOL					
				025 T3 SM PI-200g's	100g					

Pag 2 OF 2

Matrix: W - Water DS - Drum Solids Special Instructions:  
 S - Soil O - Oil DL - Drum Liquids  
 SE - Sediment A - Air F - Fish  
 SO - Solid X - Other

Item/Reason	Refill/Replenish by	Received by	Date	Time	Item/Reason	Refill/Replenish by	Received by	Date	Time

# Custody Transfer Record/Lab Work Request

WESTON Analytix Use Only  
8907HW004

Usarilama Hwarp

7231-08-02

Date	Rec'd	7116	7116	7116

NRW Contact Nancy Johnson

## Client Contacts/Phone:

[illegible]

**Materials:** W - Water DS - Drum Solids  
O - Oil OL - Drum Liquids  
S - Soil P - Pile  
SS - Sediment A - Air  
SO - Soil X - Other

[illegible]

<b>WESTON Analytics</b>	<b>COC Tape Was:</b> 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N <b>NOTES:</b>
<b>Samples Were:</b> 1 Shipped or Hand-Delivered <b>NOTES:</b> 2 Ambient or Chilled <b>NOTES:</b> 3 Received Broken/ Leaking (Improperly Sealed) Y N <b>NOTES:</b> 4 Properly Preserved Y N <b>NOTES:</b> 5 Received Within Holding Time Y N <b>NOTES:</b>	<b>COC Record Was:</b> 1 Present Upon Receipt of Samples Y N  Discrepancies Between Sample Labels and COC Record? Y N <b>NOTES:</b>





# WELTON ANALYTICS EXPLOSIVES DATA SUMMARY

RPM Batch 9907H0002/0002000200 Analytical Lot  
 Installation HAWTHORNE 00 Date Prepared  
 Matrix: KANSAS WIPES A SOIL Date Analyzed 11/16/2004

Units KANSAS-WIPES-A SOIL  
 Analyst gms lbs  
 Reviewed

Note: Data is corrected for dilution.

Comment: Test 3 - PRE TEST

LAB ID #	002-001	002-002	002-003	002-004	002-005	002-006	002-007
SAMPLE DESCRIPTION	T3 SR1 PRE #1	T3 SR1 PRE #2	T3 SR1 PRE #3	T3 SR1 PRE #4	T3 SR1 PRE #5	T3 SR1 PRE #6	T3 SR1 PRE #7
Dilution	1	10	1	10	1	10	1
SAMPLE VOLUME	—	—	—	—	—	—	—
UNITS	total ug	total ug	total ug	total ug	total ug	total ug	total ug
HMX	644	450	269	1181	266	214	513
RDX	658	720	493	311	585	751	1251
1,3,5-TNB	209	209	209	209	209	209	209
1,3-DNB	590	590	590	590	590	590	590
NB	560	510	430	430	430	430	720
Tetryl	500	500	500	500	500	500	500
2,4,6-TNT	192	192	244	192	491	192	192
2,6-DNT	400	400	400	400	400	400	400
2,4-DNT	420	420	420	420	420	420	420
QUALC DATE (year)	7/7	7/7	7/7	7/7	7/7	7/7	7/7

← POSSIBLE CONTAMINATE



# WESTON ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFW Batch 90740002000000000000 Analytical Lot \_\_\_\_\_ Units Run/Kit - 1000 - 1000  
 Installation HAWTHORNE Date Prepared \_\_\_\_\_ Analyst QAC/LOS  
 Matrix: RUNTIME WIFE 5 SOL Date Analyzed 11/17/2021 24/109 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution,

Comment: TEST 3 - PRE TEST

LAB ID #	002-017	002-018	002-019	002-020	002-021	002-022	002-023	002-024	002-025	004-001
SAMPLE DESCRIPTION	FLUSH #1	FLUSH #1	FLUSH #1	FLUSH #2	FLUSH #2	FLUSH #2	FLUSH #3	FLUSH #3	PRE-SOIL	PRE-TEST
Dilution	10	1	10	1	1	1	1	10,000	1	1
SAMPLE VOLUME	1000	1000	1000	1000	1000	1000	300	300	300	---
UNITZ	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L
HMX	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635
RDX	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490
1,3,5-TNB	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05
1,3-DNB	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295
NB	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210
Tetryl	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50
2,4,6-TNT	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960
2,6-DNT	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200
2,4-DNT	<41.5	<23.5	<16.8	<9.1	<7.7	<6.6	<5.5	<4.4	<3.3	<2.2
QAC DATE (1000)	11/17	11/17	11/17	11/17	11/17	11/17	11/17	11/17	11/17	11/17

\* POSSIBLE CONTAMINATE







# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only

8907HW010

Client 11 SATHAMA / HUAP

Work Order 2281-08-02

Date Rec'd. \_\_\_\_\_

RFW Contact Mike Martinez / Nancy Johnson

Client Contact/Phone \_\_\_\_\_

WESTON Analytics Use Only

Samples Were:  
1 Shipped or Hand-Delivered  
NOTES:

2 Ambient or Chilled  
NOTES:

3 Received Broken / Leaking (Improperly Sealed)  
Y N  
NOTES:

4 Property Preserved  
Y N  
NOTES:

5 Received Within Holding Times  
Y N  
NOTES:

COC Tape Was:  
1 Present on Outer Package Y N  
2 Unbroken on Outer Package Y N  
3 Present on Sample Y N  
4 Unbroken on Sample Y N  
NOTES:

COC Record Was:  
1 Present Upon Receipt of Sample Y N  
Discrepancies Between Sample Labels and COC Record? Y N  
NOTES:

Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerators		Type Container		Containers/Volumes		Preservative		ANALYSES REQUESTED	Date
				1	2	3	4	5	6	7	8		
001	T3 SHV1 R1	AG	7/21/09										
002	T3 SHV1 R2												
003	T3 SHV1 R3												
004	T3 SHV1 R4												
005	T3 CP S1	S	7/21/09										
006	T3 SM W1	W											
007	T3 SR1 W1	W											
008	T3 SR1 W2												
009	T3 SR1 W3												
010	T3 SR1 W4												
011	T3 SR1 W5												
012	T3 SR1 W6												
013	T3 SR1 W7												
014	T3 SR1 W8	Y	7/21/09										

T-3 POST TEST SAMPLING

Matrix: W - Water DS - Drum Solids DL - Drum Liquids  
S - Soil O - Oil A - Air P - Fish  
SE - Sediment X - Other

Special Instructions:

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time



# WESTON ANALYTICS EXPLOSIVES DATA SUMMARY

RFW Batch: 00000000000000000000  
 Installation: WASHINGTON  
 Matrix: 10000000000000000000

Analytical Lot: 00000000000000000000  
 Date Prepared: 00000000000000000000  
 Date Analyzed: 00000000000000000000

Units: 00000000000000000000  
 Analyst: 00000000000000000000  
 Reviewed: 00000000000000000000

Note: Data is corrected for dilution.

Comment: TEST 3 POST TEST

LAB ID	010-	003	010-	004	010-	005	006	010-	007	010-	008	010-	009	010-	010-	010-
SAMPLE DESCRIPTION	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1	TS SHV1
Dilution	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
SAMPLE VOLUME	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000	1000
Wtts																
HMX	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035	0.035
RDX	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040	0.040
1,3,5-TMB	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105	0.105
1,3-DNB	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095	0.095
NB	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010
Tetryl	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250	0.250
2,4,6-TNT	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010	0.010
2,6-DNT	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020
2,4-DNT	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020	0.020

DATE: 0000-0000-0000

RESPONSIBLE: 00000000000000000000







## DATA SUMMARY

Units mg/L  
Analyst QJA  
Reviewed

**Note: Data is corrected for dilution,**

Comment: T3 Post Test

[illegible]

7/2/20

[illegible]



ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA HAWTHORNE

SAMPLES RECEIVED: 07-19-89

RFW #: 8907L058

W.O.#: 2281-08-07

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of wipe samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.

SSD = Designates sample spiked with target compound.

D = Indicates duplicate analysis of a sample.

NS = Not spiked.

DL = Diluted below calibration range.

G = Indicates elevated detection limit due to sample interference.

NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

NOTE: Method holding time of seven days was exceeded for sample preparation. This holding time is applicable to soil samples. Although this holding time is exceeded, lab experience with the long term stability of explosives compounds provides an indication that the data obtained is quite likely to be representative of initial explosive concentrations.

WESTON

Data Qualifiers

< = Less than  
> = Greater than

Analysis Summary:

Samples Collected: 07-14-89  
Samples Prepared: 07-25-89  
Samples Analyzed: 08-10-89

Approved By: \_\_\_\_\_

*for* George Perry  
HPLC Unit Leader  
Lionville Analytical Laboratory

# WESTON ANALYTICS WIPE EXPLOSIVES DATA

RFW Batch Number: 8907L058 CLIENT: USATHAMA-HAWTHORNE

Sample Information	Client		---		---	
	ID :	T3 SM	REWIPE 3	2XSS	10XSS	Total ug
	RFW#:	002		1		
	D.F.:	1				
	Units:	Total ug		Total ug		Total ug
HMX.....	< 12.7			2.36(92.9%)		11.8(92.9%)
RDX.....	< 9.80			1.75(89.2%)		8.95(91.3%)
1,3,5-TNB.....	< 30.9			3.84(91.8%)		18.8(90.0%)
1,3-DNB.....	< 5.90			1.15(97.4%)		5.66(95.9%)
NITROBENZENE.....	< 4.20			0.73(86.9%)		3.55(84.5%)
TETRYL.....	< 50.0			11.3(113%)		62.5(125%)
2,4,6-TNT.....	< 19.2			3.56(92.7%)		18.2(94.8%)
2,6-DNT.....	< 4.00			0.75(93.8%)		3.66(91.5%)
2,4-DNT.....	< 4.20			0.75(89.3%)		3.64(86.7%)

Sample Information	Client		---		---	
	ID :	10XSSD				
	RFW#:					
	D.F.:	1				
	Units:	Total ug				
HMX.....	12.2(96.0%)					
RDX.....	9.24(94.2%)					
1,3,5-TNB.....	19.4(92.8%)					
1,3-DNB.....	5.83(98.8%)					
NITROBENZENE.....	3.59(85.4%)					
TETRYL.....	66.9(134%)					
2,4,6-TNT.....	19.0(99.0%)					
2,6-DNT.....	3.64(91.0%)					
2,4-DNT.....	3.68(87.6%)					

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP  
SAMPLES RECEIVED: 7-16,19,27, 8-1,3,10,16,20,22,29, 9-2,11,20  
RFW #: 8907L058,059,154 8908L203,258,315,398,462,524,534,595  
8909L595,679,804  
W.O. #: 2281-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

2/24/90  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicates.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spikes.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for epton silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.



ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L058

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
001	T3 SM PREWIPE #2	NITRATED ESTERS	10.0 u	UG	10.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L05

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTI LIMIT
-----	-----	-----	-----	-----	-----
BLANK10	89LNC006-MB1	NITRATED ESTERS	5.0	u MG/L	5
BLANK20	89LNC006-MB2	NITRATED ESTERS	5.0	u MG/L	5

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-02-0000

WESTON BATCH #: 8907L058

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC006-MB1	NITRATED ESTERS	9.0	5.0 u	10.0	90.0
BLANK20	89LNC006-MB2	NITRATED ESTERS	46.7	5.0 u	50.0	93.3
		NITRATED ESTERS	48.9	5.0 u	50.0	97.7

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L05

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC006-MB2	NITRATED ESTERS	93.3	97.7	4.6

ROY F. WESTON INC.  
INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L059

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T3 CHAMP WELL PW SP	NITRATED ESTERS	10.0	u UG	10.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L055

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTIN LIMIT
BLANK10	89LNC006-MB1	NITRATED ESTERS	5.0 u	MG/L	5.
BLANK20	89LNC006-MB2	NITRATED ESTERS	5.0 u	MG/L	5.

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L059

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC006-MB1	NITRATED ESTERS	9.0	5.0 u	10.0	90.0
BLANK20	89LNC006-MB2	NITRATED ESTERS	46.7	5.0 u	50.0	93.3
		NITRATED ESTERS	48.9	5.0 u	50.0	97.7

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L05

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC006-MB2	NITRATED ESTERS	93.3	97.7	4.6



ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L154

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T3SMWC	NITRATED ESTERS	5.0	u UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L15

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC008-MB1	NITRATED ESTERS	2.5 u	MG/L	2.
BLANK20	89LNC008-MB2	NITRATED ESTERS	2.5 u	MG/L	2.

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8907L154

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC008-MB1	NITRATED ESTERS	10.8	2.5 u	10.0	108
BLANK20	89LNC008-MB2	NITRATED ESTERS	49.6	2.5 u	50.0	99.3
		NITRATED ESTERS	49.5	2.5 u	50.0	99.0

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-J2-0000

WESTON BATCH #: 8907L1!

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC008-MB2	NITRATED ESTERS	99.3	99.0	0.20

TEST RUN 3  
500°F/24 HOURS

1311R2

# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only	3907H2016
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Client's Signature

**Work Order** 22221-03-02

Date Rec'd. \_\_\_\_\_ Date Due \_\_\_\_\_

**AFW Contact:**

**Client Contact/Phone**

[illegible]

Matrix:	W - Water	DS - Drum Solids	Special Instructions:

2 - Soil  
SE - Sediment  
SU - Solid  
G - Oil  
A - Air  
DL - Drilling Liquids  
F - Fish  
O - Other

[illegible]

<b>WESTON Analytics</b>	
<b>Use Only</b>	
<b>Samples Were:</b> <b>1 Shipped or Hand-Delivered</b> <b>NOTES:</b>	
<b>2 Ambient or Chilled</b>	
<b>NOTES:</b>	
<b>3 Received Broken/Leaking (Improperly Sealed)</b>	<b>Y      N</b>
<b>NOTES:</b>	
<b>4 Properly Preserved</b>	<b>Y      N</b>
<b>NOTES:</b>	
<b>5 Received Within Holding Times</b>	<b>Y      N</b>
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
<b>1 Present on Outer Package</b>	<b>Y      N</b>
<b>2 Unbroken on Outer Package</b>	<b>Y      N</b>
<b>3 Present on Sample</b>	<b>Y      N</b>
<b>4 Unbroken on Sample</b>	<b>Y      N</b>
<b>NOTES:</b>	
<b>COC Record Was:</b>	
<b>1 Present Upon Receipt of Samples</b>	<b>Y      N</b>
<b>Discrepancies Between Sample Labels and COC Record?</b>	
<b>Y      N</b>	
<b>NOTES:</b>	

## DATA SUMMARY

Units Went on duty successfully  
Analyst Spence  
Reviewed \_\_\_\_\_

Post

Comment: T-5, B2-5 TEST

MATERIAL	Q16-	Q16-	Q16-	Q16-
LAB ID #	Q16- SHIP	Q16- PIPE	Q16- PIPE	Q16- PIPE
SAMPLE DESCRIPTION	SHIP	PIPE	PIPE	PIPE
Dilution	1	10	10,000	
UNIT#	439	439	439	439
HMX	439	439	439	439
RDX	439	439	439	439
1,3,5-TNB	439	439	439	439
1,3-DNB	439	439	439	439
NB	439	439	439	439
Tetryl	439	439	439	439
2,4,6-TNT	439	439	439	439
2,6-DNT	439	439	439	439
2,4-DI.T	439	439	439	439

1517  
1518

7253 7131

## DATA BULKARY

Units LUNDA-104-2 1-28-72  
Analyst SPC  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution.**

Comment: TS PRE TEST

[illegible]





28



# Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only

2900HW-01B

Client USATAMA / HWAP

Work Order 2201-08-02

Date Rec'd. MM/YY/YY

RFW Contact M. MATELON, N. JOHANSEN

Client Contact/Phone 215-430-3117

WESTON Analytica Use Only

Samples Were:  
1 Shipped or Hand-Delivered  
NOTES:

2 Ambient or Chilled  
NOTES:

3 Received Broken/Leaking (Improperly Sealed)  
Y N  
NOTES:

4 Properly Preserved  
Y N  
NOTES:

5 Received Within Holding Times  
Y N  
NOTES:

COC Tape Was:  
1 Present on Outer Package Y N  
2 Unbroken on Outer Package Y N  
3 Present on Sample Y N  
4 Unbroken on Sample Y N  
NOTES:

COC Record Was:  
1 Present Upon Receipt of Samples Y N  
Discrepancies Between Sample Labels and COC Record? Y N  
NOTES:

WA Use Only Lab ID	Client ID/Description	Refrigerators		ANALYSES REQUESTED	Matrix	Date Collected										
		Any Type Contain in	Containers/Volumes													
005	T-5 SSR 2 W/ TOPARK	Via		EXP		8/2										
006	2															
007	3															
008	4															
009	T-5 SSR 2 1/5 LUGRARK					8/2/19										
010	6															
011	7															
012	8															

Special Instructions: T-5 TEST SAMPLES

Matrix:  
W - Water DS - Drum Solids  
B - Soil O - Oil DL - Drum Liquids  
SE - Sediment A - Air F - Fish  
SO - Solids X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time



# Custody Transfer Record/Lab Work Request



WESTON Analytics Use Only	220811020
---------------------------	-----------

Client: US Army / HwAAP

Work Order 2281-031-02

Date Rec'd. 11/24/11 Date Due 12/1/11

RFW Contact WONG / N. JONES  
25405 / 25  
1713-3056 / 3117

Client Contact/Phone 45 1:30--311 F

[illegible]

Refrigerators	ANALYSES REQUESTED	Date Collected	
a/Type Container		8/4	X
Containers/Volume			
Preservative			

<b>WESTON Analytcs</b>	
<b>Use Only:</b>	
<b>Samples Were:</b>	
1 Shipped or Hand-Delivered	
<b>NOTES:</b>	
<b>2 Ambient or Cooled</b>	
<b>NOTES:</b>	
<b>3 Received Broken/Leaking (Improperly Sealed)</b>	
Y	N
<b>NOTES:</b>	
<b>4 Properly Preserved</b>	
Y	N
<b>NOTES:</b>	
<b>5 Received Within Holding Times</b>	
Y	N
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
<b>NOTES:</b>	
<b>COC Record Was:</b>	
1 Present Upon Receipt of Samples	Y N
Discrepancies Between Sample Labels and COC Record?	
Y	N
<b>NOTES:</b>	

WATER	WATER	DRUM SOLIDS	SPECIAL INSTRUCTIONS:
W - Water	W - Water	DS - Drum Solids	

**3 - 3ult**      **0 - 0lt**      **DL - Drum Liquids**

**SE - Sediment A - Air F - Fish**

PH-8-08

[illegible]

## DATA SUMMARY

## Analytical Lot

Date Prepared

Date Analyzed \_\_\_\_\_

Units Earned - 10

**Analyst** **Qaim**

Reviewed

**Note: Data is corrected for dilution, %**

**Comment:** T-5 POST TEST

[illegible]

## DATA SUMMARY

RFW Batch	SEQUENCING	Analytical Lot		Units	RECEIVED - ANALYST SUPERSEDED BY ANALYST
Installation	ANALYST-ONE	Date Prepared		Analyst	SCHWAB
Matrix:	PURIFIED WASTE & SOLID	Lots Analyzed		Reviewed	
					APPROVED

**Note: Data is corrected for dilution.**

**Comment:** T-5 PST TEST

[illegible]

## DATA SUMMARY

Units PC-A113 - 44-150  
Analyst QJM  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution.**

Comment: T's Post Test

MATRIX		R		R	
LAB ID #	018-	020-	018-	020-	
	023	001			
SAMPLE DESCRIPTION	018	020			
	023	001			
Dilution	1	1			
SAMPLE VOLUME (mL)	150	104,000			
UNITS	0.0035	0.0035			
HMX	0.0035	0.0035			
RDX	0.0035	0.0035			
1,3,5-TNB	0.0035	0.0035			
1,3-DNB	0.0035	0.0035			
NE	0.0035	0.0035			
Tetryl	0.0035	0.0035			
2,4,6-TNT	0.0035	0.0035			
2,6-DNT	0.0035	0.0035			
2,4-DNT	0.0035	0.0035			

1016 - 1015 - 1014



ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA HAWTHORNE  
RFW #: 8908L203, OIL  
W.O.#: 2281-08-07

SAMPLES RECEIVED: 08-01-89

#### EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of oil samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

#### Abbreviation

#### Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

MS = Designates sample spiked with target compound.

MSD = Designates sample spiked with target compound in duplicate.

D = Indicates duplicate analysis of a sample.

NS = Not spiked.

DL = Diluted below calibration range.

G = Indicates elevated detection limit due to sample interference.

NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

#### Data Qualifiers

< = Less than  
> = Greater than

#### Analysis Summary:

Samples Collected: 07-28-89  
Samples Prepared: 08-04-89  
Samples Analyzed: 08-10-89

Approved By:

  
George Perry

HPLC Unit Leader  
Lionville Analytical Laboratory



WESTON ANALYTICS  
OIL EXPLOSIVES DATA

RFW Batch Number: 8208L2J3 CLIENT: USATHAMA-HAWTHORNE Page: 1

Sample Information	Client ID	PRE T5 GEAR OIL	PRE T5 GEAR OIL	PRE T5 GEAR OIL	PRF T-5 GEAR OIL	Blank
	RFW#:	004	004 MS	004 MS	004 MSD	1
	D.F.:	1	1	1	1	1
	Units:	ug/g	ug/g	ug/g	ug/g	ug/g
HMX.....	<	144	2610(98.4%)	2610(98.4%)	2610(98.4%)	<
RDX.....	<	2130G	3750(141%)	500G(NR)	500G(NR)	<
1,3,5-TNB.....	<	237	4180(95.7%)	4180(95.7%)	4180(95.7%)	<
1,3-DNB.....	<	66.8	1230(100%)	1230(100%)	1230(100%)	<
NITROBENZENE.....	<	47.6	729(83.0%)	729(83.0%)	729(83.0%)	<
TETRYL.....	<	566	15000(144%)	15000(144%)	15000(144%)	<
2,4,6-TNT.....	<	217	4180(104%)	4180(104%)	4180(104%)	<
2,6-DNT.....	<	45.3	800(95.8%)	800(95.8%)	800(95.8%)	<
2,4-DNT.....	<	47.6	840(96.0%)	840(96.0%)	840(96.0%)	<

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16,19,27, 8-1,5,10,16,20,22,29, 9-2,11,20

RFW #: 8907L058,059,154 8908L203,258,315,398,462,524,534,595  
8909L595,679,804

W.O. #: 2281-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.



Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

2/24/90  
Data

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L203

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	POST T5-FLSH CHMB WA	NITRATED ESTERS	5.0 u	UG	5.0
-002	POST T2-SHIP MINE	NITRATED ESTERS	5.0 u	UG	5.0
-003	PRE T5-SHIP MINE	NITRATED ESTERS	5.0 u	UG	5.0
-005	PRE T5-BLANK WIPE	NITRATED ESTERS	5.0 u	UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L201

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC008-MB1	NITRATED ESTERS	2.5 u	MG/L	2.
BLANK20	89LNC008-MB2	NITRATED ESTERS	2.5 u	MG/L	2.

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L20

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%REC
BLANK10	89LNC008-MB1	NITRATED ESTERS	10.8	2.5 u	10.0	108
BLANK20	89LNC008-MB2	NITRATED ESTERS	49.6	2.5 u	50.0	99
		NITRATED ESTERS	49.5	2.5 u	50.0	99

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HAWTHORNE  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L2

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC008-MB2	NITRATED ESTERS	99.3	99.0	0.20

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L258

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T5 FLASH CHMB WALL	NITRATED ESTERS	5.0	UG	5.0
-002	T5 SMW2 POST TEST	NITRATED ESTERS	5.6	UG	5.0
-003	T-8 SMW2 POST TEST	NITRATED ESTERS	13.0	UG	5.0
-004	T-8 WIPE BLANK PRE-	NITRATED ESTERS	5.8	UG	5.0



ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L25

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORT LIMIT
BLANK10	89LNC010-MB1	NITRATED ESTERS	2.5 u	MG/L	2
BLANK20	89LNC010-MB2	NITRATED ESTERS	2.5 u	MG/L	29

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L258

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC010-MB1	NITRATED ESTERS	9.9	2.5 u	10.0	98.8
BLANK20	89LNC010-MB2	NITRATED ESTERS	52.9	2.5 u	50.0	106
		NITRATED ESTERS	51.8	2.5 u	50.0	104

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8008L2

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC010-MB2	NITRATED ESTERS	106	104	2.2

July 1990  
Revision: Final

TEST RUN 8  
400°F/36 HOURS

1311R2

WESTON ANALYTICS  
'8:

# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only
017

Client USAF/AMAL/HW/HP  
Work Order 2181-03-02  
Date Rec'd. 2/15/89  
RFW Contact MAZELAN, CDS/OPS, TCH/STON  
Client Contact/Phone 215-430-3117

WA Use Only Lab ID	Client ID/Description
001	TPB1 RINSE 1
002	2
003	3
004	4
005	TPB2 RINSE 1
006	2
007	3
008	4
009	TSSR1 WIRE 1
010	2
011	3
012	4

Mat/As: W - Water DS - Drum Solids  
S - Soil O - Oil DL - Drum Liquide  
SE - Sediment A - Air F - Fish  
SO - Solid X - Other

Special Instructions: EXP - EXPLOSIVES TR  
ALL SAMPLES ARE PRE-TEST SAMPLES

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

WESTON Analytics Use Only	
Samples Were: 1 Shipped or Hand-Delivered NOTES:	
2 Ambient or Chilled NOTES:	
3 Received Broken/ Leaking (Improperly Sealed) Y N NOTES:	
4 Properly Preserved Y N NOTES:	
5 Received Within Holding Times Y N NOTES:	
COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:	
COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:	

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WESTON

# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only

017

Client: USATHAMA HYVAAP

Work Order: 2201-08-02

Date Rec'd: \_\_\_\_\_

RFW Contact: MAHELOH, N. Tinsal, OASIA

Client Contact/Phone: 315-430-3117

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerated	Seal Type	Container/Volume	Preservative	ANALYSES REQUESTED
013	T SSR 1 WIPE 5 LUGA	WIPE	7/31/08	X	100%	100%		
014	6	↓	↓	X				
015	7	↓	↓	X				
016	8	↓	↓	X				
017	T SSR 2 WIPE 1 LUGA	WIPE	7/31/08	X				
018	2	↓	↓	X				
019	3	↓	↓	X				
020	4	↓	↓	X				
021	T SSR 2 WIPE 5 LUGA	WIPE	7/31/08	X				
022	6	↓	↓	X				
023	7	↓	↓	X				
024	8	↓	↓	X				

T8

EXP - EXPLOSIVES

SPECIAL INSTRUCTIONS:

Matrix: W - Water U3 - Drum Solids  
 S - Soil O - Oil UL - Drum Liquids  
 SE - Sediment A - Air P - Fish  
 SO - Solids X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

ALL SAMPLES ARE PRE-TEST SAMPLES

WESTON ANALYSES Use Only

Samples Were:

1 Shipped or Hand-Delivered

NOTES:

2 Ambient or Chilled

NOTES:

3 Received Broken/Leaking (Improperly Sealed)

Y N

NOTES:

4 Properly Preserved

Y N

NOTES:

5 Received Within Holding Time

Y N

NOTES:

COC Tape Was:

1 Present on Outer Package Y N

2 Unbroken on Outer Package Y N

3 Present on Sample Y N

4 Unbroken on Sample Y N

NOTES:

COC Record Was:

1 Present Upon Receipt of Samples Y N

Discrepancies Between Sample Labels and COC Record?

Y N

NOTES:



# Custody Transfer Record/Lab Work Request

WESTON Analyticals Use Only	
0908 MW - 019	
KATHINA / HUNTER	
Client	2281-08-02
Work Order	
Date Rec'd	MAZELON, N. / 215-432-3117
RFW Contact	
Client Contact/Phone	

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator #/Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED
001	T-B C P SOLID PRETEST	SOLID	8/3/89				
002	T-B S M LVL PRETEST	WIPR	8/3/89				
003	T-B S M WHITE BLANK PRETEST	WIPR	8/3/89				
004	T-B C P PIPED BLANK PRETEST	AQ	8/3/89				
005	T-B 0 STEEL PIPE WAX RINSAR	AQ	8/5/89				
006	T-3 SSRA SPIKE RINSAR	AQ	8/11/89				
007	T-3 SSRA SPIKE RINSAR	L	1				

Special Instructions: **ALL SAMPLES are PRE TEST T-B SAMPLES**

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

WESTON Analyticals Use Only	
Samples Were:	
1 Shipped or Hand-Delivered	NOTES:
2 Arrived or Called	NOTES:
3 Received Broken/Leaking (improperly Sealed)	Y N
NOTES:	
4 Property Preserved	Y N
NOTES:	
5 Received Within Holding Time	Y N
NOTES:	
COC Tape Was:	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
NOTES:	

COC Record Was:	
1 Present Upon Receipt of Samples	Y N
Discrepancies Between Sample Labels and COC Record?	
Y N	NOTES:

# WESTON ANALYTICS EXPLOSIVES DATA SUMMARY

RFW Batch 3307440007 1/2/19 Analytical Lot \_\_\_\_\_ Units Analyzed \_\_\_\_\_  
 Installation 1987000000 Date Prepared \_\_\_\_\_ Analyst \_\_\_\_\_  
 Matrix: 1987000000 Date Analyzed 1/2/19 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution, \*

Comment: T-S PRE TEST

LAB ID #	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
SAMPLE DESCRIPTION	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
Dilution	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1	1
SAMPLE VOLUME	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
UNITS	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
HMX	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
RDX	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
1,3,5-TNB	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
1,3-DNB	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
NB	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
Tetryl	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
2,4,6-TNT	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
2,6-DNT	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
2,4-DNT	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030
QUALOC DATE	101-1004	101-1005	101-1006	101-1007	101-1008	101-1009	101-1010	101-1011	101-1012	101-1013	101-1014	101-1015	101-1016	101-1017	101-1018	101-1019	101-1020	101-1021	101-1022	101-1023	101-1024	101-1025	101-1026	101-1027	101-1028	101-1029	101-1030



**DATA SUMMARY**

RFW Batch 980600000  
Installation 12-17-00  
Matrix: 00000000000000000000

Analytical Lot \_\_\_\_\_  
Date Prepared \_\_\_\_\_  
Date Analyzed \_\_\_\_\_

Units Generated \_\_\_\_\_  
Analyst Date \_\_\_\_\_  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution, :**

**Comment:** T-9 PRE TEST

[illegible]

# WESTON ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFW Batch 2008010101 Analytical Lot \_\_\_\_\_ Units \_\_\_\_\_  
 Installation \_\_\_\_\_ Date Prepared \_\_\_\_\_ Analyst \_\_\_\_\_  
 Matrix: RDX/NE/PE/TE/BA Date Analyzed \_\_\_\_\_ Reviewed \_\_\_\_\_

Note: Data is corrected for dilution.

Comment: 1-3 PRE TEST

LAB ID #	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09
Sample Description	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09	Q19- Q09
Dilution	1	1	10	1000	10000				
Sample Volume	90	90	90	90	90				
Units									
HMX	40.000	40.000	40.000	40.000	40.000				
RDX	40.000	40.000	40.000	40.000	40.000				
1,3,5-TNB	40.000	40.000	40.000	40.000	40.000				
1,3-DNB	40.000	40.000	40.000	40.000	40.000				
NB	40.000	40.000	40.000	40.000	40.000				
Tetryl	40.000	40.000	40.000	40.000	40.000				
2,4,6-TNT	40.000	40.000	40.000	40.000	40.000				
2,6-DNT	40.000	40.000	40.000	40.000	40.000				
2,4-DNT	40.000	40.000	40.000	40.000	40.000				

Calculated Data

WESTON Analyticals Use Only	
8908HW022	

# Custody Transfer Record/Lab Work Request

WESTON ANALYTICALS

Client USATHANAB/FINA AP

Work Order 2381-08-02

Date Rec'd. 8-8-81 Date Due

RFW Contact N. STEINSON

Client Contact Phone (215) 430-3117

WA Use Only Lab ID	Client ID/Description
012	T8-SR-R1
013	1 R2
014	B3
015	B4
016	T8-PB1-R1
017	R2
018	R3
019	R4
020	T8-SHR1-R1
021	R2
022	R3
023	R4
024	T8-CP - soil
025	T8-CP-scoop-Fuel/blank R1
026	T8-Field Blank-Baker Rinse

Method 027 W-Water 05-From Sample  
 0-Soil 0-From Sample  
 CE-Sediment A-Air P-Flth  
 SO-Solid X-Other

Identification	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	<u>N. I. Steinson</u>		<u>8-8-81</u>	<u>5:32 PM</u>					

T8 Post Test Samples

WESTON Analyticals Use Only	
Samples Were:	
1 Shipped or Hand-Delivered	Y
NOTES:	
2 Ambient or Chilled	
NOTES:	
3 Received Broken/Leaking (Improperly Sealed)	
Y	N
NOTES:	
4 Properly Preserved	
Y	N
NOTES:	
5 Received Within Holding Times	
Y	N
NOTES:	
COC Tape Was:	
1 Present on Outer Package	Y
2 Unbroken on Outer Package	Y
3 Present on Sample	Y
4 Unbroken on Sample	Y
NOTES:	
COC Record Was:	
1 Present Upon Receipt of Samples	Y
Discrepancies Between Sample Labels and COC Record?	Y
NOTES:	

# Custody Transfer Record/Lab Work Request



WESTON Analytics Use Only	8908H2023
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Client USAID/USAID/USAID

Work Order 22-271-08-02

Date Rec'd. 8/9/28 Date Due

AFW Contact Nancy Smith-John

Client Contact/Phone 1215-430-317

[illegible]

**Matrix:** W - Water D9 - Drum Solids  
S - Soil DL - Drum Liquids  
SE - Sediment F - Fish  
SO - Solid X - Other

**Special Instructions:**

[illegible]

<b>WESTON Analytica</b>	
<b>Use Only</b>	
<b>Samples Were:</b>	
1 Shipped or Hand-Delivered	
<b>NOTES:</b>	
2 Ambient or Chilled	
<b>NOTES:</b>	
3 Received Broken/Leaking (If Improperly Sealed)	Y N
<b>NOTES:</b>	
4 Properly Preserved	Y N
<b>NOTES:</b>	
5 Received Within Holding Times	Y N
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
<b>NOTES:</b>	
<b>COC Record Was:</b>	
1 Present Upon Receipt of Samples	Y N
Discrepancies Between Sample Labels and COC Record?	
<b>NOTES:</b>	Y N

# WESTON ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFW Batch 3902H00000 Analytical Lot \_\_\_\_\_ Units Quantified 50.00g  
 Installation HASTHORPE Date Prepared \_\_\_\_\_ Analyst JG  
 Matrix: KINETIC WIFE 3000 Date Analyzed 4/22/99 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution.

Comment: T-3 POST TEST

LAB ID	001	002	003	004	005	006	007	008	009	010	011
SAMPLE DESCRIPTION	001	002	003	004	005	006	007	008	009	010	011
Dilution	1	1	1	1	1	1	1	1	1	1	1
SAMPLE VOLUME	-	-	-	-	-	-	-	-	-	-	-
UNITS	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
HMX	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
RDX	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
1,3,5-TNB	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
1,3-DNB	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
NB	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
Tetryl	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
2,4,6-TNT	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
2,6-DNT	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7
2,4-DNT	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7	12.7

QUALC DATE - 8/19/99

## DATA SUMMARY

RFW Batch 5808H00002  
Installation H501H00001  
Matrix: PENTAC WIFE & GOLF

**Note: Data is corrected for dilution.**

**Comment: T.B. POST TEST**

[illegible][illegible]

## DATA SUMMARY

Units RM 111111-111111-111111-111111-111111  
Analyst Gato  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution, %**

Comment: T-8 POST TEST

[illegible][illegible]

# WESTON ANALYTICS EXPLOSIVES DATA SUMMARY

RFW Batch GA1006 610016A Analytical Lot Units 610016-610018 2106-1-1-1118 2106-1-1-1118  
 Installation HAZARDOUS Date Prepared Analyst  
 Matrix: SWAYNE WIFE & SON Date Analyzed 610016-2 Reviewed

Note: Data is corrected for dilution.

Comment:

LAB ID #	BLANK	IOX	BLANK	IOX	BLANK	IOX	BLANK	IOX	BLANK	IOX
	RINSE	WIFE	RINSE	WIFE	RINSE	WIFE	RINSE	WIFE	RINSE	WIFE
Dilution	1	1	1	1	1	1	1	1	1	1
UNITS	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg
HMX	0.635	0.65	0.635	0.65	0.635	0.65	0.635	0.65	0.635	0.65
RDX	0.490	0.70	0.490	0.70	0.490	0.70	0.490	0.70	0.490	0.70
1,3,5-TNB	1.05	1.2	1.05	1.2	1.05	1.2	1.05	1.2	1.05	1.2
1,3-DNB	0.295	0.15	0.295	0.15	0.295	0.15	0.295	0.15	0.295	0.15
NB	0.210	0.03	0.210	0.03	0.210	0.03	0.210	0.03	0.210	0.03
Tetryl	2.5	23.2	2.5	23.2	2.5	23.2	2.5	23.2	2.5	23.2
2,4,6-TNT	0.960	0.95	0.960	0.95	0.960	0.95	0.960	0.95	0.960	0.95
2,6-DNT	0.200	0.06	0.200	0.06	0.200	0.06	0.200	0.06	0.200	0.06
2,4-DNT	0.210	0.09	0.210	0.09	0.210	0.09	0.210	0.09	0.210	0.09



**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16,19,27, 8-1,5,10,16,20,22,29, 9-2,11,20

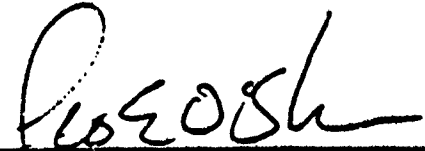
RFW #: 3907L058,059,154 8908L203,258,315,393,462,524,534,595  
8909L595,679,804

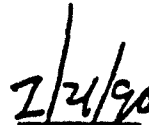
W.O. #: 2281-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

  
\_\_\_\_\_  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L258

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T5 FLASH CHMB WALL	NITRATED ESTERS	5.0 u	UG	5.0
-002	T5 SMW2 POST TEST	NITRATED ESTERS	5.6	UG	5.0
-003	T-8 SMW2 <del>POST</del> TEST PRE <sup>42</sup>	NITRATED ESTERS	13.0	UG	5.0
-004	T-8 WIPE BLANK PRE-	NITRATED ESTERS	5.8	UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L25:

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC010-MB1	NITRATED ESTERS	2.5 u	MG/L	2
BLANK20	89LNC010-MB2	NITRATED ESTERS	2.5 u	MG/L	2

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-03-02-0000

WESTON BATCH #: 6908L258

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC010-MB1	NITRATED ESTERS	9.9	2.5 u	10.0	98.8
BLANK20	89LNC010-MB2	NITRATED ESTERS	52.9	2.5 u	50.0	106
		NITRATED ESTERS	51.8	2.5 u	50.0	104

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA / HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L2

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC010-MB2	NITRATED ESTERS	106	104	2.2

## ROY F. WESTON INC.

## INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L315

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T-8-SM-W2 POST TEST	NITRATED ESTERS	5.3	UG	5.0
-002	T-8-CHAMBER WALL-W2	NITRATED ESTERS	7.5	UG	5.0
-003	T8-WIPE BLANK W2 POS	NITRATED ESTERS	5.0	u UG	5.0
-004	T13-SM-W-2 PRE TEST	NITRATED ESTERS	12.5	UG	5.0
-005	T13-WIPE BLANK W2 ET	NITRATED ESTERS	5.0	u UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L31

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC010-MB1	NITRATED ESTERS	2.5 u	MG/L	2
BLANK20	89LNC010-MB2	NITRATED ESTERS	2.5 u	MG/L	2



ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L315

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECV
BLANK10	89LNC010-MB1	NITRATED ESTERS	9.9	2.5 u	10.0	98.8
BLANK20	89LNC010-MB2	NITRATED ESTERS	52.9	2.5 u	50.0	106
		NITRATED ESTERS	51.8	2.5 u	50.0	104

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L3

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC010-MB2	NITRATED ESTERS	106	104	2.2

July 1990  
Revision: Final

TEST RUN 13  
500°F/12 HOURS

1311R2

## Custody Transfer Record/Lab Work Request

870340021	WESTON Analytics Use Only
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15A TITANE / HVAAP

Work Order 22BX-CB-02

Date Rec'd. \_\_\_\_\_ Date Due \_\_\_\_\_

RFW Contact - Yenick, M. 304

Client Contact/Phone (213) 737-3333

WA Use Only Lab ID	Client ID/Description
001	T13 P31 LUNATE R1
002	R2
003	R3
004	R4
005	T13 P32 LUNATE R1
006	R2
007	R3
008	R4
009	T13 CP SOIL
010	FIELD BLANK
011	T13 SSR1 SAMPLE
012	T13 SSR2 SPIKE LUNATE
013	T13 PB FIELD BLANK

<u>Refrigerators</u>	<u>#Type Container</u>	<u>Containers Volume</u>	<u>Preservative</u>	<u>ANALYSES REQUESTED</u> ➔	<u>Date Collected</u>	<u>Matrix</u>
		Amies Swab			X	AEN
					X	↓
					X	↓
					X	AGN
					X	↓
					X	↓
					X	SOLD
					X	HON
					X	AEN
					X	ACN
					X	AGN

WESTON Analytics Use Only	Samples Were: 1 Shipped or Hand- Delivered NOTES:	2 Ambient or Chilled NOTES:	3 Received Broken/ Leaking (Improperly Sealed) Y N NOTES:	4 Properly Preserved Y N NOTES:	5 Received Within Holding Times Y N NOTES:	COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample NOTES: Y N	COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:
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Special Instructions: T13 PAE TEST SAMPLES

[illegible]

**WESTON**

# Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only

8908H2021

Client USATAMA / HWAAP

Work Order 2281-68-02

Date Rec'd 4/10/2017

RFW Contact (215) 430-3117

Client Contact/Phone (215) 430-3117

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator #	#Type Container	Container Volume	Preservative	ANALYSES REQUESTED	WESTON Analytica Use Only
Q14	T13 S561 W1 UPPER	WAF			VDA				<p>1 Shipped or Hand Delivered</p> <p>NOTES:</p> <p>2 Ambient or Chilled</p> <p>NOTES:</p> <p>3 Received Broken/Leaking (Integrity Sealed)</p> <p>Y N</p> <p>NOTES:</p> <p>4 Property Preserved</p> <p>Y N</p> <p>NOTES:</p> <p>5 Received With Holding Times</p> <p>Y N</p> <p>NOTES:</p>
Q15	W2								
Q16	W3								
Q17	W4								
Q18	W5 LOWER								<p>COC Tape Was:</p> <p>1 Present on Outer Package Y N</p> <p>2 Unbroken in Outer Package Y N</p> <p>3 Present on Sample Y N</p> <p>4 Unbroken on Sample Y N</p> <p>NOTES:</p>
Q19	W6								
Q20	W7								
Q21	W8								
Q22	T13 S562 W1 UPPER								<p>COC Record Was:</p> <p>1 Present Upon Receipt of Samples Y N</p> <p>Discrepancies Between Sample Labels and COC Record? Y N</p> <p>NOTES:</p>
Q23	W2								
Q24	W3								
Q25	W4								

Matrix: W - Water O - Oil DL - Drum Liquids  
 S - Solid A - Air F - Fish  
 SD - Solid

Special Instructions:

T-13 PRE TEST SAMPLES

Name/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	C. Yank		8/24						





# WESTON ANALYTICS EXPLOSIVES DATA SUMMARY

RFV Batch 2303M2021 Analytical Lot \_\_\_\_\_ Units ~~ANALYST~~ ~~DATE~~ ~~REVIEWED~~ 2018  
 Installation WHOLESALE Date Prepared \_\_\_\_\_ Analyst \_\_\_\_\_  
 Matrix: 2303M2021 Date Analyzed 2018 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution.

Comment: T-13 PRE TEST

LAB ID #	Q21-030	Q21-031	Q21-032	Q21-033	Q21-034	Q21-035	Q21-036	Q21-037	Q21-038	Q21-039	Q21-040
SAMPLE DESCRIPTION	T-13	T-13	T-13	T-13	T-13	T-13	T-13	T-13	T-13	T-13	T-13
Dilution	1	1	10	100	10	10	100	100			
SAMPLE VOLUME	-	-	250	250	250	250	250	250			
UNIT'S	12.7	57.7	26.35	26.35	26.35	26.35	26.35	26.35			
HMX	29.80	29.80	29.80	29.80	29.80	29.80	29.80	29.80			
RDX	220.9	220.9	220.9	220.9	220.9	220.9	220.9	220.9			
1,3,5-TNB	25.90	25.90	25.90	25.90	25.90	25.90	25.90	25.90			
1,3-DNB	2.94	2.94	2.94	2.94	2.94	2.94	2.94	2.94			
NE	250.0	250.0	250.0	250.0	250.0	250.0	250.0	250.0			
Tetryl	219.2	219.2	219.2	219.2	219.2	219.2	219.2	219.2			
2,4,6-TNT	24.20	24.20	24.20	24.20	24.20	24.20	24.20	24.20			
2,6-DNT	24.20	24.20	24.20	24.20	24.20	24.20	24.20	24.20			
2,4-DNT	24.20	24.20	24.20	24.20	24.20	24.20	24.20	24.20			
UNITS	219.2	219.2	219.2	219.2	219.2	219.2	219.2	219.2			





WESTON 4 8.3

Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only  
8903 HWO25

Client USAFHAMA / HWAAP  
Work Order 2281-08-02  
Date Rec'd. Subaka  
RFW Contact Subaka  
Client Contact/Phone (215) 430-3117

WA Use Only Lab ID	Client ID/Description
012	T13 CP - Soil
013	T13 Field Blank Rinse-R1
014	T13 PBA R1 Post
015	R3
016	R3
017	R4
018	T13 PA-Field Blank R1
019	T13 API R1 Post
020	R3
021	R3
022	R4

Matrix: W - Water D3 - Drum Solids  
S - Soil O - Oil DL - Drum Liquids  
SE - Sediment A - Air F - Fish  
BO - Solid X - Other

Reinforced	Relinquished by	Received by	Date	Time
	<u>Subaka</u>		<u>8/14/89</u>	

Refrigerator	#Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED	Matrix	Date Collected
	VERA 1125	500ml	COOL	EXPENSIVE	Soil	8-14-89
					ACN	8-14-89
					ACN	8-14-89
					↓	↓
					↓	↓
					ACN	8-14-89
					ACN	8-14-89
					↓	↓
					↓	↓
					ACN	8-14-89
					ACN	8-14-89
					↓	↓
					↓	↓

T13 Post Test Samples

Reinforced	Relinquished by	Received by	Date	Time

WESTON Analytica Use Only

Samples Were:  
1 Shipped or Hand-Delivered  
NOTES:

2 Ambient or Chilled  
NOTES:

3 Received Broken/Leaking (Improperly Sealed)  
Y N  
NOTES:

4 Properly Preserved  
Y N  
NOTES:

5 Received Within Holding Times  
Y N  
NOTES:

COC Tape Was:  
1 Present on Outer Package Y N  
2 Unbroken on Outer Package Y N  
3 Present on Sample Y N  
4 Unbroken on Sample Y N  
NOTES:

COC Record Was:  
1 Present Upon Receipt of Samples Y N  
Discrepancies Between Sample Labels and COC Record? Y N  
NOTES:

3013

WESTON

## Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only
8908 K20025

Client: USATHHMA / HWAAP

Work Order: 2281-08-02

Date Rec'd: 2/27/09

RFW Contact: Subacka / N. Johnson

Client Contact/Phone: (215) 430-3117

W/A Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator #/Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED
023	T13 SHRI RI Post	KN	8-14-89	X			
024	R2 Post	↓	↓				
025	R3 ↓	↓	↓				
026	R4 ↓	↓	↓				
027	T13 SHRI Field Chiller	KN	8-14-89	X			

Special Instructions:

Matrix: W - Water DS - Dism Solids  
 O - Oil OL - Dism Liquids  
 SG - Sediment A - Air F - Fish  
 CO - Solids X - Other

Name/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	<i>A.T. Subacka</i>		2/27/09						

RFW 21-21-001/A-588

2-915

WESTON Analytica Use Only	
Samples Were:	
1 Shipped or Hand-Delivered	NOTES:
2 Ambient or Chilled	NOTES:
3 Received Broken/Leaking (Improperly Sealed)	NOTES:
4 Properly Preserved	NOTES:
5 Received Within Holding Times	NOTES:
COC Tape Was:	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
COC Record Was:	
1 Present Upon Receipt of Samples	Y N
Discrepancies Between Sample Labels and COC Record?	
Y N	NOTES:

T13 Post Test Samples



**WEBSTON ANALYTICAL EXPLOSIVES**

RFW Batch 8908H02025  
Installation HAWTHORNE  
Matrix: RUSSTE-WPPT-5016  
Analytical Lot \_\_\_\_\_  
Date Prepared \_\_\_\_\_  
Date Analyzed 8/14/89  
Units RUSSTE-WPPT-5016 ug 5016-1  
Analyst JGM  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution.**

Comment: T-13 POST TEST

[illegible]

# WESTON ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFM Batch 530RH2025 Analytical Lot                      Units QMSITE-115300 WIPE - Handing SON-1  
 Installation WASTHORN Date Prepared                      Analyst QAM  
 Matrix: QMSITE WPE 1501C Date Analyzed 8/14/89 Reviewed                     

Note: Data is corrected for dilution, "

Comment: I-13 POST TEST

MATRIX	R		F		R		R		R	
LAB ID #	025-	023	025-	024	025-	025	025-	026	025-	027
SAMPLE DESCRIPTION	T13 SAC1 R1	T13 SAC1 R2	T13 SAC1 R3	T13 SAC1 R4	T13 SAC1 R5	T13 SAC1 R6	T13 SAC1 R7	T13 SAC1 R8	T13 SAC1 R9	T13 SAC1 R10
Dilution	1	1	1	1	1	1	1	1	1	1
SAMPLE VOLUME (mL)	300	300	300	300	300	300	300	300	300	300
UNITS	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg	ug/mg
HMX	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635
RDX	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490	<0.490
1,3,5-TNB	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05
1,3-DNB	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295
NB	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210
Tetryl	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5
2,4,6-TNT	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960	<0.960
2,6-DNT	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200	<0.200
2,4-DNT	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210

-QALAC DATE - 8/14 - 8/14 8/14 8/14  
 (1989)

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16,19,27, 8-1,5,10,16,20,22,29, 9-2,11,20

RFW #: 8307L058,059,154 8908L203,258,315,398,462,524,534,595  
8909L595,679,804

W.O. #: 2281-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

  
\_\_\_\_\_  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable; result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.



ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WGRK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L3

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORT LIMIT
-----	-----	-----	-----	-----	-----
-001	T-8-SM-W2 POST TEST	NITRATED ESTERS	5.3	UG	!
-002	T-8-CHAMBER WALL-W2	NITRATED ESTERS	7.5	UG	!
-003	T8-WIPE BLANK W2 POS	NITRATED ESTERS	5.0 u	UG	!
-004	T13-SM-W-2 PRE TEST	NITRATED ESTERS	12.5	UG	!
-005	T13-WIPE BLANK W2 ET	NITRATED ESTERS	5.0 u	UG	!

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L315

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC010-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC010-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%R
-----	-----	-----	-----	-----	-----	---
BLANK10	89LNC010-MB1	NITRATED ESTERS	9.9	2.5 u	10.0	
BLANK20	89LNC010-MB2	NITRATED ESTERS	52.9	2.5 u	50.0	1
		NITRATED ESTERS	51.8	2.5 u	50.0	1

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L315

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC010-M82	NITRATED ESTERS	106	104	2.2

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L3

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORT LIMIT
-----	-----	-----	-----	-----	-----
-001	POST T13 SM WS (ETOH)	NITRATED ESTERS	5.0	u UG	
-002	POST T13FC CH WAL W2	NITRATED ESTERS	5.0	u UG	
-003	POST T13 WIPE BL W2	NITRATED ESTERS	7.5	UG	
-004	PRE T14 SMW2 (ETOH)	NITRATED ESTERS	5.0	u UG	
-005	PRE T14 WIPE BL W2	NITRATED ESTERS	5.0	u UG	

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L398

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC010-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC010-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5

ROY F. WESTON INC.  
INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RI
BLANK10	89LNC010-MB1	NITRATED ESTERS	9.9	2.5 u	10.0	9
BLANK20	89LNC010-MB2	NITRATED ESTERS	52.9	2.5 u	50.0	10
		NITRATED ESTERS	51.8	2.5 u	50.0	10

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L398

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC010-MB2	NITRATED ESTERS	106	104	2.2



July 1990  
Revision: Final

TEST RUN 14  
400°F/12 HOURS

1311R2

WESTON Analytica Use Only
2006H0024

# Custody Transfer Record/Lab Work Request



Client USATHAMA / HWAAP  
 Work Order 2281-08-02  
 Date Rec'd. 8-14-87  
 RFW Contact Salacka, Nancy Johnson  
 Client Contact/Phone (205) 430-3117

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator #/Type Container	Preservative	ANALYSES REQUESTED
001	T14 SSRI W1 upper	Wipe	8-14-87	X		
002	W2			X		
003	W3			X		
004	W4			X		
005	W5 lower			X		
006	W6			X		
007	W7			X		
008	W8			X		
009	T14 SSRI W1 upper	Wipe	8-14-87	X		
010	W2			X		
011	W3			X		
012	W4			X		
013	W5 lower			X		
014	W6			X		
015	W7			X		

Matrix: W - Water DS - Drum Solids  
 S - Soil O - Oil DL - Drum Liquids  
 SE - Sediment A - Air F - Fish  
 SO - Solid X - Other

T14 Pre-test samples

Item/Reason	Relinquished by	Received by	Date	Time	Relinquished by	Received by	Date	Time
	<u>N. Salacka</u>		<u>8-14-87</u>					

<b>WESTON Analytica Use Only</b> Samples Were: 1 Sealed or Hand-Delivered NOTES: 2 Ambient or Chilled NOTES: 3 Received Broken/Leaking (Improperly Sealed) Y N NOTES: 4 Properly Preserved Y N NOTES: 5 Received Within Holding Times Y N NOTES:	<b>CCC Tape Was:</b> 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:	<b>COC Record Was:</b> 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:
--	--	--

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WESTON

# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only

8708 HLM234

Client: USA THANA / HWAAP

Work Order: 2281-08-02

Date Rec'd: 2/14/89

RFW Contact: Sal Jacka / N. Johnson

Client Contact/Phone: (215) 430-3117

WA Use Only	Client ID/Description	Matrix	Date Collected	Refrigerator #/Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
017	T14 SSB2 W8 100gr	Wipe	8-14-89													
018	SM W1 (ACN)	Wipe	8-14-89													
019	T14 Wipe Blank W1 (ACN)	Wipe	8-14-89													
020	T14 CP Soil	Soil	8-14-89													
021	T14 Field Blank Rinse - Soap ACN	ACN	8-14-89													
022	T14 PBI R'	ACN	8-14-89													
023	R3	↓	↓													
024	R4	↓	↓													

Mobile: W - Water DS - Drum Solids O - Oil DL - Drum Liquids SE - Sediment A - Air F - Fish SO - Solid X - Other

Special Instructions:

T14 Pre-Test Samples

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	Sal Jacka		8-14-89						



## WESTERN ANALYTICAL EXPLOSIVES

RFW Batch 802H6202Y  
Installation HAWTHORNE  
Matrix: ANSDELAURE 150N

Analytical Lot  
Date Prepared  
Date Analyzed

9/14/99

Units Reviewed  
Analyst  
Reviewed

**Note: Data is corrected for dilution, %**

Comment: T-14 PRE TEST

LABEL	DILUTION	SAMPLE VOLUME	UNITS
LAB ID #			
SAMPLE DESCRIPTION			
Dilution	(mL)		
SAMPLE VOLUME			
UNITS			
RHX			
RUX			
1,3,5-TNB			
1,3-DNB			
NB			
Tetryl			
2,4,6-TNT			
2,6-DNT			
2,4-DNT			

.. QNLOC DATE

**WESTON ANALYTICAL EXPLOSIVES**

Units element - ughd uipe - tclug sllc-ufg  
Analyst gpm  
Reviewed \_\_\_\_\_

RRFW Batch 9908K02024 Analytical Lot \_\_\_\_\_  
 Installation HAUSTHURNE Date Prepared \_\_\_\_\_  
 Matrix: ENVIRONMENTAL SOIL Date Analyzed \_\_\_\_\_

**Note: Data is corrected for dilution.**

**Comment:** T-14 PPE TEST

[illegible]

**WESTON ANALYTICAL EXPLOSIVES**

## DATA BONDAGE

RRFW Batch QALCC 2/14/69  
Installation HAWAIIAN  
Matrix: BUNDAF-WOPE & SOIL

**Notes: Data is corrected for dilution.**

**Comment:**

MATERIAL LAB ID #	R		R		L2		L3		S	
	BLANK	ION	BLANK	ION	BLANK	ION	BLANK	ION	BLANK	ION
	RWATE	RWATE SPIKE	BLANK WIPE	ION WIPE SPIKE	BLANK	ION	BLANK	ION	BLANK	ION
Dilution	1	1	1	1	1	1	1	1	1	1
UNITS	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L	ug/L
HMX	60.675	6.85	612.7	142	1124	1024	612.7	13.2	1024	1024
RDX	60.490	4.81	612.7	99.3	1024	1024	612.7	9.15	1024	1024
1,3,5-TNB	61.05	9.95	620.9	206	112	112	620.9	19.4	112	112
1,3-DNB	60.225	2.77	65.50	57.3	60.590	5.39	60.590	5.39	60.590	5.39
HB	60.210	2.02	64.20	42.2	60.420	4.19	60.420	4.19	60.420	4.19
Tetryl	62.5	23.5	650.0	487	650	650	650.0	43.4	650	650
2,4,6-TNT	60.960	8.25	619.2	172	632	632	619.2	15.9	632	632
2,6-DNT	60.200	2.11	640.0	43.2	602	602	640.0	4.07	602	602
2,4-DNT	60.210	1.95	642.0	40.2	602	602	642.0	3.91	602	602

WESTON

# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only

8908HW026

Client: USATHAMA / HWIAP

Work Order: 2281-08-02

Date Rec'd: 2/18/87

RFW Contact: Slacka / N Johnson

Client Contact/Phone: (214) 430-3117

WA Use Only	Lab ID	Client ID/Description
	001	TIH SSRI W1 upper
	002	W3
	003	W3
	004	W4
	005	W5 lower
	006	W6
	007	W7
	008	W8
	009	TIH SM W1 ACN
	010	TIH EC Wells W1 ACN
	011	TIH Wipe Blank W1 ACN

Refrigerator	W1
#/Type Container	W1
Containers/Volume	W1
Preservative	W1
ANALYSES REQUESTED	W1
Date Collected	8-18-87
Matrix	Wipe
Time	
Received by	
Relinquished by	
Item/Reason	
Date	
Time	

Special Instructions:

W - Wipe DS - Drum Solids  
 O - Oil DL - Drum Liquids  
 SS - Sediment A - Air F - Fish  
 SO - Solid X - Other

TIH Post Test Samples

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	Slacka		2/18/87						

WESTON Analytics Use Only

Samples Were:

1 Shipped or Hand-Delivered

NOTES:

2 Ambient or Chilled

NOTES:

3 Received Broken/Leaking (Integrity Sealed)

Y N

NOTES:

4 Properly Preserved

Y N

NOTES:

5 Received Within Holding Times

Y N

NOTES:

COC Tape Was:

1 Present on Outer Package Y N

2 Unbroken on Outer Package Y N

3 Present on Sample Y N

4 Unbroken on Sample Y N

NOTES:

COC Record Was:

1 Present Upon Receipt of Samples Y N

Discrepancies Between Sample Labels and COC Record?

Y N

NOTES:



WESTON Analytica Use Only
8908HW026

# Custody Transfer Record/Lab Work Request

WESTON Analytica

Client USATHAMA / HWAAP  
 Work Order 2281-08-02  
 Date Rec'd. 2/15/08  
 ASW Contact Salacko / N. Johnson  
 Client Contact Phone (215) 430-3119

Refill/Operator #	Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED	Matrix	Date Collected
	Amber	200.1	Evap	EXPLOSIVE		
013	T14 CP	SOIL			SOIL	8-18-89
013	T14 CP	FIELD BLANK			ACN	8-18-89
014	T14 PBI	R1			ACN	8-18-89
015		R3				
016		R3				
017		R4				
018	T14 PBI	FIELD BLANK			ACN	8-18-89
019	T14 SPI	R1			ACN	8-18-89
020		R2				
021		R3				
022		R4				

Matrix: W - Water DS - Drum Solids  
 S - Soil O - Oil DL - Drum Liquids  
 SS - Sediment A - Air F - Fish  
 SO - Solid X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	<u>N. T. Salacko</u>								

T14 Post Test Samples

WESTON Analytica Use Only Samples Were: 1 Shipped or Hand-Delivered NOTES: 2 Ambient or Chilled NOTES: 3 Received Broken/Leaking (Improperly Sealed) Y N NOTES: 4 Properly Preserved Y N NOTES: 5 Received Within Holding Times Y N NOTES:	COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:	COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:
--	---	--

WESTON ANALYTICS

# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only

8908HW026

Client: USATHAMIA/HWAAP

Work Order: 2381-08-02

Date Rec'd: 2/18/89

RFW Contact: Salacke

Client Contact/Phone: 215-430-3117

WA Use Only Lab ID	Client ID/Description
023	TH SHB RI
024	BA
025	R3
026	R4
027	TH SHB Field Blank RI

Refrigerator	#Type Container	Container Volume	Preservative	ANALYSES REQUESTED	Matrix	Date Collected
	Amber	500ml	Citric Acid	EXP	ACN	8-18-89
					↓	↓
					↓	↓
					ACN	8-18-89

Special Instructions:

TH Post Test Samples

Media: W - Waste, DS - Drum Solids, O - Oil, DL - Drum Liquids, SE - Sediment, A - Air, F - Fish, SO - Solid, X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	Salacke		2/18/89						

WESTON Analytics Use Only

Samples Were: 1 Shipped or Hand-Delivered

NOTES:

2 Airtight or Chilled

NOTES:

3 Received Bickered Leaking (improperly Sealed)

Y N

NOTES:

4 Properly Preserved

Y N

NOTES:

5 Received Within Holding Times

Y N

NOTES:

COC Tape Was:

1 Present on Outer Package Y N

2 Unbroken on Outer Package Y N

3 Present on Sample Y N

4 Unbroken on Sample Y N

NOTES:

COC Record Was:

1 Present Upon Receipt of Samples Y N

Discrepancies Between Sample Labels and COC Record? Y N

NOTES:

## DATA SUMMARY

RFW Batch 99CS HW 022 -  
Installation HAWTHORNE  
Matrix: Ringold, Wipe, & Soil

Analytical Lot  
Date Prepared  
Date Analyzed

Units Rinckel USM, Wipe-Tests  
Analyst AIS  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution.**

Comment: T-14 Post test Samples

[illegible]

Office Date (1957)

## DATA SUMMARY

RFW Batch 9908 MW 026-  
Installation - MATHERNE  
Matrix: Rineau, Wipe, & Still

Analytical Lot  
Date Prepared  
Date Analyzed

Analytical Lot	
Date Prepared	
Date Analyzed	5/15/31/5

Units \_\_\_\_\_  
Analyst \_\_\_\_\_  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution.**

connect:  
T-14 Post test Samples

[illegible]

GAJEE Date - 8/18/1959

# WESTON ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFW Batch 94108-HW 026-  
Installation WASHINGTON  
Matrix: Rinsate, Wipe, & Soil

Analytical Lot  
Date Prepared  
Date Analyzed

Units Rinsate  $\mu\text{g/ml}$ , wipe-Tet, Soil  $\mu\text{g/g}$   
Analyst  
Reviewed

Note: Data is corrected for dilution.

Comment: T14 Test Samples 7

MATRIX	R	R	R	R	R	R	R	R	R
LAB ID	026-023	026-024	026-025	026-026	026-027				
Sample Description	T14 SHRI R1	T14 SHRI R2	T14 SHRI R3	T14 SHRI R4	T14 SHRI R5				
Dilution	1	1	1	1	1				
Sample $\mu\text{l}/\text{st}$	200 ml	300 ml	300 ml	300 ml	250 ml				
Unit	$\mu\text{g/ml}$	$\mu\text{g/ml}$	$\mu\text{g/ml}$	$\mu\text{g/ml}$	$\mu\text{g/ml}$				
HMX	2.44	2.40	1.50	0.98	0.635				
RDX	21.9	22.9	8.65	2.9	0.49				
1,3,5-TNB	2.33	2.24	1.23	1.05	1.05				
1,3-DNB	0.215	0.215	0.215	0.215	0.215				
NB	0.210	0.210	0.210	0.210	0.210				
Tetryl	0.25	0.25	0.25	0.25	0.25				
2,4,6-TNT	273	28.2	17.0	11.3	0.96				
2,6-DNT	0.20	0.20	0.20	0.20	0.20				
2,4-DNT	0.36	0.395	0.465	0.25	0.21				

Exp/oc Date 5/18 8/15 8/18 8/18 8/18

(1997)

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16, 19, 27, 8-1, 5, 10, 16, 20, 22, 29, 9-2, 11, 20

RFW #: 8907L058, 059, 154 8908L203, 258, 315, 398, 462, 524, 534, 595  
8909L595, 679, 804

W.O. #: 2281-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

7/24/90  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L398

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-----	-----	-----	-----	-----	-----
-001	POST T13 SM WS (ETOH	NITRATED ESTERS	5.0 u	UG	5.0
-002	POST T13FC CH WAL W2	NITRATED ESTERS	5.0 u	UG	5.0
-003	POST T13 WIPE BL W2	NITRATED ESTERS	7.5	UG	5.0
-004	PRE T14 SMV2 (ETOH)	NITRATED ESTERS	5.0 u	UG	5.0
-005	PRE T14 WIPE BL W2	NITRATED ESTERS	5.0 u	UG	5.0



ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-02-0000

WESTON BATCH #: 8908L39

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTI LIMIT
BLANK10	89LNC010-MB1	NITRATED ESTERS	2.5 u	MG/L	2
BLANK20	89LNC010-MB2	NITRATED ESTERS	2.5 u	MG/L	2

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #. 8908L398

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC010-MB1	NITRATED ESTERS	9.9	2.5 u	10.0	98.8
BLANK20	89LNC010-MB2	NITRATED ESTERS	52.9	2.5 u	50.0	106
		NITRATED ESTERS	51.8	2.5 u	50.0	104

ROY F. WESTON INC.  
INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L3

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC010-MB2	NITRATED ESTERS	106	104	2.2

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-02-0000

WESTON BATCH #: 8908L462

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T14 SM W2 ETOH (POST	NITRATED ESTERS	5.0 u	UG	5.0
-002	T14 FC WALLS W2 ETOH	NITRATED ESTERS	20.3	UG	5.0
-003	T14 POST WIPE BLANK	NITRATED ESTERS	5.0 u	UG	5.0
-004	T15 PRE SM W2 ETOH	NITRATED ESTERS	6.6	UG	5.0
-005	T15 PRE WIPE BLANK	NITRATED ESTERS	5.0 u	UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02 0000

WESTON BATCH #: 8908L4

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORT LIMIT
-----	-----	-----	-----	-----	-----
BLANK10	89LNC012-MB1	NITRATED ESTERS	2.5 u	MG/L	
BLANK20	89LNC012-MB2	NITRATED ESTERS	2.5 u	MG/L	

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L462

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC012-MB2	NITRATED ESTERS	95.2	97.6	2.5

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 3908L

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RI
BLANK10	89LNC012-MB1	NITRATED ESTERS	10.1	2.5 u	10.0	10
BLANK20	89LNC012-MB2	NITRATED ESTERS	47.6	2.5 u	50.0	50
		NITRATED ESTERS	48.8	2.5 u	50.0	50

July 1990  
Revision: Final

TEST RUN 15  
600°F/12 HOURS

1311R2



WESTON

Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only  
8908H-V027

Client: USATHAMA / HW/AAP  
Work Order: 2281-08-02  
Date Rec'd: \_\_\_\_\_ Date Due: \_\_\_\_\_  
RFW Contact: Subrock / A. Johnson  
Client Contact/Phone (215) 430-3117

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator#	#Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED	WESTON Analytica Use Only
EE1	TIS SSR1 W1 upper	Wipe	8-21-87	VOA					Samples Were: 1 Shipped or Hand-Delivered NOTES:  2 Ambient or Chilled NOTES:  3 Received Broken/Leaking (improperly Sealed) Y N NOTES:  4 Properly Preserved Y N NOTES:  5 Received Within Holding Times Y N NOTES:  COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:  COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:
EE2	W2								
EE3	W3								
EE4	W4								
EE5	W5 lower								
EE6	W6								
EE7	W7								
EE8	W8								
EE9	TIS SSR2 W1 upper	Wipe	8-21-87						
EE10	W2								
EE11	W3								
EE12	W4								
EE13	W5 lower								
EE14	W6								
EE15	W7								

TIS PRE TEST SAMPLES

Special Instructions:  
W - Water DS - Drum Solids  
O - Oil DL - Drum Liquids  
SE - Sediment A - Air F - Fish  
SO - Solid X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

# Custody Transfer Record/Lab Work Request

WESTON

WESTON Analytica Use Only

8908HW027

Client USATHAMA / HW/AP

Work Order 2281-08-02

Date Rec'd. Salacka Date Due N. Johnson

RFW Contact Salacka

Client Contact/Phone (215) 730-3117

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator#	#Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED
016	T15 SSR2 W8 1600g	Wipe	8-21-89		VEA Amber	800m		
017	T15 SM W1 ACN	Wipe	8-21-89					
018	T15 Wipe Blank W1 ACN	Wipe	8-21-89					
019	T15 CP Soil	Soil	8-21-89					
020	T15 CP FISH Blank Rinse	ACN	8-21-89					
021	T15 PBI R1	ACN	8-21-89					
022	R3							
023	R3							
024	R4							

Matrix: W - Water DS - Drum Solids Special Instructions: T15 Pre Test Samples

S - Soil O - Oil DL - Drum Liquids  
SE - Sediment A - Air F - Fish  
SO - Solid X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time
	<u>H. T. Salacka</u>		<u>8/21/89</u>						

WESTON Analytica Use Only

Samples Were:  
1 Shipped or Hand-Delivered  
NOTES:

2 Ambient or Chilled  
NOTES:

3 Received Broken/Leaking (Improperly Sealed)  
Y N  
NOTES:

4 Properly Preserved  
Y N  
NOTES:

5 Received Within Holding Times  
Y N  
NOTES:

COC Tape Was:  
1 Present on Outer Package Y N  
2 Unbroken on Outer Package Y N  
3 Present on Sample Y N  
4 Unbroken on Sample Y N  
NOTES:

COC Record Was:  
1 Present Upon Receipt of Samples Y N  
Discrepancies Between Sample Labels and COC Record? Y N  
NOTES:

WESTON

# Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only

8908HW027

Client: KAITHAMPA / HWVAP

Work Order: 2281-05-02

Date Rec'd: 2/15/89

RFW Contact: SALUKA / A. JOHNSON

Client Contact Phone: (215) 430-3117

WA Use Only Lab ID	Client ID/Description
025	T15 PB2 RI
026	B3
027	B3
028	B4
029	T15 PB Field Blank RI
030	T15 API Spike Rinsate
031	T15 APA Spike Rinsate
032	T15 SSR1 Spike Rinsate
033	T15 SSR2 Spike Rinsate

Matrix: W - Water DS - Drum Solids O - Oil DL - Drum Liquids SE - Sediment A - Air F - Fish SO - Solids X - Other

T15 Pre Test Samples

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

<b>WESTON Analytica Use Only</b> Samples Were: 1 Shipped or Hand-Delivered NOTES: 2 Ambient or Chilled NOTES: 3 Received Broken/Leaking (If Properly Sealed) Y N NOTES: 4 Properly Preserved Y N NOTES: 5 Received Within Holding Times Y N NOTES:		<b>COC Tape Was:</b> 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:	<b>COC Record Was:</b> 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record Y N NOTES:
--	--	--	---

## DATA SUMMARY

Reviewed

Comment: T15 Pre Test Samples.

[illegible]

1921

## DATA SUMMARY

RFH Batch 8768410-007--

## Analytical Lot

## Installation Wichtige Hinweise

Date Prepared

Matrix: React, cope, & sell

La fe de la fe de la fe

Units  
Kingsbury  
Application  
1955  
10/26/55

**Analyst** \_\_\_\_\_ **A.C.**

Reviewed

**Note: Data is corrected for dilution, %**

comment: T15 Pre Test samples

[illegible][illegible]

(1201)

## Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only
8708440-029 -

Client USATHAMA / HUNAP

Work Order 2281-03-02

Date Rec'd. \_\_\_\_\_

RFW Contact N. Johnson, M. MARELON

Client Contact/Phone \_\_\_\_\_

WA Use Only Lab ID	Client ID/Description	Date		Matrix	Date Collected	Refrigerator		ANALYSES REQUESTED	Preservative		Containers/Volume		Type Container		Seal		Date	
		Matrix	Date			Matrix	Date		Matrix	Date	Matrix	Date	Matrix	Date	Matrix	Date	Matrix	Date
001	TIS SSR 1 W1 TOP	W1	8/24/89	W1	8/24/89													
002	TIS SSR 1 W2 TOP	W2																
003	TIS SSR 1 W3 TOP	W3																
004	TIS SSR 1 W4 TOP	W4																
005	TIS SSR 1 W5 BOTTOM	W5																
006	TIS SSR 1 W6 BOTTOM	W6																
007	TIS SSR 1 W7 BOTTOM	W7																
008	TIS SSR 1 W8 BOTTOM	W8																
009	TIS SSR FIELD Blank	Blank																
010	TIS API R1 Post Test	API R1																
011	TIS API R2	API R2																
012	TIS API R3	API R3																
013	TIS API R4	API R4																
014	TIS API FIELD Blank	Blank																

Matrix: W - Water DS - Drum Solids Special Instructions: T-15 POST TEST SAMPLES

S - Soil O - Oil DL - Drum Liquids

SE - Sediment A - Air F - Fish

SO - Solid X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

RFW 21-21-001/A-5788

EXP = EXPLOSIVES

## Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only
8908 HW - 009 -

Client USATHAMA / HWAA  
 Work Order 2281-08-02  
 Date Rec'd.             
 RFW Contact N. Johnson M. Malle/m  
 Client Contact/Phone           

WA Use Only Lab ID	Client ID/Description
015	T-15 PB1 R1 Post Test
016	T-15 PB1 R2 Post Test
017	T-15 PB1 R3 Post Test
018	T-15 PB1 R4 Post Test
019	T-15 PB Field Blank Post Test
020	T-15 SHR1 R1 Post Test
021	T-15 SHR1 R2 Post Test
022	T-15 SHR1 R3 Post Test
023	T-15 SHR1 R4 Post Test
024	T-15 SHR1 Field Blank Post Test
025	T-15 CP Soil Post Test
026	T-15 CP Field Blank Post Test

Matrix: W - Water DS - Drum Solids Special Instructions: T-15 Post Test Samples  
 S - Soil O - Oil DL - Drum Liquids 600°F / 12 hrs.  
 SS - Sediment A - Air F - Fish  
 SO - Solid X - Other

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

WESTON Analytics Use Only
Samples Were: 1 Shipped or Hand-Delivered NOTES:
2 Ambient or Chilled NOTES:
3 Received Broken/Leaking (Impurity Sealed) Y N NOTES:
4 Properly Placed Y N NOTES:
5 Received Within Holding Time Y N NOTES:
COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:
COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:

# Custody Transfer Record/Lab Work Request



WESTON Analytics Use Only

8/26/14 / 01061257


2281-08-02

Date Rec'd. \_\_\_\_\_ Date Due \_\_\_\_\_

33FW Contact N. JOHANSEN, M. MAZEL 0810 006

**Client Contact/Phone:**

[illegible]

Refrigerator#	#Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED 	Date Collected
	W19				X
					X
					X
					X
					X

[illegible]

Matrix: W - Water D9 - Drum Solids  
 - Soil O - Oil DL - Drum Liquids  
 E - Sediment F - Fish  
 - Solid X - Other

Special Instructions: T-15 POST TEST SAMPLES  
 600°F/17 hrs

<b>WESTON Analytics</b>	
<b>Use Only</b>	
<b>Samples Were:</b>	
1 Shipped or Hand-Delivered	
<b>NOTES:</b>	
2 Ambient or Chilled	
<b>NOTES:</b>	
3 Received Broken/Leaking (Improperly Sealed)	Y N
<b>NOTES:</b>	
4 Properly Preserved	Y N
<b>NOTES:</b>	
5 Received Within Holding Times	Y N
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
<b>NOTES:</b>	
<b>COC Record Was:</b>	
1 Present Upon Receipt of Samples	Y N
Discrepancies Between Sample Labels and COC Record?	
	Y N
<b>NOTES:</b>	



## WESTON ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFW Batch 64/Dec 8/27/89 Analytical Lot \_\_\_\_\_ Units Rinsed MS/MS Wipe total MS, Seal MS/8  
 Installation FAWTHACHONE Date Prepared \_\_\_\_\_ Analyst \_\_\_\_\_  
 Matrix: Rinsed, Wipe, Seal Date Analyzed 5/27/89 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution, :

Comment: T-15 Post test Sample / Dec

MATRIX	R	R	W	W	S	S
LAB ID #	Rinsed Blank	10r Rinsed	Wipe Blank	10r Wipe	Seal Blank	Seal 10r
Dilution	1	1	1	1	1	1
Units	mg/ml	mg/ml	total mg	total mg	mg/g	mg/g
HMX	<0.533	98.24	<12.7	100%	<1.27	95.0
RDX	<0.49	88.61	<9.8	96.3	<0.98	82.4
1,3,5-TNB	<1.05	85.61	<20.9	88.0	<2.09	87.3
1,3-DNB	<0.295	87.01	<5.54	87.2	<0.589	88.5
HB	<0.210	87.6	<1.19	90.9	<0.419	89.7
Tetryl	<2.5	85.31	<50.0	88.6	<5.0	86.3
2,4,6-TNT	<0.96	78.21	<19.2	81.8	<1.92	80.9
2,6-DNT	<0.20	90.84	<4.0	93.8	<0.40	92.3
2,4-DNT	<0.21	79.61	<4.2	82.6	<0.42	81.1



## DATA SUMMARY

Units Ringier AG, Switzerland  
Analyst ALB  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution.**

comment: T15 Post Test Samples

[illegible]

**WESTON ANALYTICS EXPLOSIVES**

RFW Batch 5908-HC--029  
Installation WATERWONE  
Matrix: Rinsok, usipe, S211

Analytical Lot  
Date Prepared  
Date Analyzed

8	8r	is	'63	Leis
---	----	----	-----	------

Units Reside As/m, wife detain, Seil 46/8  
Analyst -AIS  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution, %**

**Comment:**

MATRIX	R		S		R		W		W		W	
LAB ID #	029-023	029-024	029-025	029-026	029-027	029-028	029-029	029-030	029-031	029-032	029-033	029-034
Sample Description	TIS SM	TIS SM	TIS CP	TIS	TIS SM	TIS SM	TIS Fresh	TIS Fresh	TIS Fresh	TIS Fresh	TIS Fresh	TIS Fresh
Dilution	RV	FICH BIK	50:1	FICH BIK	W1	FICH BIK	Chub with Wg	Chub with Bk	Chub with Bk	Chub with Bk	Chub with Bk	Chub with Bk
Sample Vol: $\mu$ l	300 ml	300 ml	17 ml	250 ml	—	—	—	—	—	—	—	—
Units	ug/ml	ug/ml	ug/gw	ug/ml	total ug	total ug	total ug	total ug	total ug	total ug	total ug	total ug
HMX	<0.635	<0.635	<1.27	<0.635	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7
RDX	<0.49	<0.49	<0.98	<0.49	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8
1,3,5-TNB	<1.05	<1.05	<2.09	<1.05	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9
1,3-DNB	<0.295	<0.295	<0.589	<0.295	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89	<5.89
NB	<0.210	<0.210	<0.419	<0.210	<4.19	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0
Tetryl	<2.5	<2.5	<5.0	<2.5	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0
2,4,6-TNT	<0.96	<0.96	<1.92	<0.96	1.3 J	1.2 J	1.9 J	1.9 J	1.9 J	1.9 J	1.9 J	1.9 J
2,6-DNT	<0.20	<0.20	<0.40	<0.20	<4.0	<4.0	<4.0	<4.0	<4.0	<4.0	<4.0	<4.0
2,4-DNT	<0.21	<0.21	<0.42	<0.21	1.7 J	1.4 J	1.6 J	1.6 J	1.6 J	1.6 J	1.6 J	1.6 J

20/10/88	Disc	12/5	12/8	8/27	12/5	12/3	12/8	8/27
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**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16,19,27, 8-1,5,10,16,20,22,29, 9-2,11,20

RFW #: 8907L058,059,154 8908L203,258,315,398,462,524,534,595  
8909L595,679,804

W.O. #: 2281-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

7/24/90  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2331-08-02-0000

WESTON BATCH #: 8908L462

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTIN LIMIT
-----	-----	-----	-----	-----	-----
-001	T14 SM W2 ETOH (POST	NITRATED ESTERS	5.0 u	UG	5.
-002	T14 FC WALLS W2 ETOH	NITRATED ESTERS	20.3	UG	5.
-003	T14 POST WIPE BLANK	NITRATED ESTERS	5.0 u	UG	5.
-004	T15 PRE SM W2 ETOH	NITRATED ESTERS	6.6	UG	5.
-005	T15 PRE WIPE BLANK	NITRATED ESTERS	5.0 u	UG	5.

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L462

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-----	-----	-----	-----	-----	-----
BLANK10	89LNC012-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC012-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5



ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L46

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC012-MB2	NITRATED ESTERS	95.2	97.6	2.5

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L462

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC012-MB1	NITRATED ESTERS	10.1	2.5 u	10.0	101
BLANK20	89LNC012-MB2	NITRATED ESTERS	47.6	2.5 u	50.0	95.2
		NITRATED ESTERS	48.8	2.5 u	50.0	97.6

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/21/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L53

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T15SMW2 POST TEST	NITRATED ESTERS	5.0	u UG	5
-002	T15SM FB POST TEST	NITRATED ESTERS	5.0	u UG	5
-003	T15 FLSH CHMB WALLW2	NITRATED ESTERS	7.9	UG	5
-004	T15 FLSH CHMB WALLBL	NITRATED ESTERS	5.0	u UG	5

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/21/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L534

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC012-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC012-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/21/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2201-08-02-0000

WESTON BATCH #: 8908L5:

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%REC
BLANK10	89LNC012-MB1	NITRATED ESTERS	10.1	2.5 u	10.0	10%
BLANK20	89LNC012-MB2	NITRATED ESTERS	47.6	2.5 u	50.0	95%
		NITRATED ESTERS	48.8	2.5 u	50.0	97%

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/21/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L534

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LHC012-MB2	NITRATED ESTERS	95.2	97.6	2.5

July 1990  
Revision: Final

TEST RUN 16  
600°F/6 HOURS

1311R2



# Custody Transfer Record/Lab Work Request

WESTON Analytica Use Only	
8908 HW-028	

Client USAF/AFM/AFM  
Work Order 2281-08-02  
Date Rec'd. 2281-08-02  
RFW Contact AFM/AFM, Johnson  
Client Contact/Phone \_\_\_\_\_

WA Use Only Lab ID	Client ID/Description
001	T16 SSR1 W1 TOP PRE
002	T16 SSR1 W2 TOP
003	T16 SSR1 W3 TOP
004	T16 SSR1 W4 TOP
005	T16 SSR1 W5 BOTTOM PRE
006	T16 SSR1 W6 BOTTOM PRE
007	T16 SSR1 W7 BOTTOM PRE
008	T16 SSR1 W8 BOTTOM PRE
009	T16 SSR2 W1 TOP PRE
010	T16 SSR2 W2
011	T16 SSR2 W3
012	T16 SSR2 W4

Matrix: V - Water D - Drum Solids  
S - Soil O - Oil CA - Drum Liquids  
SE - Sediment A - Air F - Fish  
SO - Solid X - Other

Special Instructions: T-16 PRE TEST SAMPLES

600°F/16 hr.

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

WESTON Analytica Use Only	
Samples Were: 1 Shipped or Hand-Delivered NOTES:	
2 Ambient or Chilled NOTES:	
3 Received Broken/Leaking (Improperly Sealed) Y N NOTES:	
4 Properly Preserved Y N NOTES:	
5 Received Within Holding Times Y N NOTES:	
COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:	
COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:	



# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only	
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Client CSATHAMA / HAWARD Date Rec'd 11/22/11 Date Due 11/22/11  
Work Order 228108-02 Client Contact/Phone 14221111

Client <u>CSATHAMA / HUWABO</u>		Refrigerators	
Work Order <u>228108-02</u>		#Type Container <u>60A</u>	
Date Rec'd. _____		Containers/Volume	
RFW Contact <u>MARCELIN JOHNSON</u>		Preservative	
Client Contact/Phone _____		ANALYSES REQUESTED <u>Explosive</u>	
WA Use Only	Client ID/Description	Matrix	Date Collected
Lab ID			
013	T16 SSR 2 W5 BATT PRE	WIPE	8/24/08
014	T16 SSR 2- W6 BATT PRE	WIPE	↓
015	T16 SSR 2 W7 BATT PRE	WIPE	↓
016	T16 SSR 2 W8 BATT PRE	WIPE	↓
017	T16 SSR FIELD BLANK	WIPE	8/24/08

Substr.: ☐ W. Water ☐ DS - Drum Solids ☐ Special Instructions: **T-16 PRE TEST SAMPLES**  
☐ O - Oil ☐ DL - Drum Liquids **600' F/6 hrs**  
☐ A - Air ☐ F - Fish  
☐ SS - Sediment ☐ X - Other

[illegible]

<b>WESTON Analytics</b>	
<b>Use Only</b>	
<b>Samples Were:</b>	
1 Shipped or Hand-Delivered	
<b>NOTES:</b>	
2 Ambient or Chilled	
<b>NOTES:</b>	
3 Received Broken/Leaking (Improperly Sealed)	Y N
<b>NOTES:</b>	
4 Properly Preserved	Y N
<b>NOTES:</b>	
5 Received Within Picking Times	Y N
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
<b>NOTES:</b>	
<b>COC Record Was:</b>	
1 Present Upon Receipt of Samples	Y N
<b>Discrepancies Between Sample Labels and COC Record?</b>	
	Y N
<b>NOTES:</b>	

WESTON Analytics Use Only	
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USATHAMA/HW 94P

Work Order 2281-08-02

Date Rec'd. \_\_\_\_\_ Date Due \_\_\_\_\_

NEW Contact N. Johnson

**Client: Contact/Phone:**

[illegible]

Matrix:	W - Water	DS - Drum Solids	Special Instructions:

T-16 PRE TEST SAMPLES

600°F/6 hr.

Matrix:	W - Water	DS - Drum Solids
S - Soil	O - Oil	DL - Drum Liquids
SE - Sediment	A - Air	F - Fish
SO - Solid		X - Other

[illegible]

<b>WESTON Analytics</b>	
<b>Use Only</b>	
<b>Samples Were:</b>	
1 Shipped or Hand-Delivered	
<b>NOTES:</b>	
<b>2 Ambient or Chilled</b>	
<b>NOTES:</b>	
<b>3 Received Broken/Leaking (Improperly Sealed)</b>	
Y N	
<b>NOTES:</b>	
<b>4 Properly Preserved</b>	
Y N	
<b>NOTES:</b>	
<b>5 Received Within Holding Times</b>	
Y H	
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
<b>NOTES:</b>	
<b>COC Record Was:</b>	
1 Present Upon Receipt of Samples	Y N
<b>Discrepancies Between Sample Labels and COC Record?</b>	
Y N	
<b>NOTES:</b>	





# WESTON ANALYTICALS EXPLOSIVES

## DATA SUMMARY

RFW Batch GA/QC 9/25/84 Analytical Lot \_\_\_\_\_ U. Its Rinsd/C-DE(m), wipe-telalag, soil 46/8  
 Installation LAQUINORISE Date Prepared \_\_\_\_\_ Analytic \_\_\_\_\_  
 Matrix: Rinsd/C, Wipe & Soil Date Analyzed 9/25/84 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution, \*

Comment: TIC Pre Test GA/QC 1

Matrix LAB ID #	R		W		S	
	Rinsd/C Blank	10x Rinsd/C	Wipe Blank	10x Wipe	Soil Blank	10x Soil
Dilution	1	1	1	1	1	1
Units	mg/ml	mg/ml	Total mg	Total mg	mg/g	mg/g
IMX	<0.635	6.55	<12.7	99.9	<1.27	98.4
RDX	<0.49	4.56	<9.8	98.7	<0.98	98.6
1,2,5-TNB	<1.05	9.6	<20.9	99.0	<2.09	98.1
1,3-DNB	<0.295	2.71	<5.89	98.1	<0.581	93.7
HB	<0.210	2.03	<4.19	94.7	<0.419	98.1
Tetryl	<2.5	22.2	<50.0	93.0	1.50	93.1
2,4,6-TNT	<0.96	7.65	<19.2	91.4	<1.92	90.6
2,6-DNT	<0.20	2.00	<4.0	90.5	<0.40	90.1
2,4-DNT	<0.21	1.90	<4.2	90.3	<0.42	90.8

# WESTON ANALYTICAL EXPLOSIVES

RFW Batch 8908-HU-028 -  
Installation - HAUSTHORNE  
Matrix: Rhinoc, w/pe, 9.5011

Analytical Lot  
Date Prepared  
Date Analyzed

Units <sup>Reviewed</sup>  
Analyst  
Reviewed

units Rinsdie-usia, wipe-ted at, still us/su

**Analyst \_\_\_\_\_**  
**Reviewed \_\_\_\_\_**

1875/5/15/508

**Note: Data is corrected for dilution, %**

Comment: T16 Pre-Test Samples !

[illegible]

(b5b1)  
(2500, 20/10)

## DATA SUMMARY

RFW Batch 8908 HJ-028-  
Installation HAWTHORNE  
Matrix: Rinsate, wipe, Soil

Analytical Lot \_\_\_\_\_  
Date Prepared \_\_\_\_\_  
Date Analyzed 5/25/89 8:26 PM

Units Rinsate-us/m, wipe-totals, soil us/Su  
Analyst -ALS  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution,**

comment: T-16 - Pre Test samples

MATRIX	R	S	R	R	R	R	R	R
LAB ID #	028- -028	029 -029	028 -028	028 -028	028 -028	028 -028	028 -028	028 -028
Sample Description	TIC PB Field BIK	TIG CP SI	Tig CP FIELD BK	TIGSSH SPIN	TIGSSH SPIN	TIGSSH SPIN	TIGSSH SPIN	TIGSSH SPIN
Dilution	1	10000	1	100	1000	100	1000	1000
Sample Vol/vol	250ml	1gm	250ml	30	30	30	30	30
Units	ug/ml	ug/gm	ug/ml	ug/ml	ug/ml	ug/ml	ug/ml	ug/ml
IHX	<0.635	<12700	<0.635	<62.5	<62.5	<62.5	<62.5	<62.5
RDX	<0.49	<9800	<0.49	<49	<49	<49	<49	<49
1,3,5-TNB	<1.05	<20900	<1.05	<105	<105	<105	<105	<105
1,3-DNE	<0.315	<5890	<0.315	<29.5	<29.5	<29.5	<29.5	<29.5
NB	<0.210	<4190	<0.210	<21	<21	<21.0	<21.0	<21.0
Tetryl	<2.5	<52000	<2.50	<250	<250	<250	<250	<250
2,4,6-TNT	<0.96	<195000	<0.96	<495	<495	<495	<495	<495
2,6-DNT	<0.20	<4000	<0.20	<20.0	<20.0	<20.0	<20.0	<20.0
2,4-DNT	<0.21	<4200	<0.21	<21	<21	<21.0	<21.0	<21.0



# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only

8908 HW 030 -

USATHAMA / HWIAP

2291-64-02

Date Due

N. Johnson / M. Mazelon

315-430-3117

WESTON Analytics Use Only		Samples Were:		1 Shipped or Hand-Delivered		NOTES:			
2 Ambient or Chilled		NOTES:		3 Received Broken/Leaking (Improperly Sealed)		Y N			
4 Properly Preserved		NOTES:		5 Received Within Holding Times		Y N			
COC Tape Was:		1 Present on Outer Package		Y N		2 Unbroken on Outer Package		Y N	
3 Present on Sample		Y N		4 Unbroken on Sample		Y N		NOTES:	
COC Record Was:		1 Present Upon Receipt of Sample		Y N		Discrepancies Between Sample Labels and COC Record?		Y N	
NOTES:									

Refrigerator#	#/Type Container	Containers/Volumes	Preservative	ANALYSES REQUESTED	Matrix	Date Collected	Client ID/Description	Lab ID	Item/Reason	Relinquished by	Received by	Date	Time
					ACN	9/31/99	Powder Box T16 P81 R1 Post R2	001					
							R3	002					
							R4	003					
							Field Blank	004					
							Heated Riser T16 SHW R1 Post R2	005					
							R3	006					
							R4	007					
							Field Blank	008					
							Support Rack T16 SSRIWI Post Wips W2	009					
							W3	010					
							W4	011					
							W5	012					
								013					
								014					
								015					

Matrix: W - Water D3 - Drum Solids DL - Drum Liquids S - Soil O - Oil F - Fish SE - Sediment A - Air X - Other SO - Solid

T16 POST-TEST 1 CHRS. @ 600°F



## Custody Transfer Record/Lab Work Request

WESTON Analyticals Use Only
8000-HW-030-

Client USATHAMA/HWAAPWork Order 2281-08-02Date Rec'd. 2/15/95RFW Contact N. Johnson / M. MazzolenClient Contact/Phone 215-430-3117

MA Use Only Lab ID	Client ID Description	Matrix	Date Collected	Refrigerator#	#Type Container	Containers/Volume	Preservative	ANALYSES REQUESTED	WESTON Analyticals Use Only
016	Support Rock T16 SHVIRI Post	Wipe	2/15/95						Samples Were: 1 Shipped or Hand-Delivered NOTES: 2 Ambient or Cooled NOTES: 3 Received Broken/Leaking (Improperly Sealed) Y N NOTES: 4 Properly Preserved Y N NOTES: 5 Received With/Holding Times Y N NOTES:
017	W7								
018	W9								
019	Field Blank								
020	Slay Pipe T16 CP Soil Post	Soil							
021	" " " Field Blank	ACN							COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:
022	Ship Mine T16 CM W1 Post	Wipe							
023	" " " Field Blank	"							
024	Heated Valve T16 SHVIRI Post	ACN							
025	R2								
026	R3								COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:
027	R4								
028	Field Blank								
029	Chamber Walls T16 W1 Post	Wipe							
030	" " " Field Blank								

Matrix: W - Water DS - Drum Solids Special Instructions:

S - Soil O - Oil DL - Drum Liquids

SE - Sediment A - Air F - Fish

SO - Solid X - Other

T16 Post-Test 6 HRS. @ 600°F

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

# DATA SUMMARY

## WESTON ANALYTICS EXPLOSIVES

RFW Batch QA/QC 9/1/89 Analytical Lot                      Units Remedial ml, wipe 100 ml, soil 100 ml  
 Installation WATERBURY Date Prepared                      Analyst                       
 Matrix:                      Date Analyzed 8/21/89 Reviewed                     

Note: Data is corrected for dilution, "

Comment: T16 - Post Test 600F @ 6hr / Or Samples

MATRIX	R	R	W	W	S	S
LAB ID #	Rinsate Blank	100 ml	wipe Blank	100 ml	soil Blank	100 ml
Dilution	1	1	1	1	1	1
Units	100 ml	100 ml	100 ml	100 ml	100 ml	100 ml
HMX	0.035	0.035	0.035	0.035	0.035	0.035
RDX	0.049	0.049	0.049	0.049	0.049	0.049
1,3,5-TNB	0.05	0.05	0.05	0.05	0.05	0.05
1,3-DNB	0.095	0.095	0.095	0.095	0.095	0.095
NB	0.210	0.210	0.210	0.210	0.210	0.210
Tetryl	0.25	0.25	0.25	0.25	0.25	0.25
2,4,6-TNT	0.096	0.096	0.096	0.096	0.096	0.096
2,6-DNT	0.020	0.020	0.020	0.020	0.020	0.020
2,4-DNT	0.021	0.021	0.021	0.021	0.021	0.021

## DATA SUMMARY

RFW Batch 9908 H10-C30  
Installation HAWTHORNE  
Matrix: Rinsate, wipe, soil  
Analytical Lot \_\_\_\_\_  
Date Prepared \_\_\_\_\_  
Date Analyzed 8/21/87, 9/11/89  
Units Rinsate, wipe, soil, soil wipe  
Analyst AJS  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution, %**

Comment: T16- Post Test 600°F @ 6 hour.

[illegible][illegible]

(1989).

## WESTON ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFW Batch 890340-020

Analytical Lot

Installation: Hawthorne

Date Prepared

Matrix: Rinse, wipe, soil

Date Analyzed

Units Rinse, wipe, soil, wipe total up, Soil up

Analyst

Reviewed

Note: Data is corrected for dilution.

Comment: TIC - Post Test Sample 600F @ 6 hours

MATRIX	LAB ID #	W	W	W	W	W	W	W	W	S	R	W
	020-012	020-013	020-014	020-015	020-016	020-017	020-018	020-019	020-020	020-021	020-022	
Sample Description	SR TIC SSRI W2	SR TIC SSRI W3	SR TIC SSRI W4	SR TIC SSRI W5	SR TIC SSRI W6	SR TIC SSRI W7	SR TIC SSRI W8	SR TIC SSRI W9	CP TIC CP Soil	CP TIC CP Soil	CP TIC CP Soil	SR TIC SSRI W1
Dilution	1	1	1	1	1	1	1	1	1	1	1	1
Sample Vol: $\mu$ l	—	—	—	—	—	—	—	—	19m	250	—	—
Units	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	ug/m	ug/m	Total ug	Total ug
HMX	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7	<1.27	<0.635	<12.7	<12.7
RDX	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8	<0.98	<0.49	<9.8	<9.8
1,3,5-TNB	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9	<2.09	<1.05	<20.9	<20.9
1,3-DNB	<5.90	<5.90	<5.90	<5.90	<5.90	<5.90	<5.90	<5.90	<0.59	<0.295	<5.90	<5.90
NB	<4.20	<4.2	<4.2	<4.2	<4.2	<4.2	<4.2	<4.2	<0.42	<0.210	<4.2	<4.2
Tetryl	<50.0	<50	<50	<50	<50	<50	<50	<50	<5.0	<2.5	<50	<50
2,4,6-TNT	8.7 J	10.3 J	8.6 J	8.7 J	13.2 J	10.3 J	10.2 J	12.3 J	<1.92	<0.96	7.6 J	<4.0
2,6-DNT	<4.0	<4.0	<4.0	<4.0	<4.0	<4.0	<4.0	<4.0	<0.40	<0.20	<4.0	<4.0
2,4-DNT	<4.2	<4.2	1.0 J	<4.2	<4.2	1.0 J	<4.2	1.0 J	<0.42	<0.21	2.3 J	<4.2

20/10/90 14/8 14/8 14/8 14/8 14/8 14/8 14/8 14/8 14/8 14/8 14/8 14/8

(1989)

# WESTON ANALYTICALS EXPLOSIVES

## DATA SUMMARY

RPM Batch 9908440-030

Analytical Lot

Installation HAUGHMORNE

Date Prepared

Matrix: Rinsate, wipe, Soil

Date Analyzed

Units Rinsate 159 ml, wipe 100 ug, Soil 159 gr

Analyst

Reviewed

Note: Data is corrected for dilution, '

Comment: T6.. Post Test Samples 600°F @ 6 hours

LAB ID	V3	R			R			R			W		
		030-023	030-024	030-025	030-026	030-027	030-028	030-029	030-030	030-031	030-032	030-033	030-034
Sample Description	SM TIC HV TIC SHV R1	SM TIC HV TIC SHV R2	SM TIC HV TIC SHV R3	SM TIC HV TIC SHV R4	SM TIC HV TIC SHV R5	SM TIC HV TIC SHV R6	SM TIC HV TIC SHV R7	SM TIC HV TIC SHV R8	SM TIC HV TIC SHV R9	SM TIC HV TIC SHV R10	SM TIC HV TIC SHV R11	SM TIC HV TIC SHV R12	SM TIC HV TIC SHV R13
Dilution	1	1	1	1	1	1	1	1	1	1	1	1	1
Sample Vol/Lot	(mls)	1000	1000	1000	1000	1000	250	---	---	---	---	---	---
Units	Total ug	ug/ml	ug/ml	ug/ml	ug/ml	ug/ml	ug/ml	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
INH	<12.7	<0.635	<0.635	<0.635	<0.635	<0.635	<0.635	<12.7	<12.7	<12.7	<12.7	<12.7	<12.7
RDX	<9.8	<0.49	<0.49	<0.49	<0.49	<0.49	<0.49	<9.8	<9.8	<9.8	<9.8	<9.8	<9.8
1,3,5-TNB	<20.9	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<20.9	<20.9	<20.9	<20.9	<20.9	<20.9
1,3-DNB	<5.90	<0.295	<0.295	<0.295	<0.295	<0.295	<0.295	<5.90	<5.90	<5.90	<5.90	<5.90	<5.90
NB	<4.20	<0.210	<0.210	<0.210	<0.210	<0.210	<0.210	<4.20	<4.20	<4.20	<4.20	<4.20	<4.20
Tetryl	<50.0	<2.50	<2.50	<2.50	<2.50	<2.50	<2.50	<50.0	<50.0	<50.0	<50.0	<50.0	<50.0
2,4,6-TNT	<10.5 J	<0.96	<0.96	<0.96	<0.96	<0.96	<0.96	<10.5 J	<10.5 J	<10.5 J	<10.5 J	<10.5 J	<10.5 J
2,6-DNT	<4.0	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<4.0	<4.0	<4.0	<4.0	<4.0	<4.0
2,4-DNT	<1.2 J	<0.21	<0.21	<0.21	<0.21	<0.21	<0.21	<1.2 J	<1.2 J	<1.2 J	<1.2 J	<1.2 J	<1.2 J

DATE: 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81 8/31/81

(1989)

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HWAAP  
RFW #: 8909L597 - RINSATES  
W.O. #: 2281-08-02

SAMPLES RECEIVED: 09-02-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02 modified for the analysis of rinsates.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

<u>Abbreviation</u>	<u>Description</u>
---------------------	--------------------

BLX	= Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.
-----	---

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS	= Designates sample spiked with target compound.
SSD	= Designates sample spiked with target compound in duplicate.
D	= Indicates duplicate analysis of a sample.
NS	= Not spiked.
DL	= Diluted below calibration range.
G	= Indicates elevated detection limit due to sample interference.
NR	= Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less Than  
> = Greater Than

Analysis Summary

Samples Collected: 08-31-89  
Samples Prepared: 09-07-89  
Samples Analyzed: 09-22-89

C. Zerk H. I.  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

10-13-89  
Date

WESTON ANALYTICS  
EXPLOSIVES IN RINSATE DATA SUMMARY

RFW Batch Number: 8909L597      CLIENT: USATHAMA HWAAP      Page: 1

Sample Information	T16SHV1		T16SHR1		T16PB1		2XSS	
	ID :	R1 DUP	ID :	R1 DUP	ID :	R1 DUP	BLANK	2XSS
	RFW#:	001	RFW#:	002	RFW#:	003		
	D.F.:	1	D.F.:	1	D.F.:	1		
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....	< 254	< 254	< 254	< 254	< 254	< 254	< 1.27	3.09(120t)
RDX.....	< 196	< 196	< 196	< 196	< 196	< 196	< 0.98	2.22(112t)
1,3,5-TNB.....	< 418	< 418	< 418	< 418	< 418	< 418	< 2.09	4.45(105t)
1,3-DNB.....	< 118	< 118	< 118	< 118	< 118	< 118	< 0.59	1.25(105t)
NITROBENZENE.....	< 84	< 84	< 84	< 84	< 84	< 84	< 0.42	0.84(99.2t)
TETRYL.....	< 1000	< 1000	< 1000	< 1000	< 1000	< 1000	< 5.00	7.18(71.1t)
2,4,6-TNT.....	< 384	< 384	< 384	< 384	< 384	< 384	< 1.92	3.95(75.8t)
2,6-DNT.....	< 80	< 80	< 80	< 80	< 80	< 80	< 0.40	0.88(108t)
2,4-DNT.....	< 84	< 84	< 84	< 84	< 84	< 84	< 0.42	0.87(103t)

Sample Information	10XSS		10XSSD	
	ID :	RFW#:	ID :	RFW#:
	D.F.:	1	D.F.:	1
Units:	Total ug	Total ug	Total ug	Total ug
HMX.....	15.2(118t)	15.2(117t)	15.0(117t)	15.0(117t)
RDX.....	10.9(111t)	10.7(109t)	10.7(109t)	10.7(109t)
1,3,5-TNB.....	22.2(105t)	22.1(105t)	22.1(105t)	22.1(105t)
1,3-DNB.....	6.20(105t)	6.22(105t)	6.22(105t)	6.22(105t)
NITROBENZENE.....	4.17(98.9t)	4.22(100t)	4.22(100t)	4.22(100t)
TETRYL.....	49.3(97.7t)	47.7(94.4t)	47.7(94.4t)	47.7(94.4t)
2,4,6-TNT.....	17.9(92.7t)	17.1(88.4t)	17.1(88.4t)	17.1(88.4t)
2,6-DNT.....	4.28(106t)	4.41(109t)	4.41(109t)	4.41(109t)
2,4-DNT.....	4.16(98.3t)	4.31(102t)	4.31(102t)	4.31(102t)

**WESTON**

ROY P. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16, 19, 27, 8-1, 5, 10, 16, 20, 22, 29, 9-2, 11, 20

RFW #: 8907L058, 059, 154 8908L203, 258, 315, 398, 462, 524, 534, 595  
8909L595, 679, 804

W.O. #: 2281-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

2/24/90  
Date



ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L524

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T16SMW2 PRE TEST	NITRATED ESTERS	5.0 u	UG	5.0
-002	T16SM WIPE RL PRTEST	NITRATED ESTERS	5.0 u	UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L52

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTI LIMIT
-----	-----	-----	-----	-----	-----
BLANK10	89LNC012-MB1	NITRATED ESTERS	2.5 u	MG/L	2
BLANK20	89LNC012-MB2	NITRATED ESTERS	2.5 u	MG/L	2 +

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L524

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC012-MB1	NITRATED ESTERS	10.1	2.5 u	10.0	101
BLANK20	89LNC012-MB2	NITRATED ESTERS	47.6	2.5 u	50.0	95.2
		NITRATED ESTERS	48.8	2.5 u	50.0	97.6

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-IWAA?  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8908L5

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC012-M32	NITRATED ESTERS	95.2	97.6	2.5

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8909L595

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-019	T16SMW1POST	NITRATED ESTERS	5.0 u	UG	5.0
-020	T16SM FIELD BLANK	NITRATED ESTERS	5.0 u	UG	5.0
-021	T16 CHAMBER WELL W1	NITRATED ESTERS	5.0 u	UG	5.0
-022	T16 CHAMBER WELL BLA	NITRATED ESTERS	5.0 u	UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8909L59

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORT LIMIT
-----	-----	-----	-----	-----	-----
BLANK10	89LNC012-MB1	NITRATED ESTERS	2.5 u	MG/L	2
BLANK20	89LNC012-MB2	NITRATED ESTERS	2.5 u	MG/L	2

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8909L595

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC012-MB1	NITRATED ESTERS	10.1	2.5 u	10.0	101
BLANK20	89LNC012-MB2	NITRATED ESTERS	47.6	2.5 u	50.0	95.2
		NITRATED ESTERS	49.8	2.5 u	50.0	97.6



ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8909L55

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC012-MB2	NITRATED ESTERS	95.2	97.6	2.5

July 1990  
Revision: Final

TEST RUN 17  
600°F/48 HOURS

1311R2

WESTON Analytics Use Only

8908-462031

# Custody Transfer Record/Lab Work Request



Client USATRIAMIA/HK/TAAP

Work Order 2481-08-02

Date Rec'd.                     

AFW Contact N. JOHNSON / M. MAZELON

Client Contact/Phone (215) 430-1117

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator #	#Type Container	Con:ainers/Volume	Preservative	ANALYSES REQUESTED
014	Aluminum Pipe TITAP R1	ACN	8/31/15					
015	R2							
016	R3							
017	R4							
018	TITAP2 R1							
019	R2							
020	R3							
021	R4							
022	TITAP Field Blank							
023	STED Pipe (2)							
024	TIT SPI R1							
025	R2							
026	R3							
027	R4							

Matrix: W - Water DS - Drum Solids Special Instructions:  
 S - Soil O - Oil DL - Drum Liquids  
 SE - Sediment A - Air F - Fish  
 SO - Solid X - Other

T17 Pre Test 600F @ 48 hours.

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

WESTON Analytics

Use Only

Samples Were:

1 Shipped or Hand-Delivered

NOTES:

2 Ambient or Chilled

NOTES:

3 Received Broken/Leaking (Improperly Sealed)

Y N

NOTES:

4 Properly Preserved

Y N

NOTES:

5 Received Within Holding Time

Y N

NOTES:

COC Tape Was:

1 Present on Outer Package Y N

2 Unbroken on Outer Package Y N

3 Present on Sample Y N

4 Unbroken on Sample Y N

NOTES:

COC Record Was:

1 Present Upon Receipt of Samples N

Discrepancies Between Sample Labels and COC Record?

Y N

NOTES:



## Custody Transfer Record/Lab Work Request

WESTON Analyticals Use Only
8002 HW-031

Client: USATHAMA/HWIAAF

Work Order: 3281-08-02

Date Rec'd: \_\_\_\_\_ Date Due: \_\_\_\_\_

RFW Contact: N. JOHNSON / M. MAZELON

Client Contact/Phone: (215) 430 3117

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected	Refrigerator/ #/Type Container	Containers/Volume Preservative	ANALYSES REQUESTED
032	Steam Heated RISKS	AEH	8/20/08			
033	T17 SHR R1					
034	R2					
035	R3					
036	R4					
037	T17 SHR R1					
038	R2					
039	R3					
040	R4					
041	T17 SHR Field Blank					
042	Steam Heated Valves T17 SHR R1					
043	R2					
044	R3					
045	R4					
046	T17 SHV Field Blank					

Matrix: W - Water D8 - Drum Solids Special Instructions:

S - Soil O - Oil DL - Urine Liquids

SE - Sediment A - Air F - Fish

SO - Sludge X - Other

T17 Pre Test 600F @ 48 hours.

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

<b>WESTON Analyticals Use Only</b> Samples Were: 1 Shipped or Hand-Delivered NOTES: 2 Ambient or Chilled NOTES: 3 Received Broken/Leaking (Improperly Sealed) Y N NOTES: 4 Properly Preserved Y N NOTES: 5 Received Within Holding Times Y N NOTES: COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES: COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record Y N NOTES:
--

WESTON Analytix Use Only

100-3  
100-3

2281-08-02

Date Rec'd. \_\_\_\_\_ Date Due \_\_\_\_\_

ARFW Contact M. Johnson, M. MAZELON

**Client Contact Phone -**

AWA Use Only Lab ID	Client ID/Description
046	T17 SHV2 R1 PREP
047	R2
048	R3
049	R4

Refrigerator#	Type Container	Containers/Vials	Preservative	ANALYSES REQUESTED
AAQ				Exp
			X	
			X	
			X	
			X	

### Special Instructions:

T17 PRETEST  
SAMPLES

Materials:	W - Water	DS - Drum Solids
S - Soil	O - Oil	DL - Drum Liquids
GE - Sediment	A - Air	F - Fish
NO - Solid		N - Char

[illegible]

<b>WESTON Analytics</b>	
<b>Use Only</b>	
<b>Samples Were:</b>	
1 Shipped or Hand-Delivered	
<b>NOTES:</b>	
<b>2 Ambient or Chilled</b>	
<b>NOTES:</b>	
<b>3 Received Broken/Leaking (improperly Sealed)</b>	
Y N	
<b>NOTES:</b>	
<b>4 Properly Preserved</b>	
Y N	
<b>NOTES:</b>	
<b>5 Received Within Holding Times</b>	
Y N	
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
1 Present on Outer Package	Y N
2 Unbroken on Outer Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
<b>NOTES:</b>	
<b>COC Record Was:</b>	
1 Present Upon Receipt of Samples	Y N
<b>Discrepancies Between Sample Labels and COC Record?</b>	Y N
<b>NOTES:</b>	

## NESTON ANALYTICAL EXPLOSIVES

RFW Batch QACe 9/1/89  
Installation HAUTHERNE  
Matrix: Rinsate

Analytical Lot \_\_\_\_\_  
Date Prepared \_\_\_\_\_  
Date Analyzed 9/1/89

Units Rinsate 45 ml  
Analyst ALS  
Reviewed \_\_\_\_\_

**Note: Data is corrected for dilution, %**

Comment: T17 Pre Test Sample / BC @ 600°F for 48 hrs.

LAB ID #	MATRIX		R		R	
	Blank	10X Rinse - Rinse	Blank	10X Rinse - Rinse	Blank	10X Rinse - Rinse
Dilution	1	1				
Knits	15 ml	15 ml				
HMX	<0.625	103%				
RDX	<0.49	103%				
1,3,5-TNB	<1.05	103%				
1,3-DNB	<0.215	103%				
NB	<0.210	103%				
Tetryl	<2.5	106%				
2,4,6-TNT	<0.96	103%				
2,6-DNT	<0.20	103%				
2,4-DNT	<0.21	98%				

**WESTON ANALYTICAL EXPLOSIVES**

RFW Batch 9908 401-031  
 Installation HAUTIERNE  
 Matrix: Rinsate

Analytical Lot	Units	Rinsate	ug/ml
Date Prepared	Analyst	-N/C	
Date Analyzed	Reviewed		

9/1/89

**Note: Data is corrected for dilution, %**

Comment: T17 Pre Test Samples 600°F @ 48 hours.

[illegible]



# WESTON ANALYTICS EXPLOSIVES DATA SUMMARY

RFW Batch 8908440 031 Analytical Lot Units Rinsalt us/m  
 Installation HAMMERNE Date Prepared Analyst  
 Matrix: Rinsalt Date Analyzed 9/1/89 Reviewed

Notes: Data is corrected for dilution.

Comment: T17 Pre Test Sample 600% @ 48 hours

MATRIX	R	R	R	R	R	R	R	R	R
LAB ID	031	031	031	031	031	031	031	031	031
Sample Description	032-035	036-039	040	041-044	045	046-049	050	051-054	055
Dilution	R1 → R4	R1 → R4	R1 → R4	R1 → R4	R1 → R4	R1 → R4	R1 → R4	R1 → R4	R1 → R4
Sample Vol. (ml)	1	1	1	1	1	1	1	1	1
Unit	us/m	us/m	us/m	us/m	us/m	us/m	us/m	us/m	us/m
HMX	<0.635	0.30J	<0.635	0.10J	<0.635	<0.635	<0.635	<0.635	<0.635
RDX	0.14J	2.71	<0.49	<0.49	<0.49	<0.49	<0.49	<0.49	<0.49
1,3,5-TNB	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05	<1.05
1,3-DNB	<0.205	<0.205	<0.205	<0.205	<0.205	<0.205	<0.205	<0.205	<0.205
NB	<0.21	<0.21	<0.21	<0.21	<0.21	<0.21	<0.21	<0.21	<0.21
Tetryl	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5	<2.5
2,4,6-TNT	<0.96	0.15J	<0.96	<0.96	<0.96	<0.96	<0.96	<0.96	<0.96
2,6-DNT	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20	<0.20
2,4-DNT	<0.21	<0.21	<0.21	2.64	<0.21	<0.21	1.77	<0.21	<0.21

OK/OK date 9/1/89 9/1/89 9/1/89  
 (1989)



ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HWAAP  
RFT #: 8909L679 - WIPES  
W.O. #: 2281-08-02

SAMPLES RECEIVED: 09-11-89

#### EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to U.S.G.S. methodology for picric acid.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

#### Abbreviation

#### Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

BS = Designates sample spiked with target compounds at 10x detection limit.  
BSD = Designates sample spiked with target compound in duplicate.  
D = Indicates duplicate analysis of a sample.  
NS = Not spiked.  
DL = Diluted below calibration range.  
G = Indicates elevated detection limit due to sample interference.  
NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

NOTE: Samples have been analyzed for picric acid and results converted mathematically to ammonium picrate.

NOTE: Spike recoveries for these analysis ranged from 18% to 38%. Reported detection limits take these low recoveries into account.

#### Data Qualifiers

< = Less Than and > = Greater Than

#### Analysis Summary

Samples Collected: 09-08-89  
Samples Prepared: 09-13-89  
Samples Analyzed: 09-29-89

Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

10-11-89  
Date

WESTON ANALYTICS  
EXPLOSIVES IN WIPE SAMPLES

RFW Batch Number: 8909L679

CLIENT: USATHAMA-HWAAP

Page: 1

Sample  
Information

Client T17FC  
ID : WALLS W1  
RFW#: 026  
D.F.: 1  
Units: Total ug

T17FC  
WALLS BLK  
G27  
1

BLANK  
1

BS 1  
1  
BS 2  
1  
BS 3  
1

Total ug Total ug Total ug

Ammonium Picrate..... < 10 < 10 9.3(113t) 45(110t) 41(99t)

**WESTON**ROY F. WESTON, INC.  
Lionville LaboratoryCLIENT: USATHAMA - HWAAP  
RFW #: 8909L679 - WIPES  
W.O. #: 2281-08-02

SAMPLES RECEIVED: 09-11-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to U.S.G.S. methodology for picric acid.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

<u>Abbreviation</u>	<u>Description</u>
---------------------	--------------------

BLK -	Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.
-------	---

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

BS -	Designates sample spiked with target compounds at 10x detection limit.
BSD -	Designates sample spiked with target compound in duplicate.
D -	Indicates duplicate analysis of a sample.
NS -	Not spiked.
DL -	Diluted below calibration range.
G -	Indicates elevated detection limit due to sample interference.
NR -	Not reported.

NOTE: Spikes have been reported as result (% recovery).

NOTE: Samples have been analyzed for picric acid and results converted mathematically to ammonium picrate.

NOTE: Spike recoveries for these analysis ranged from 18% to 38%. Reported detection limits take these low recoveries into account.

Data Qualifiers

< = Less Than and > = Greater Than

Analysis SummarySamples Collected: 09-08-89  
Samples Prepared: 09-13-89  
Samples Analyzed: 09-29-89

Chuck Hill  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

10-13-89  
Date

WESTON ANALYTICS  
EXPLOSIVES IN RINSATES DATA SUMMARY

RFW Batch Number: 8909L679

CLIENT: USATHAMA-HWAAP

Page: 1

Sample Information	Client	T17PB1R1	T17PB1R2	T17PB1R3	T17PB1R4	T17PB	T17SHV1R
ID :	POST TEST	POST TEST	POST TEST	POST TEST	POST TEST	FIELD BL	1PSTTEST
RFW#:	001	002	003	004	005		006
D.F.:	1	1	1	1	1		1
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug

Ammonium Picrate..... < 10 < 10 < 10 < 10 < 10 < 10

Sample Information	Client	T17SHV1R2	T17SHV1R3	T17SHV1R4	T17SHV	T17SHR1R1	T17SHR1R
ID :	POST TEST	POST TEST	POST TEST	POST TEST	FIELD BLK	POST TEST	2PSTTEST
RFW#:	007	008	009	010	011	012	
D.F.:	1	1	1	1	1	1	1
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug

Ammonium Picrate..... < 10 < 10 < 10 < 10 < 10 < 10

Sample Information	Client	T17SHR1R3	T17SHR1R4	T17SHR	T17AP1	T17AP1	T17AP1
ID :	POST TEST	POST TEST	POST TEST	FIELD BLK	R1	R2	R3
RFW#:	013	014	015	016	017	018	
D.F.:	1	1	1	1	1	1	1
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug

Ammonium Picrate..... < 10 < 10 < 10 < 10 < 10 < 10

WESTON ANALYTICS  
EXPLOSIVES IN RINSATES DATA SUMMARY

RFW Batch Number: 8909L679

CLIENT: USATHAMA-HWAAP

Page: 2

Sample Information	Client	T17AP1	T17AP	T17SP1R1	T17SP1R2	T17SP1R3	T17SP1R4
ID :	R4		FIELD BLK	POST TEST	POST TEST	POST TEST	POSTTEST
RFW#:	019	020		021	022	023	024
D.F.:	1	1		1	1	1	1
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug

Ammonium Picrate..... < 10 < 10 < 10 < 10 < 10

Sample Information	Client	T17SP	858	858	858	858	857
ID :	FIELD BLK		BLANK	BS1	BS2	BS3	BLANK
RFW#:	025			1	1	1	1
D.F.:	1						
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug

Ammonium Picrate..... < 10 < 10 < 2.4(30t) 7.3(18t) 10.4(25t) < 10

Sample Information	Client	857	857	857	857	857	857
ID :	857		BS1	BS2	BS3	BS3	BS3
RFW#:	1		1	1	1	1	1
D.F.:	1						
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug

Ammonium Picrate..... 3.1(38t) 12.6(31t) 13.1(32t)

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HWAAP  
RTW #: 8909L595 - RINSATES  
W.O. #: 2281-08-02

SAMPLES RECEIVED: 09-02-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02 modified for the analysis of rinsates.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

BS = Designates sample spiked with target compound.  
BSD = Designates sample spiked with target compound in duplicate.  
D = Indicates duplicate analysis of a sample.  
NS = Not spiked.  
DL = Diluted below calibration range.  
G = Indicates elevated detection limit due to sample interference.  
NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

NOTE: Samples have been analyzed for picric acid and results converted mathematically to ammonium picrate.

NOTE: Spike recoveries for these analysis ranged from 18% to 29%. Reported detection limits take these low recoveries into account.

Data Qualifiers

< = Less Than and > = Greater Than

Analysis Summary

Samples Collected: 08-30-89  
Samples Prepared: 09-06-89  
Samples Analyzed: 09-29-89

Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

10-13-89  
Date

WESTON ANALYTICS  
EXPLOSIVES IN RINSATES DATA SUMMARY

RFW Batch Number: 8909L595

CLIENT: USATHAHA-HWAAP

Page: 1

Sample  
Information

Client	T17SHR1	T17SHV1	---			---		
ID :	WR	WR1						
RFW#:	001	010	BLANK	BS 1	BS 2	BS 3		
D.F.:	1	100	1	1	1	1		
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug		

Ammonium Picrte..... < 10 25.1 < 10.0 1.5(18t) 12.1(29t) 12.0(29t)



July 1980  
Revision: Final

TEST RUN 18  
300°Y/6 HOURS

1311R2



# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only	
8909HW 032	

Client USATAMA / HAWAII  
Work Order 2281-08-02  
Date Rec'd. 2/28/08  
RFW Contact N. JOHNSON / MIKE MARZULLA  
Client Contact/Phone \_\_\_\_\_

WA Use Only Lab ID	Client ID/Description	Matrix	Date Collected
001	T18 PB1 R1 PRE TEST	AG	9/6/89
002	R2		X
003	R3		X
004	R4		X
005	T18 PB FIELD Blank PRE TEST		X
006	T18 PB2 R1 PRE TEST		X
007	R2		X
008	R3		X
009	R4	AG	9/6/89
010			
011	T18 CP Soil PRE TEST	S	9/6/89
012	T18 CP Field Blank	AG	9/6/89
013			

Matrix: W - Water DS - Drum Solids X - Other  
G - Oil DL - Drum Liquids  
SE - Sediment A - Air F - Fish  
SO - Solid WI - Wipe L - EP/CLP Leachate

Item/Function	Relinquished by	Received by	Date	Time	Item/Function	Relinquished by	Received by	Date	Time

WESTON Analytics Use Only	
Samples Were: 1 Shipped or Hand-Delivered NOTES:	
2 Ambient or Chilled NOTES:	
3 Received Broken/ Leaking (Improperly Sealed) Y N NOTES:	
4 Properly Preserved Y N NOTES:	
5 Received Within Holding Times Y N NOTES:	
COC Tape Was: 1 Present on Outer Package Y N 2 Unbroken on Outer Package Y N 3 Present on Sample Y N 4 Unbroken on Sample Y N NOTES:	
COC Record Was: 1 Present Upon Receipt of Samples Y N Discrepancies Between Sample Labels and COC Record? Y N NOTES:	

Special Instructions: T-18 PRE TEST SAMPLES  
500°F/6hr

EXP = EXPOSIVES

1053

WESTCO Analytics Use Only

8909 HWS-032

# Custody Transfer Record/Lab Work Request

WESTCO ANALYTICS

Client USATHINKA / HANAMP

Work Order 2281-08-02

Lab Rec'd. 2281-08-02

RFW Contact M. Johnson / M. Johnson

Client Contact/Phone

Lab ID	Client ID/Description	Matrix	Date Collected
012	T185521 W1 PRE-TEST	W1	9/14/19
013	W2		
014	W3		
015	W4		
016	W5		
017	W6		
018	W7		
019	W8		
020	T185521 FIELD BLANK	W1	9/14/19

Special Instructions: T-18 PRE TEST SAMPLES  
500°F / 6hr.

Item/Ref	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

Use Only

Samples Were:

1 Shipped or Hand-Delivered

NOTES:

2 At Night or Chilled

NOTES:

3 Received Broken/Leaking (Improperly Sealed)

Y N

NOTES:

4 Properly Preserved

Y N

NOTES:

5 Received Within Holding Times

Y N

NOTES:

COC Type Was:

1 Present on Outer Package Y N

2 Unbroken on Outer Package Y N

3 Present on Sample Y N

4 Unbroken on Sample Y N

NOTES:

COC Record Was:

1 Present Upon Receipt of Samples Y N

Discrepancies Between Sample Labels and COC Record? Y N

NOTES:

# Custody Transfer Record/Lab Work Request

WESTON Analytics Use Only  
750 977 6918

УСТАНАВА: НУНАР

2281-03-02

**Work Order** \_\_\_\_\_ **Date Rec'd.** \_\_\_\_\_ **Date Due** \_\_\_\_\_

RFW Contact N. Johnson / M. Mize

**Client Contact/Phone:**

Client ID/Description	WA Use Only

LAB ID	T185582	W1	TOP	PR: ET	WIRE	COLLECTED
023A9		W2				X
024DE		W3				X
02501E		W4	↓			X
026		W5 BOTTOM				X
027		W6				X
028		W7				X
029		W8	↓			X

Special Instructions: F-18 PRE-TEST SAMPLES  
500°F/16 hr.

Matrix:	W - Water	DS - Drum Solids	X - Other
O - Oil	O - Oil	DL - Drum Liquids	
E - Sediment	A - Air	F - Fish	
O - Solid	W1 - Wipe	L - EPICLIP Leachate	

[illegible]

<b>WESTON Analytics</b>	
<b>Use Only</b>	
<b>Samples Were:</b>	
1 Shipped or Hand-Delivered	
<b>NOTES:</b>	
<b>2 Ambient or Chilled</b>	
<b>NOTES:</b>	
<b>3 Received Broken/Leaking (Improperly Sealed)</b>	
Y N	
<b>NOTES:</b>	
<b>4 Properly Preserved</b>	
Y N	
<b>NOTES:</b>	
<b>5 Received Within Holding Times</b>	
Y N	
<b>NOTES:</b>	
<b>COC Tape Was:</b>	
1 Present on Outlets Package	Y N
2 Unbroken on Outlier Package	Y N
3 Present on Sample	Y N
4 Unbroken on Sample	Y N
<b>NOTES:</b>	
<b>COC Record Was:</b>	
1 Present Upon Receipt of Samples	Y N
<b>Discrepancies Between Sample Labels and COC Record?</b>	
Y N	
<b>NOTES:</b>	





# WESTON ANALYTICALS EXPLOSIVES

## DATA SUMMARY

REF: Batch 04/02 9/6/89  
 Installation HAWSHATCH  
 Matrix: Risole, Wipe, Soil

Analytical Lot  
 Date Prepared  
 Date Analyzed 9/6/89

Units Risole 45/100, Wipe 100/100, Soil 100/100  
 Analyst  
 Reviewed

Note: Data is corrected for dilution.

Comment: T-18 Pre-Test Samples 500°F @ 6 hours / On/Off Set 1

Matrix LAB ID #	R		W		S		S	
	Blank Risque	10X Risque	Blank Wipe	10X Wipe	Blank Soil	10X Soil	Blank Soil	10X Soil
Dilution	1	1	1	1	1	1	1	1
Units	45/100	45/100	45/100	45/100	45/100	45/100	45/100	45/100
10X	<0.635	6.7	<12.7	145	<1.27	127	<1.27	127
RDX	<0.49	5.1	<9.8	110	<0.98	921	<0.98	921
1,3,5-TNB	<1.05	11.0	<20.9	240	<2.09	211	<2.09	211
1,3-DNB	<0.295	3.04	<5.90	558	<0.59	570	<0.59	570
NB	<0.210	2.13	<4.20	42.9	<0.42	3.70	<0.42	3.70
Tetryl	<2.5	25.7	<50.0	562	<5.0	49.1	<5.0	49.1
2,4,6-TNT	<0.96	9.75	<19.2	214	<1.92	18.1	<1.92	18.1
2,6-DNT	<0.20	2.1	<4.0	45.1	<0.40	3.42	<0.40	3.42
2,4-DNT	<0.21	2.19	<4.20	47.1	<0.42	3.50	<0.42	3.50

WESTON ANALYTICS USE ONLY

8909440 033

Client WATKINS/DAVID

Work Order 2281-08-02

Date Rec'd.                      Date Due                     

AFW Contact M. Thomas/M. MAZELRA

Client Contact/Phone                     

WA Use Only Lab ID	Client ID/Description
001	TIB SM HILL PR-TEST
002	TIB SM FIELD Blank
003	TIB SSRI SPIKE Rinsate
004	TIB SSR2 SPIKE Rinsate

Matrix: W - Water DS - Drum Solids  
S - Soil O - Oil DL - Drum Liquids  
SE - Sediment A - Air F - Fish  
SO - Solid X - Other

Special Instructions:

T-18 RE TEST SAMPLES  
500°F/GHR.

Item/Reason	Relinquished by	Received by	Date	Time	Item/Reason	Relinquished by	Received by	Date	Time

AFW 21-21-001/A-5/03

EXP = EXPOSURES

7-115

WESTON ANALYTICS

Use Only

Samples Were:  
1 Shipped or Hand-Delivered

NOTES:

2 Ambient or Chilled  
NOTES:

3 Received Broken/  
Leaking (Improperly Sealed)  
Y N

NOTES:

4 Properly Preserved  
Y N

NOTES:

5 Received Within  
Holding Times  
Y N

NOTES:

COC Tape Was:

1 Present on Outer  
Package Y N

2 Unbroken on Outer  
Package Y N

3 Present on Sample  
Y N

4 Unbroken on Sample  
Y N

NOTES:

COC Record Was:

1 Present Upon Receipt  
of Samples Y N

Discrepancies Between  
Sample Labels and COC  
Record? Y N

NOTES:



## WESTON ANALYTICALS EXPLOSIVES

DATA SUMMARY

REF Batch QA/SC 9/7/89

Installation HANNAH/SC

Matrix: Rinsate, Wipe

Analytical Lot

Date Prepared

Date Analyzed 9/7/89

Units Rinsate, Wipe, Analyte

Analyst

Reviewed

Notes: Data is corrected for dilution.

Comment: T-18 Pre Test Samples QC 500f @ 6 hours

MATRIX	R	R	W	W
LAB ID	Blank Rinsate	Blank Wipe	Blank Wipe	Blank Wipe
Dilution	1	1	1	1
Units	mg/L	mg/L	mg/L	mg/L
HDX	<0.635	1.35	11.7	15.4
RDX	<0.49	5.35	19.8	15.0
1,3,5-TNB	<1.05	11.5	20.9	16.5
1,3-DNB	<0.295	2.11	5.90	7.47
HB	<0.210	1.2	4.20	45.37
Tetryl	<2.50	35.1	50.0	356
2,4,6-TNB	<0.96	8.65	19.2	120
2,6-DNT	<0.20	2.18	4.0	30.2
2,4-DNT	<0.21	2.02	4.20	27.9

# MISSION ANALYTICS EXPLOSIVES

## DATA SUMMARY

RFW Batch 8409 HW-033 Analytical Lot \_\_\_\_\_ Units 24.5 µS/ml, wipe Total of \_\_\_\_\_  
 Installation HUMMER Date Prepared \_\_\_\_\_ Analyst AS  
 Matrix: Kiesel, wipe Date Analyzed 9/7/89 Reviewed \_\_\_\_\_

Note: Data is corrected for dilution.

Comment: T-18 Pre Test Sample 500°F @ 6 hours

LAB ID #	W		U		R	
	033	033	033	033	033	033
Sample Description	001	001	001	002	003	004
Dilution	1	10	1000	1	100	100
Sample Vol. ml						
Units	Total µg	Total µg	Total µg	Total µg	µS/ml	µS/ml
HMX	4430	4430	4430	4430	4430	4430
RDX			29300	29300	29300	29300
1,3,5-TNB	30.5	30.5	30.5	30.5	30.5	30.5
1,3-DNB	5.90	5.90	5.90	5.90	5.90	5.90
NB	21.1	21.1	21.1	21.1	21.1	21.1
Tetryl	59.0	59.0	59.0	59.0	59.0	59.0
2,4,6-TNT			4920	4920	4920	4920
2,6-DNT	4.0	4.0	4.0	4.0	4.0	4.0
2,4-DNT	39.1	39.1	39.1	39.1	39.1	39.1

9/7/89 (1989) - 9/7 9/7 9/7 9/7 9/7 9/7

**WESTEN**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HWAAP  
RTV #: 8909L304 - WIPES  
T.O. #: 2231-08-02

SAMPLES RECEIVED: 09-20-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02. Explosives in Soil, modified for the analysis of wipe samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

<u>Abbreviation</u>	<u>Description</u>
---------------------	--------------------

BLX	= Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.
-----	---

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

33	= Designates sample spiked with target compound.
3SD	= Designates sample spiked with target compound in duplicate.
D	= Indicates duplicate analysis of a sample.
NS	= Not spiked.
DL	= Diluted below calibration range.
G	= Indicates elevated detection limit due to sample interference.
NR	= Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less Than  
> = Greater Than

Analysis Summary

Samples Collected: 09-18-89  
Samples Prepared: 09-22-89  
Samples Analyzed: 09-22-89

*for Robert H. J.*  
Cartar Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

*10-12-89*  
Date

**CLIENT: USATHAMA-HWAP**

பெயர்: 1

Sample Information	Client ID :		T18FC WALLS W1	T18FC WALLS BL	T18SSR1 W1 TOP	T18SSR1 W2	T18SSR1 W3	T18SSR1 W4
	RFW#:	D.F.:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
	005	1	< 12.7	< 9.80	< 12.7	< 12.7	< 12.7	< 12.7
HMX.....			< 9.80	< 9.80	< 9.80	< 9.80	< 9.80	< 9.80
RDX.....			< 20.9	< 20.9	< 20.9	< 20.9	< 20.9	< 20.9
1,3,5-TNB.....			< 5.90	< 5.90	< 5.90	< 5.90	< 5.90	< 5.90
1,3-DNB.....			< 4.20	< 4.20	< 23.8G	< 14.5G	< 6.72G	< 6.41G
NITROBENZENE.....			< 50.0	< 50.0	< 50.0	< 50.0	< 50.0	< 50.0
TETRYL.....			< 19.2	< 19.2	< 19.2	< 19.2	< 19.2	< 19.2
2,4,6-TNT.....			< 4.00	< 4.00	< 4.00	< 4.00	< 4.00	< 4.00
2,6-DNT.....			< 4.20	< 4.20	< 4.20	< 4.20	< 4.20	< 4.20
2,4-DNT.....								

[illegible]

# WESTON ANALYTICS EXPLOSIVES IN HIPE SAMPLES DATA SUMMARY

RFW Batch Number: 8909L804

CLIENT: USATHAMA-HWAAP

Page: 2

Sample Information	Client		T18SM		---		---		---	
	ID :	FIELD BL	017		BLANK		2XSS		10XSS	
	RFW#:		1		1		1		1	
	D.F.:		1		1		1		1	
	Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....		< 12.7	< 1.27	< 1.27	1.91(74.2%)	1.91(74.2%)	9.37(73.1%)	9.37(73.1%)		
RDX.....		< 9.80	< 9.80	< 9.80	1.62(81.6%)	1.62(81.6%)	7.68(77.7%)	7.68(77.7%)		
1,3,5-TNB.....		39.6	< 2.09	< 2.09	3.19(75.2%)	3.19(75.2%)	16.4(77.4%)	16.4(77.4%)		
1,3-DNB.....		< 5.90	< 0.59	< 0.59	0.98(82.2%)	0.98(82.2%)	4.84(82.5%)	4.84(82.5%)		
NITROBENZENE.....		< 4.20	< 0.42	< 0.42	0.74(87.7%)	0.74(87.7%)	3.69(87.7%)	3.69(87.7%)		
TETRYL.....		< 50.0	< 5.00	< 5.00	6.82(67.6%)	6.82(67.6%)	37.1(73.4%)	37.1(73.4%)		
2,4,6-TNT.....		< 19.2	< 1.92	< 1.92	3.25(83.6%)	3.25(83.6%)	14.8(76.3%)	14.8(76.3%)		
2,6-DNT.....		< 4.00	< 0.40	< 0.40	0.59(72.9%)	0.59(72.9%)	2.95(73.1%)	2.95(73.1%)		
2,4-DNT.....		< 4.20	< 0.42	< 0.42	0.68(80.7%)	0.68(80.7%)	3.42(80.9%)	3.42(80.9%)		

Sample Information	Client		---		---		---		---	
	ID :	FIELD BL	017		BLANK		2XSS		10XSS	
	RFW#:		1		1		1		1	
	D.F.:		1		1		1		1	
	Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....		8.14(63.5%)								
RDX.....		6.94(70.2%)								
1,3,5-TNB.....		14.8(70.0%)								
1,3-DNB.....		4.44(74.9%)								
NITROBENZENE.....		3.47(82.2%)								
TETRYL.....		30.9(61.2%)								
2,4,6-TNT.....		13.1(67.6%)								
2,6-DNT.....		2.75(68.4%)								
2,4-DNT.....		3.10(73.2%)								

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HWAAP  
RPT #: 8909L803 - RINSATES  
W.O. #: 2281-08-02

SAMPLES RECEIVED: 09-20-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of rinsates.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation                      Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.  
SSD = Designates sample spiked with target compound in duplicate.  
D = Indicates duplicate analysis of a sample.  
NS = Not spiked.  
DL = Diluted below calibration range.  
G = Indicates elevated detection limit due to sample interference.  
NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less Than  
> = Greater Than

Analysis Summary

Samples Collected: 09-18-89  
Samples Prepared: 09-22-89  
Samples Analyzed: 09-22-89

Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

10-13-89  
Date



**AKW Batch Number: 89091803**

**CLIENT: USATHANK FWAAP**

232

Sample Information		Client		10XSS		2XSS		10XSS	
ID :	RPW#:	BLANK	1	Total ug	Total ug	1	Total ug	1	Total ug
D.F.:	Units:	1	Total ug	Total ug	Total ug	1	Total ug	1	Total ug
IRMX.....	<	1.27	2.31 (89.7%)	11.1 (86.4%)					
KDX.....	<	0.98	1.89 (95.1%)	8.74 (88.4%)					
1,3,5-TNB.....	<	2.09	3.63 (85.6%)	18.7 (88.6%)					
1,3-DNB.....	<	0.59	1.10 (92.4%)	5.44 (91.7%)					
NITROBENZENE.....	<	0.42	0.83 (97.6%)	4.11 (97.4%)					
PETRYL.....	<	5.00	8.35 (82.7%)	44.8 (88.8%)					
2,4,6-TNT.....	<	1.92	3.77 (97.1%)	17.6 (90.8%)					
2,6-DNT.....	<	0.40	0.68 (83.4%)	3.42 (84.9%)					
2,4-DNT.....	<	0.42	0.70 (91.9%)	3.97 (93.8%)					

Sample Information	Client ID	RFW#	D.F.	Units	Total ug
HEX	10.4	(81.1%)			
RDZ	8.19	(82.9%)			
1,3,5-TNB	17.6	(83.1%)			
1,3-DNB	5.15	(86.8%)			
NITROBENZENE	3.97	(94.0%)			
TETRYL	41.6	(82.3%)			
2,4,6-TNT	16.4	(84.7%)			
2,6-DNT	3.29	(81.5%)			
2,4-DNT	3.77	(84.0%)			



**WESTERN**

ROY P. NULTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HWAAP  
API #: 8909L303 - SOIL  
M.O. #: 2231-08-02

SAMPLES RECEIVED: 09-20-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLX = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.

ECD = Designates sample spiked with target compound in duplicate.

D = Indicates duplicate analysis of a sample.

NS = Not spiked.

DL = Diluted below calibration range.

G = Indicates elevated detection limit due to sample interference.

NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less Than

> = Greater Than

Analysis Summary

Samples Collected: 09-18-89

Samples Prepared: 09-22-89

Samples Analyzed: 09-22-89

*C. Z. Nulton*  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

*10-13-89*  
Date

# WESTON ANALYTICS EXPLOSIVES IN SOIL DATA SUMMARY

RFW Batch Number: 89091303

CLIENT: USA/HADA-HWAAP

Page: 2

Sample Information	Client		T19CP		BLANK		2XSS		10XSS	
	ID :	SOLID	RFW#:	001	1	1	1	1	1	1
	D.F.:	1	Units:	ag/g	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....	<	1.27	<	1.27	<	1.27	2.88(113%)	11.8(92.8%)		
RDX.....	<	0.98	<	0.98	<	0.98	2.13(111%)	8.89(90.7%)		
1,3,5-TNB.....	<	2.09	<	2.09	<	2.09	4.58(110%)	20.4(97.5%)		
1,3-DNB.....	<	0.59	<	0.59	<	0.59	1.36(115%)	5.85(99.3%)		
NITROBENZENE.....	<	0.42	<	0.42	<	0.42	0.92(110%)	4.12(98.4%)		
TETRYL.....	<	5.00	<	5.00	<	5.00	11.3(113%)	48.8(97.5%)		
2,4,6-TNT.....	<	1.92	<	1.92	<	1.92	4.63(120%)	15.6(97.1%)		
2,6-DNT.....	<	0.40	<	0.40	<	0.40	0.90(112%)	3.91(97.7%)		
2,4-DNT.....	<	0.42	<	0.42	<	0.42	0.94(112%)	4.11(97.8%)		

Sample Information	Client		T19CP		BLANK		2XSS		10XSS	
	ID :	SOLID	RFW#:	001	1	1	1	1	1	1
	D.F.:	1	Units:	ag/g	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....	<	1.27	<	1.27	<	1.27	2.88(113%)	11.8(92.8%)		
RDX.....	<	0.98	<	0.98	<	0.98	2.13(111%)	8.89(90.7%)		
1,3,5-TNB.....	<	2.09	<	2.09	<	2.09	4.58(110%)	20.4(97.5%)		
1,3-DNB.....	<	0.59	<	0.59	<	0.59	1.36(115%)	5.85(99.3%)		
NITROBENZENE.....	<	0.42	<	0.42	<	0.42	0.92(110%)	4.12(98.4%)		
TETRYL.....	<	5.00	<	5.00	<	5.00	11.3(113%)	48.8(97.5%)		
2,4,6-TNT.....	<	1.92	<	1.92	<	1.92	4.63(120%)	15.6(97.1%)		
2,6-DNT.....	<	0.40	<	0.40	<	0.40	0.90(112%)	3.91(97.7%)		
2,4-DNT.....	<	0.42	<	0.42	<	0.42	0.94(112%)	4.11(97.8%)		

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HAWTHORNE      SAMPLES RECEIVED: 09-22-89  
REF #: 3909L351, RINSATES  
D.O. #: 2281-03-02

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, modified for the analysis of rinsates.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

<u>Abbreviation</u>	<u>Description</u>
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BLK =	Reagent blank analyzed to provide an indication of lab contamination and its effect on reported analytical data.
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Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS =	Designates sample spiked with target compound.
SSD =	Designates sample spiked with target compound in duplicate.
D =	Indicates duplicate analysis of a sample.
NS =	Not spiked.
DL =	Diluted below calibration range.
G =	Indicates elevated detection limit due to sample interference.
NR =	Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less Than      > = Greater Than

Analysis Summary

Samples Collected: 09-20-89  
Samples Prepared: 09-26-89  
Samples Analyzed: 10-24-89

Carter Nulton (R)  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

10/29  
Date

WESTON ANALYTICS  
EXPLOSIVES IN KINSATE DATA SUMMARY

RPM Batch Number: 8909L851 CLIENT: USATHAMA-HAWTHORNE Page: 1

Sample Information	Client		T18 MOTOR		2X'S		10XSS	
	ID :	SOAK TEST	001	1	Total ug	Total ug	Total ug	Total ug
	RPM#:							
	D.F.:	1400						
	Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....	<	220	2.43(94.4%)			13.1(102%)		
RDX.....	<	170	1.82(92.0%)			10.1(102%)		
1,3,5-TNB.....	<	370	4.02(94.8%)			21.6(102%)		
1,3-DNB.....	<	100	1.14(95.8%)			6.05(102%)		
Nitrobenzene.....	<	74	0.79(94.5%)			4.35(103%)		
Tetryl.....	<	880	6.47(64.0%)			46.4(91.9%)		
2,4,6-TNT.....	<	340	2.72(69.9%)			17.4(89.9%)		
2,6-DNT.....	<	70	0.85(106%)			4.24(105%)		
2,4-DNT.....	<	70	0.82(96.4%)			4.34(103%)		

Sample Information	Client		10XSSD		BLANK	
	ID :	1	Total ug	Total ug	Total ug	Total ug
	RPM#:					
	D.F.:					
	Units:	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....		12.5(97.2%)	<	1.27		
RDX.....		9.74(98.6%)	<	0.98		
1,3,5-TNB.....		21.1(99.6%)	<	2.09		
1,3-DNB.....		5.90(99.5%)	<	0.59		
Nitrobenzene.....		4.25(101%)	<	0.42		
Tetryl.....		42.8(84.8%)	<	5.00		
2,4,6-TNT.....		15.5(79.9%)	<	1.92		
2,6-DNT.....		4.16(103%)	<	0.40		
2,4-DNT.....		4.23(100%)	<	0.42		

**WIPES**

ROY F. WESSON, INC.  
Lionville Laboratory

CLIENT: EPAAP  
LW #: 0001L325-Wipes  
M.O. #: 2231-03-02

SAMPLES RECEIVED: 01-25-90

ENCLOSURE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Modified for the analysis of wipe samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.  
SSD = Designates sample spiked with target compound in duplicate.  
D = Indicates duplicate analysis of a sample.  
NS = Not spiked.  
DL = Diluted below calibration range.  
G = Indicates elevated detection limit due to sample interference.  
NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less Than  
> = Greater Than

Analysis Summary

Samples Collected: 01-26-90  
Samples Prepared: 01-30-90  
Samples Analyzed: 01-30-90

Carter Nulton, Ph.D.  
Vice President  
Lionville Analytical Laboratory

2/12/90  
Date

Roy F. Weston, Inc. - Lionville Laboratory  
EIP ANALYTICAL DATA PACKAGE FOR  
UCATHAMA-SWAAP

DATE RECEIVED: 01/26/90

RFW LOT # :9001L326

CLIENT ID	RFW #	MTX	PREP #	COLLECTION	EXTR/PREP	ANALYSIS
T12 CLAY PIPE POST T	001	WI		01/26/90		

# WESTON ANALYTICS NIPE EXPLOSIVES DATA

RFW Batch Number: 9001L326

CLIENT: HWAAP

Page: 1

Sample Information	Client		T 18		CLAYPIPE		BLANK		2XSS		10XSS	
	ID:		POST T				1		1		WA	
	RPM#:		001									
	D.F.:		10									
	Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
PAX.....	<	12.7	<	1.27	2.18(86.8%)	11.6(90.1%)						
NDX.....	<	9.80	<	0.98	1.71(87.1%)	8.86(90.3%)						
1,3,5-TNB.....	<	20.9	<	2.09	3.63(91.2%)	19.8(94.3%)						
1,3-DNB.....	<	5.90	<	0.59	1.07(96.7%)	5.86(99.3%)						
NITROBENZENE.....	<	55.4	<	0.42	1.08(93.7%)	4.83(115%)						
TRINYL.....	<	50.0	<	5.00	8.94(94.6%)	49.5(98.9%)						
2,4,6-TNT.....	<	19.2	<	1.92	3.63(98.3%)	19.7(120%)						
2,6-DNT.....	<	4.00	<	0.40	0.73(89.2%)	3.90(97.5%)						
2,4-DNT.....	<	4.20	<	0.42	0.72(89.9%)	4.00(95.3%)						

Client

Sample Information

ID: 10XSSD  
RPM#: 1  
D.F.: 1  
Units: Total ug

PAX.....	11.7(91.2%)
NDX.....	9.00(91.2%)
1,3,5-TNB.....	20.1(95.9%)
1,3-DNB.....	5.86(99.3%)
NITROBENZENE.....	4.55(108%)
TRINYL.....	49.0(98.0%)
2,4,6-TNT.....	19.3(118%)
2,6-DNT.....	3.77(94.1%)
2,4-DNT.....	3.93(93.9%)

WESTEN

ROY F. WESTEN, INC.  
Lionville Laboratory

CLIENT: HMAAP  
REF #: 90011326-Soil  
I.O. #: 2231-08-02

SAMPLES RECEIVED: 01-26-90

EXPLOSIVE INDICATIVE

Samples have been prepared and analyzed according to JSATHAMA Method LW02, Explosives in soil.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLX - Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS - Designates sample spiked with target compound.  
SSD - Designates sample spiked with target compound in duplicate.  
D - Indicates duplicate analysis of a sample.  
NS - Not spiked.  
DL - Diluted below calibration range.  
G - Indicates elevated detection limit due to sample interference.  
NR - Not reported.

NOTE: Spikes have been reported as result (% recovery).

NOTE: Soil results are reported in a dry weight basis.

Data Qualifiers

< = Less Than      > = Greater Than

Analysis Summary

Samples Collected: 01-26-90  
Samples Prepared: 01-30-90  
Samples Analyzed: 01-30-90

R. H. Hult  
Carter Hult, Ph.D.  
Vice President  
Lionville Analytical Laboratory

2-12-90  
Date



Roy F. Weston, Inc. - Lionville Laboratory  
REP ANALYTICAL DATA PACKAGE FOR  
FLATIRON-SWAAP

DATE RECEIVED: 01/26/90

REP LOT # 190011325

CLIENT ID	REP #	M.L.	PREP #	COLLECTION	EXTR/PREP	ANALYSIS
213 CLAYPIPE GROUND	002	WI		01/26/90		



**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP

SAMPLES RECEIVED: 7-16,19,27, 8-1,5,10,16,20,22,29, 9-2,11,20

REF #: 8907L058,059,154 8908L203,253,315,393,462,524,534,595

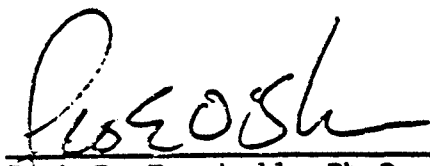
8909L595,679,804

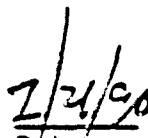
N.O. #: 2231-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.

  
\_\_\_\_\_  
Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

  
\_\_\_\_\_  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-03-02-0000

WESTON BATCH #: 8909L679

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-028	T13SMW2 PRE TEST	NITRATED ESTERS	27.6	UG	20.0
-029	T13SM FIELD BLANK	NITRATED ESTERS	5.0 u	UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8909L679

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC012-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC012-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-02-0000

WESTON BATCH #: 8909L679

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%REC
BLANK10	89LNC012-MB1	NITRATED ESTERS	10.1	2.5 u	10.0	101
BLANK20	89LNC012-MB2	NITRATED ESTERS	47.6	2.5 u	50.0	95.
		NITRATED ESTERS	48.8	2.5 u	50.0	97.

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-02-0000

WESTON BATCH #: 3909L679

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC012-M82	NITRATED ESTERS	95.2	97.6	2.5



## ROY F. WESTON INC.

## INORGANICS DATA SUMMARY REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-02-0000

WESTON BATCH #: 8909L304

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-001	T18 SMW2	NITRATED ESTERS	5.0	u UG	5.0
-002	T18 SM FIELD BLANK	NITRATED ESTERS	5.0	u UG	5.0
-003	T18 FLSH CHMB WA W2	NITRATED ESTERS	5.0	u UG	5.0
-004	T18 FLSH CHMB WA BLN	NITRATED ESTERS	5.0	u UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-02-0000

WESTON BATCH #: 8909L804

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC014-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC014-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/20/90

CLIENT: USATHAMA-HNAAP  
WORK ORDER: 2231-03-02-0000

WESTON BATCH #: 3909L30

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%REC
BLANK10	89LNC014-MB1	NITRATED ESTERS	10.1	2.5 u	10.0	101
BLANK20	89LNC014-MB2	NITRATED ESTERS	49.3	2.5 u	50.0	99
		NITRATED ESTERS	43.9	2.5 u	50.0	97

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/20/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-02-0000

WESTON BATCH #: 8909L304

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC014-MB2	NITRATED ESTERS	99.5	97.7	1.8

**APPENDIX G**

**ANALYTICAL DATA SUMMARY TABLES FOR STACK TEST PROGRAM**

1311R2

## APPENDIX G

Appendix G contains data collected from stack testing that was conducted during T2, T3, and T5. Two types of data are included. The first type consists of raw operational data from the flash chamber inlet, flash chamber outlet, and the afterburner outlet. These data were used to generate Tables 3-6, 3-7, and 3-8 in the main report. The following information is included:

- Flash chamber inlet
  - Test data.
  - Inputs for calculations.
  - CEM report data for total hydrocarbons.
- Flash Chamber Outlet (sheet 1, explosives data)
  - Test data.
  - Inputs for calculations.
  - Laboratory report data for explosives.
- Flash Chamber Outlet (sheet 2, smokeless powder data)
  - Test data.
  - Inputs for calculations.
  - Smokeless powder results from sample train.
  - CEM report data for total hydrocarbons.
- Afterburner Outlet (sheet 1, explosives data)
  - Test data.
  - Inputs for calculations.
  - Laboratory report data for explosives.
- Afterburner Outlet (sheet 2, smokeless powder and particulate data)
  - Test data.
  - Inputs for calculations.
  - Laboratory report data.
    - Particulate catch.
    - Smokeless powder catch.
  - CEM report data for NO<sub>x</sub> and total hydrocarbons.

The second type of data consists of analytical data summaries generated by the offsite laboratory (WESTON Analytics Division, Lionville, Pennsylvania). The analytical data summaries provide the following information:

- Inorganic narrative (explosives narrative presented, where applicable).

- Glossary of terms.
- Inorganics data summary report.
- Inorganics quality assurance/quality control (QA/QC) report.
- Explosives narrative.
- Explosives data summary.

The inorganic narrative is generally a summary of the quality control results and a description of any problems encountered during the analysis of the samples. The glossary of terms defines the data qualifiers used in the report, abbreviations, and laboratory chronology and holdtime report codes.

The inorganics data summary presents the actual results of the analysis. In addition, the lab sample number, site ID, analyte tested, and the reporting limit are provided.

The inorganics QA/QC report includes the analysis of a method blank, inorganics accuracy report, and an inorganics duplicate spike report.

July 1990  
Revision: Final

STACK TEST 2  
400°F/24 HOURS  
RAW OPERATIONAL DATA

1311R2



SAWTOORNE ARMY AMMUNITION PLANT  
SAWTOORNE, NEVADA

Test Data	T2-1	T2-2	T2-3
Run number		FLASH CHAMBER INLET	
Location			
Date	07-25-89	07-25-89	07-26-89
Time period	0340-1345	1720-2200	0950-1400
Operator	COO	COO	COO

Inputs For Calcs.			
Sq. ft. delta P	0.130120	0.441590	0.158260
Delta H	0.75000	0.75000	0.75000
Stack temp. (deg.F)	330.75	311.37	743.00
Meter temp. (deg.F)	100.30	97.30	99.30
Sample volume (act.)	164.255	143.065	125.522
Barometric press. (in.Hg)	26.44	26.44	26.40
Volume H2O imp. (ml)	75.30	50.30	25.00
Weight chnge sil. gel (g)	37.30	39.30	34.00
% CO2	1.900	1.900	1.800
% O2	17.300	17.300	17.500
ppm CO	131.300	175.100	200.300
% N	81.100	81.100	80.900
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	305.30	280.00	250.00
Static pressure (in.H2O)	0.06	0.06	0.06
Nozzle dia. (in.)	NA	NA	NA
Meter box cal.	0.9991	0.9991	0.9991
Cp of pitot tube	0.34	0.34	0.34

Com Report Data

Total Hydrocarbon PPM	29.6	39.8	45.6
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HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

Test Data	EXPLOSIVES TEST		
Run number	T2-1	T2-2	T2-3
Location	FLASH CHAMBER OUTLET		
Date	7-25-89	7-25-89	7-26-89
Time period	0830-1536	1558-2331	0945-1414
Operator	JDO/SK	SK/WS	SK/WS

Inputs For Calcs.			
Sq. rt. delta P	0.434755	0.510594	0.506651
Delta H	1.10647	1.40764	1.35625
Stack temp. (deg.F)	345.42	405.99	424.35
Meter temp. (deg.F)	105.74	102.26	106.34
Sample volume (act.)	233.731	324.082	171.536
Barometric press. (in.Hg)	26.44	26.31	26.40
Volume H2O imp. (ml)	72.00	116.00	35.00
Weight chnge sil. gel (g)	57.00	64.35	37.00
% CO2	1.200	1.100	1.100
% O2	16.200	18.400	18.300
CO ppm	86.700	92.300	122.700
% N	82.600	80.600	80.600
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	360.00	445.00	240.00
Static pressure (in.H2O)	-0.44	-0.56	-0.54
Nozzle dia. (in.)	0.300	0.300	0.300
Meter box cal.	1.0020	1.0020	1.0020
Cp of pitot tube	0.84	0.84	0.84

Laboratory Report Data, Total ug

HMX	<	3180.00	<	3180.00		4.18
RDX	<	2450.00	<	2450.00	<	2.45
Trinitrobenzene (1 3 5 TNB)	<	5230.00	<	5230.00	<	5.23
Dinitrobenzene (1 3 DNB)	<	1480.00	<	1480.00		4.46
Nitrobenzene	<	1050.00	<	1050.00	<	1.05
Tetryl	<	12500.00	<	12500.00	<	12.50
2 4 6 Trinitrotoluol (TNT)		70400.00		39600.00		93.50
2 4 Dinitrotoluene (2 4 DNT)	<	1050.00	<	1050.00	<	1.05
2 6 Dinitrotoluene (2 6 DNT)	<	1000.00	<	1000.00	<	1.00

SMITHSONIAN ENVIRONMENTAL PLANT  
MILPITAS, CALIF.

Test Data	PARTICULATE TEST		
	T2-1	T2-2	T2-3
Run Number	7-15-79	7-15-79	7-15-79
Location	FLASH CHAMBER OUTLET	FLASH CHAMBER OUTLET	FLASH CHAMBER OUTLET
Date	7-15-79	7-15-79	7-15-79
Time period	0330-1526	1629-2331	0945-1444
Operator	JOJO/CX	JOJO/CX	JOJO/CX
Inputs For Calcs.			
Eq. rt. Delta P	0.140399	0.101035	0.199036
Delta H	1.10442	1.10774	1.10563
Stack temp. (deg.F)	343.79	403.76	423.33
Pitot temp. (deg.F)	113.08	103.62	114.74
Sample volume (act.)	348.742	315.669	330.476
Barometric press. (in.Hg)	29.44	29.31	29.40
Volume H2O imp. (ml)	12.00	109.00	12.00
Weight chnge sil. gel (g)	45.00	66.00	37.00
% CO2	1.100	1.100	1.100
% O2	16.200	15.400	15.300
CO ppm	26.700	92.000	122.700
% H	32.600	30.500	30.600
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	260.00	420.00	240.00
Static pressure (in.H2O)	-0.50	-0.57	-0.57
Nozzle dia. (in.)	0.310	0.310	0.310
Meter box cal.	1.0020	1.0020	1.0020
Cp of pitot tube	0.34	0.34	0.34
Smokeless powder			
Total Nitrated Esters, ug	30003.5	13601.49	1591.88
Com Report Data			
Total Hydrocarbon PPM	23.9	28.9	34.3

WANTONNE ARMY AMMUNITION PLANT  
WANTONNE, NEVADA

Test Data	EXPLOSIVES TEST		
Run number	T2-1	T2-2	T2-3
Location	AFTERSURNER MUYLET		
Date	7-25-69	7-25-69	7-25-69
Time period	0800-1537	1540-2340	0945-1444
Operator	CM/SK	CM/WS	CM/SK

Inputs For Calcs.			
St. ht. delta P	0.069896	0.103104	0.092647
Delta H	0.33191	1.01125	0.955208
Stack temp. (deg.F)	1725.68	1790.24	1721.35
Water temp. (deg.F)	112.41	108.92	114.34
Sample volume (act.)	157.991	224.444	144.556
Barometric press. (in.Hg)	29.44	26.31	29.40
Volume H2O imp. (ml)	280.00	320.00	175.00
Weight chge sil. gel (g)	43.00	55.00	31.00
% CO2	7.100	6.500	5.000
% O2	9.300	10.700	11.500
PPM CO	7.500	6.000	7.000
% H	83.000	82.800	82.500
Area of stack (sq.ft.)	17.10	17.10	17.10
Sample time (min.)	340.00	360.00	240.00
Static pressure (in.H2O)	-0.10	-0.10	-0.10
Nozzle dia. (in.)	0.750	0.300	0.300
Water box cal.	0.9953	0.9953	0.9953
Cp of pitot tube	0.84	0.84	0.84

Laboratory Report Data, Total ug

IMX		12.52	2.16 <	1.27
SDX	<	0.98 <	0.98	2.92
Trinitrobenzene (1 3 5 TNB)		5.90 <	2.09 <	2.09
Dinitrobenzene (1 3 DNB)		0.50	0.24	0.87
Nitrobenzene	<	0.42 <	0.42 <	0.42
Tetryl	<	5.00 <	5.00 <	5.00
2 4 5 Trinitrotoluol (TNT)	<	1.92 <	1.92 <	1.92
2 4 Dinitrotoluene (2 4 DNT)	<	0.42 <	0.42 <	0.42
2 5 Dinitrotoluene (2 6 DNT)	<	0.40 <	0.40 <	0.40

ANTHROME ARMY AMMUNITION PLANT  
ANTHROME, NEVADA

Test Data	SMOKELESS POWDER AND PARTICULATE TEST		
Run Number	T2-1	T2-2	T2-3
Location	AFTERBURNER OUTLET		
Date	7-25-69	7-25-69	7-25-69
Time period	0830-1037	1640-2340	0945-1414
Operator	JM/SK	JM/WS/SK	JM/WS
<b>Inputs For Calcs.</b>			
Std. rt. Delta P	0.099753	0.101708	0.104104
Delta H	1.45147	1.52653	1.19458
Stack temp. (deg.F)	1663.93	1703.27	1639.71
Aeter temp. (deg.F)	109.50	105.31	110.25
Sample volume (act.)	235.949	256.203	151.315
Barometric press. (in.Hg)	25.44	25.31	25.40
Volume H2O imp. (ml)	339.00	340.00	198.00
Weight chnge sil. gel (g)	50.00	56.00	35.00
% CO2	7.10	6.50	6.00
% O2	9.20	10.70	11.50
PPM CO	7.50	6.20	7.00
% H	33.00	32.30	32.50
Area of stack (sq.ft.)	17.10	17.10	17.10
Sample time (min.)	340.00	360.00	240.00
Static pressure (in.H2O)	-0.10	-0.10	-0.10
Nozzle dia. (in.)	0.360	0.360	0.310
Meter box cal.	1.0030	1.0030	1.0030
Cp of pitot tube	0.34	0.34	0.34
<b>Laboratory Report Data</b>			
Front half acetone, g.	0.0049	0.0018	0.0024
Filter catch, g.	0.0025	0.0018	0.0020
Total particulate catch, g.	0.0074	0.0036	0.0044
<b>Smokeless powder</b>			
Nitrated Esters	< 1805	< 1660	< 1447
<b>Cam Report Data</b>			
NOx PPM	58.9	54.6	54.8
Total Hydrocarbon PPM	0.2	0.0	0.3

July 1990  
Revision: Final

**STACK TEST 3**  
**500°F/36 HOURS**  
**RAW OPERATIONAL DATA**

1311R2

PANTHORNE ARMY AMMUNITION PLANT  
PANTHORNE, NEVADA

Test Data

Run number	T3-1	T3-2	T3-3
Location		FLASH CHAMBER INLET	
Date	07-17-89	07-17-89	07-13-89
Time period	0450-1206	1449-1900	1440-2100
Operator	JDO	JDO	JDO

Inputs For Calcs.

Sq. ft. Delta P	0.489600	0.529150	0.524400
Delta H	1.30000	0.75000	0.70000
Stack temp. (deg.F)	1123.00	1050.30	935.00
Water temp. (deg.F)	110.00	100.00	103.00
Sample volume (act.)	238.741	127.621	190.899
Barometric press. (in.Hg)	26.48	25.94	25.97
Volume H2O imp. (ml)	115.00	80.00	50.00
Weight chnge sil. gel (g)	20.00	23.00	47.00
% CO2	2.400	2.200	1.300
% O2	15.000	16.500	16.700
ppm CO	9.200	55.500	113.600
% N	81.000	81.200	81.500
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	436.00	251.00	380.00
Static pressure (in.H2O)	0.06	0.06	0.06
Nozzle dia. (in.)	NA	NA	NA
Meter box cal.	0.9991	0.9991	0.9991
Cp of pitot tube	0.34	0.34	0.84

Gen Report Data

Total Hydrocarbon PPM	49.0	33.1	38.2
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WANTHORNE ARMY AMMUNITION PLANT  
WANTHORNE, NEVADA

Test Data	EXPLOSIVES TEST		
	T3-1	T3-2	T3-3
Run number			
Location	FLASH CHAMBER OUTLET		
Date	7-17-89	7-17-89	7-18-89
Time period	0445-1226	1439-2221	1433-2134
Operator	JDO/MS	JDO/SK	JDO/MS

Inputs For Calcs.	T3-1	T3-2	T3-3
Sq. ft. delta P	0.461140	0.442933	0.502224
Delta H	1.03269	0.92759	1.20219
Stack temp. (deg.F)	440.22	510.21	512.69
Peter temp. (deg.F)	96.24	113.48	111.32
Sample volume (act.)	229.737	146.367	243.277
Barometric press. (in.Hg)	25.48	25.34	25.37
Volume H2O imp. (ml)	100.00	74.00	124.00
Weight chnge sil. gel (g)	56.00	31.00	49.00
% CO2	1.400	1.300	1.130
% O2	17.200	17.500	17.500
PPH CO	19.000	100.400	169.000
% H	81.400	81.200	81.300
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	360.00	240.00	360.00
Static pressure (in.H2O)	-0.48	-0.48	-0.56
Nozzle dia. (in.)	0.300	0.300	0.300
Peter box cal.	1.0020	1.0020	1.0020
Cp of pitot tube	0.84	0.84	0.84

Laboratory Report Data, Total ug

HMX	<	3180.00 <	31.80 <	12.70
RDX	<	2450.00 <	24.50 <	9.80
Trinitrobenzene (1 3 5 TNB)	<	5230.00 <	52.30	21.70
Dinitrobenzene (1 3 DNB)	<	1480.00 <	14.80 <	5.90
Nitrobenzene	<	1050.00 <	10.50	22.00
Tetryl	<	12500.00 <	125.00 <	50.07
2 4 6 Trinitrotoluol (TNT)		89200.00	64.20	171.00
2 4 Dinitrotoluene (2 4 DNT)	<	1056.00 <	10.50 <	4.20
2 6 Dinitrotoluene (2 6 DNT)	<	1000.00 <	10.00 <	4.00



AMTORGUE RISKY POLLUTION PLANT  
AMTORGUE, NEVADA

Test Data	PARTICULATE TEST		
	TS-1	TS-2	TS-3
Run Number	7-17-79	7-17-79	7-18-79
Location	0445-1223	1441-2221	1424-2124
Date	000/VS	JM/SK	JM/VS
Time period			
Operator			
Inputs For Calcs.			
Sq. ft. duct P	0.456053	0.447826	0.460654
Delta H	1.40324	1.20092	1.20877
Stack temp. (deg.F)	440.59	507.35	498.24
Meter temp. (deg.F)	103.47	119.51	113.28
Sample volume (act.)	240.263	156.636	240.406
Barometric press. (in.Hg)	26.48	25.94	25.87
Volume H2O imp. (ml)	107.00	79.00	128.00
Weight change sil. gel (g)	40.50	33.00	46.00
% CO2	1.400	1.300	1.300
% O2	17.200	17.500	17.600
PPM CO	19.000	100.400	169.000
% H	81.400	81.200	81.300
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	370.00	240.07	360.00
Static pressure (in.H2O)	-0.48	-0.50	-0.52
Nozzle dia. (in.)	0.310	0.310	0.310
Meter box cal.	1.0020	1.0020	1.0020
Cp of pitot tube	0.34	0.34	0.34
Smokeless powder			
Nitrated Esters	35692.58	3099.38	7703.13
Cam Report Data			
Total Hydrocarbon PPM	33.9	27.8	27.9

HAWTHORNE ARMY AMMUNITION PLANT  
HAWTHORNE, NEVADA

Test Data	EXPLOSIVES TEST		
	T3-1	T3-2	T3-3
Run number			
Location	AFTERBURNER OUTLET		
Date	7-17-89	7-17-89	7-18-89
Time period	0445-1226	1440-2221	1433-2134
Operator	JM/WS	JM/SK	JM/WS

Inputs For Calcs.

Sq. ft. Delta P	0.090423	0.084823	0.096900
Delta H	0.30397	0.54542	0.72431
Stack temp. (deg.F)	1818.47	1802.19	1806.30
Meter temp. (deg.F)	98.33	116.21	118.50
Sample volume (act.)	174.486	112.964	191.591
Barometric press. (in.Hg)	25.48	25.94	25.97
Volume H2O imp. (ml)	275.00	185.00	310.00
Weight chnge sil. gel (g)	42.00	25.00	43.00
% CO2	6.500	6.700	6.200
% O2	10.300	11.000	11.200
PPH CO	4.900	1.300	6.600
% H	83.200	82.300	82.500
Area of stack (sq.ft.)	17.10	17.10	17.10
Sample time (min.)	360.00	240.00	360.00
Static pressure (in.H2O)	-0.10	-0.10	-0.10
Nozzle dia. (in.)	0.760	0.760	0.760
Meter box cal.	0.9953	0.9953	0.9953
Cp of pitot tube	0.84	0.84	0.84

Laboratory Report Data, Total ug

HMX	<	1.27 <	1.27 <	1.27
RDX		3.81	3.82	2.80
Trinitrobenzene (1 3 5 TNB)	<	2.09	3.46	2.78
Dinitrobenzene (1 3 DNB)		5.60	8.40	5.17
Nitrobenzene	<	0.42	20.20 <	0.42
Tetryl	<	5.00 <	5.00 <	5.00
2 4 6 Trinitrotoluol (TNT)	<	1.92 <	1.92 <	1.92
2 4 Dinitrotoluene (2 4 DNT)	<	0.42 <	0.42 <	0.42
2 6 Dinitrotoluene (2 6 DNT)	<	0.40 <	0.40 <	0.40

INTEGRAL GUN AMMUNITION PLANT  
INTEGRAL, NEVADA

Test Data	PARTICULATE TEST		
	TS-1	TS-2	TS-3
Run Number		AFTERBURNER OUTLET	
Location			
Date	7-17-39	7-17-39	7-13-39
Time period	0445-1226	1440-2221	1434-2134
Operator	JH/WS	JH/GK	JH/WS
Inputs For Calcs.			
Sq. ft. Delta P	0.073102	0.034311	0.037440
Delta H	0.33597	1.07917	1.12131
Stack temp. (deg.F)	1747.39	1000.35	1739.20
Water temp. (deg.F)	28.10	113.51	114.58
Sample volume (act.)	191.334	142.223	221.776
Barometric press. (in.Hg)	26.48	25.24	25.97
Volume H2O imp. (ml)	328.00	252.00	376.00
Weight change sil. gel (g)	40.30	31.30	46.30
% CO2	6.300	6.700	6.200
% O2	10.300	11.000	11.200
PPM CO	4.200	1.300	6.600
% H	33.200	32.300	32.500
Area of stack (sq.ft.)	17.10	17.10	17.10
Sample time (min.)	360.00	240.00	360.00
Static pressure (in.H2O)	-0.09	-0.10	-0.10
Nozzle dia. (in.)	0.360	0.260	0.360
Water box cal.	1.0030	1.0030	1.0030
Cp of pitot tube	0.34	0.34	0.34
Laboratory Report Data			
Front half acetone, g.	0.0009	0.0030	0.0033
Filter catch, g.	0.0016	0.0019	0.0024
Total particulate catch, g.	0.0025	0.0049	0.0057
Smokeless powder			
Nitrated Esters	3184.97	2237.525	5774.47
Gas Report Data			
NOx PPM	55.4	48.8	47.4
Total Hydrocarbon PPM	0.1	0.3	0.1

July 1990  
Revision: Final

STACK TEST 5  
300°F/24 HOURS  
RAW OPERATIONAL DATA

1311R2

SAWTOOTH ARMY AMMUNITION PLANT  
SAWTOOTH, NEVADA

Test Data			
Run number	T5-1	T5-2	T5-3
Location		FLASHCHAMBER INLET	
Date	07-29-89	07-29-89	07-30-89
Time period	1017-1630	1500-2400	1200-1630
Operator	JDG	JDG	JDG

Inputs For Calcs.

Sq. ft. delta P	0.424260	0.489900	0.415890
Delta P	0.75000	0.75000	0.75000
Stack temp. (deg.F)	373.30	1075.00	397.50
Meter temp. (deg.F)	98.00	92.00	101.50
Sample volume (act.)	183.074	143.753	130.243
Barometric press. (in.Hg)	26.41	26.41	26.38
Volume H2O imp. (ml)	50.00	55.00	44.00
Weight chge sil. gel (g)	34.00	33.00	23.00
% CO2	1.00	2.20	2.00
% O2	17.40	16.50	16.70
ppm CO	136.00	261.00	206.10
% H	81.00	81.30	81.30
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	373.00	300.00	240.00
Static pressure (in.H2O)	0.05	0.05	0.05
Nozzle dia. (in.)	NA	NA	NA
Meter box cal.	0.9991	0.9991	0.9991
Cp of pivot tube	0.34	0.34	0.34

Cam Report Data

Total Hydrocarbon PPM	32.2	50.8	45.8
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# HAWTHORNE ARMY AMMUNITION PLANT HAWTHORNE, NEVADA

Test Data	EXPLOSIVES TEST		
Run number	T5-1	T5-2	T5-3
Location	FLASH CHAMBER OUTLET		
Date	7-20-89	7-20-89	7-30-89
Time period	0955-1720	1820-0129	1221-1719
Operator	SK/WS	WS/SK	SK/WS

Inputs For Calcs.			
Sq. ft. delta P	0.139205	0.528697	0.502866
Delta H	1.77349	1.37347	1.22000
Stack temp. (deg.F)	253.35	479.84	521.23
Water temp. (deg.F)	106.33	99.28	103.60
Sample volume (act.)	254.112	256.323	161.335
Barometric press. (in.Hg)	25.11	25.41	26.37
Volume H2O imp. (ml)	60.00	73.00	50.00
Weight chnge sil. gel (g)	49.00	66.00	34.00
% CO2	1.200	1.500	1.600
% O2	18.100	17.400	17.500
PPM CO	106.000	171.200	188.500
% N	80.700	81.000	80.900
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	390.00	360.00	240.00
Static pressure (in.H2O)	-0.49	-0.58	-0.57
Nozzle dia. (in.)	0.300	0.300	0.300
Water box cal.	1.0020	1.0020	1.0020
Cp of pitot tube	0.84	0.84	0.84

## Laboratory Report Data, Total ug

HMX	<	2380.00 <	127.00 <	12.70
RDX	<	1840.00 <	98.00 <	9.80
Trinitrobenzene (1 3 5 TNB)	<	3920.00 <	209.00 <	20.90
Dinitrobenzene (1 3 DNB)	<	1110.00 <	59.00 <	5.90
Nitrobenzene	<	788.00 <	42.00 <	4.20
Tetryl	<	9380.00 <	500.00 <	50.00
2 4 6 Trinitrotoluol (TNT)		76800.00	677.00	184.00
2 4 Dinitrotoluene (2 4 DNT)	<	780.00 <	42.00 <	4.20
2 6 Dinitrotoluene (2 6 DNT)	<	750.00 <	40.00 <	4.00

ANTHROPIC DUMP DECONTAMINATION PLANT  
 JEFFERSON, NEVADA

Test Data	PARTICULATE TEST		
	TS-1	TS-2	TS-3
Run Number			
Location		FLASH CHAMBER OUTLET	
Date	7-29-79	7-29-79	7-30-79
Time period	0955-1720	0824-0129	1221-1719
Operator	JK/MS	MS/SK	JK/MS

Inputs For Calcs.

Sq. ft. Delta P	0.455045	0.505283	0.504881
Delta H	1.51256	1.20542	1.34229
Stack temp. (deg.F)	379.26	477.57	519.33
Water temp. (deg.F)	114.20	107.35	116.51
Sample volume (act.)	278.342	247.516	172.069
Barometric press. (in.Hg)	28.41	28.41	28.37
Volume H2O (sp. (ml)	77.00	97.00	62.00
Weight chnge sil. gel (g)	48.00	52.00	34.00
% CO2	1.200	1.300	1.600
% O2	13.100	17.400	17.500
PPM CO	106.000	171.200	188.500
% H	30.700	31.000	30.900
Area of stack (sq.ft.)	1.77	1.77	1.77
Sample time (min.)	390.00	360.00	240.00
Static pressure (in.H2O)	-0.50	-0.57	-0.58
Nozzle dia. (in.)	0.310	0.310	0.310
Water box cal.	1.0020	1.0020	1.0020
Cp of pitot tube	0.34	0.34	0.34

Nitrated Esters	23326.00	1041.31	4389.53
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Cam Report Data

Total Hydrocarbon PPM	25.0	34.7	30.5
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WANTHORNE ARMY PRODUCTION PLANT  
WANTHORNE, NEVADA

Test Data	EXPLOSIVES TEST		
	TS-1	TS-2	TS-3
Run number			
Location	AFTERBURNER OUTLET		
Date	7-29-89	7-29-89	7-30-89
Time period	0955-1720	1824-0129	1221-1718
Operator	JM/WS	JM/SK	JM/SK
Inputs For Calcs.			
Sq. rt. delta P	0.099307	0.100790	0.096163
Delta H	0.06603	1.30944	0.927500
Stack temp. (deg.F)	1692.26	1703.71	1713.36
Merer temp. (deg.F)	117.94	105.44	119.65
Sample volume (act.)	239.435	219.621	142.886
Barometric press. (in.Hg)	26.41	26.41	26.37
Volume H2O imp. (ml)	358.00	301.00	180.00
Height chnge sil. gel (g)	46.50	63.00	36.00
% CO2	6.800	6.200	6.100
% O2	10.300	11.000	11.200
PPM CO	6.900	5.800	6.900
% N	83.100	82.300	82.700
Area of stack (sq.ft.)	17.10	17.10	17.10
Sample time (min.)	390.00	360.00	240.00
Static pressure (in.H2O)	-0.10	-0.10	-0.10
Nozzle dia. (in.)	0.300	0.300	0.300
Water box cal.	0.9953	0.9953	0.9953
Cp of pitot tube	0.34	0.34	0.34
Laboratory Report Data, Total ug			
HMX	12.70	1.47 <	1.27
RDX	2.76	2.57	2.84
Trinitrobenzene (1 3 5 TNB) <	2.09	2.19	7.62
Dinitrobenzene (1 3 DNB)	2.63	7.60	1.90
Nitrobenzene <	0.42	1.56	1.91
Tetryl <	5.00 <	5.00 <	5.00
2 4 6 Trinitrotoluol (TNT) <	1.92 <	1.92 <	1.92
2 4 Dinitrotoluene (2 4 DNT) <	0.42 <	0.42 <	0.42
2 6 Dinitrotoluene (2 6 DNT) <	0.40 <	0.40 <	0.40



WITCOMB ARMY AMMUNITION PLANT  
WITCOMB, NEVADA

Test Data

Run Number  
Location  
Date  
Time period  
Operator

NITRATED ESTERS AND PARTICULATE TEST

TS-1 TS-2 TS-3

AFTERBURNER OUTLET

7-29-89 7-29-89 7-30-89  
0955-1720 1824-0129 1221-1713  
JH/WS JH/CX JH/WS

Inputs for Calcs.

sq. ft. Delta P	0.028273	0.107720	0.101726
Delta H	1.12049	1.25056	1.25358
Stack temp. (deg.F)	1697.56	1712.46	1719.36
Water temp. (deg.F)	111.27	102.55	111.29
Sample volume (act.)	243.418	242.749	156.510
Barometric press. (in.Hg)	25.41	25.41	25.37
Volume H2O imp. (ml)	316.30	339.00	204.00
Weight chnge sil. gel (g)	53.30	59.30	32.30
% CO2	6.50	6.20	6.10
% O2	10.30	11.30	11.20
PPM CO	6.90	5.50	6.20
% H	53.10	52.30	52.70
Area of stack (sq.ft.)	17.10	17.10	17.10
Secale time (min.)	390.00	360.00	240.00
Static pressure (in.H2O)	-0.10	-0.10	-0.10
Nozzle dia. (in.)	0.310	0.310	0.310
Water box cal.	1.0030	1.0030	1.0030
Cp of pitot tube	0.34	0.34	0.34

Laboratory Report Data

Front half acetone, g.	0.0029	0.0012	0.0000
Filter catch, g.	0.0015	0.0005	0.0000
Total particulate catch, g.	0.0044	0.0017	0.0000

Nitrated Esters	1847.5 <	2575 <	1413
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Can Report Data

NOx PPM	57.3	48.7	51.7
Total Hydrocarbon PPM	0.6	0.3	0.4

July 1990  
Revision: Final

**STACK TEST 2**  
**400°F/24 HOURS**  
**ANALYTICAL DATA SUMMARY**

1311R2

**WESTON**


ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP  
SAMPLES RECEIVED: 7-19, 20, 8-1  
REF#: 8907L060,073,153, 137  
8908L202  
W.O.#: 0291-08-02

INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.



Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

7/24/90  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

## ROY F. WESTON INC.

## INORGANICS DATA SUMMARY REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
 WORK ORDER: 2231-03-04-0000

WESTON BATCH #: 3907L158

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-015	UH-FCO-PART-BHW T2-1	NITRATED ESTERS	29700	UG	1400
-016	UH-FCO-PART-BHA T2-1	NITRATED ESTERS	743	UG	338
-017	UH-AO-PART-FHA T2-1	PARTICULATE	0.0061	grams	0.0000
-018	UH-AO-PART-FILT-T2-1	PARTICULATE	0.0026	grams	0.0000
-019	UH-AO-PART-BHW-T2-1	NITRATED ESTERS	1550 u	UG	1550
-020	UH-AO-PART-BHA-T2-1	NITRATED ESTERS	250 u	UG	250
-035	UH-FCO-PART-BHW T2-2	NITRATED ESTERS	12600	UG	1250
-036	UH-FCO-PART-BHA T2-2	NITRATED ESTERS	1420	UG	425
-037	UH-AO-PART-FHA T2-2	PARTICULATE	0.0031	grams	0.0000
-038	UH-AO-PART-FILT T2-2	PARTICULATE	0.0018	grams	0.0000
-039	UH-AO-PART-BHW T2-2	NITRATED ESTERS	1480 u	UG	1480
-040	UH-AO-PART-BHA T2-2	NITRATED ESTERS	175 u	UG	175
-051	COMP FLO PT T2-1	NITRATED ESTERS	5.0 u	UG	5.0
-052	COMP AO PT T2-1	NITRATED ESTERS	5.0 u	UG	5.0
-053	COMP FLO PT T2-2	NITRATED ESTERS	11.1	UG	5.0
-054	COMP AO PT T2-2	NITRATED ESTERS	5.0 u	UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/16/90

CLIENT: USATHANA-HWAAP  
WORK ORDER: 2231-03-04-0000

WESTON BATCH #: 8907L158

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC008-MB1	NITRATED ESTERS	2.5 u	MG/L	2.
BLANK20	89LNC008-MB2	NITRATED ESTERS	2.5 u	MG/L	2.

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-03-04-0000

WESTON BATCH #: 3907L158

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	39LNC008-M81	NITRATED ESTERS	10.3	2.5 u	10.0	108
BLANK20	39LNC008-M82	NITRATED ESTERS	49.6	2.5 u	50.0	99.3
		NITRATED ESTERS	49.5	2.5 u	50.0	99.3

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-08-04-0000

WESTON BATCH #: 3907L11

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	39LNC008-MB2	NITRATED ESTERS	99.3	99.0	0.20



## ROY F. WESTON INC.

## INORGANICS DATA SUMMARY REPORT 02/13/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-04-0000

WESTON BATCH #: 8907L187

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-016	UH-FCO-PART-BHW T2-3	NTRATED ESTERS	1330	UG	1150
-017	UH-FCO-PART-BHA T2-3	NTRATED ESTERS	650	u UG	650
-018	UH-AO-PART-FHA T2-3	PARTICULATE	0.0037	grams	0.0000
-019	UH-AO-PART FLT-T2-3	PARTICULATE	0.0020	grams	0.0000
-020	UH-AO-PART-BHW T2-3	NTRATED ESTERS	1180	u UG	1180
-021	UH-AO-PART-BHA T2-3	NTRATED ESTERS	262	u UG	252
-024	COMP FCO PART T2-3	NTRATED ESTERS	6.4	UG	5.0
-025	COMP AO PART T2-3	NTRATED ESTERS	5.0	u UG	5.0

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-04-0000

WESTON BATCH #: 8907L137

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTIN LIMIT
BLANK10	89LNC008-MB1	NTRATED ESTERS	2.5	u MG/L	2.5
BLANK20	89LNC008-MB2	NTRATED ESTERS	2.5	u MG/L	2.5

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/16/90

CLIENT: USATH MA-HWAAP  
WORK ORDER: 2291-03-04-0000

WESTON BATCH #: 39071187

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	39LNC008-MB1	NTRATED ESTERS	10.3	2.5 u	10.0	103
BLANK20	39LNC008-MB2	NTRATED ESTERS	49.5	2.5 u	50.0	99.3
		NTRATED ESTERS	49.5	2.5 u	50.0	99.0

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-08-04-0000

WESTON BATCH #: 8907L18

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC008-MB2	NTRATED ESTERS	99.3	99.0	0.20

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HAWTHORNE  
RFV #: 3907L153, Air  
W.O.#: 2231-08-04

SAMPLES RECEIVED: 07-27-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of MI-5 samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.  
SSD = Designates sample spiked with target compound in duplicate.  
D = Indicates duplicate analysis of a sample.  
NS = Not spiked.  
DL = Diluted below calibration range.  
G = Indicates elevated detection limit due to sample interference.  
NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less than  
> = Greater than

Analysis Summary:

Samples Collected: 07-25-89  
Samples Prepared: 07-28,31-89  
Samples Analyzed: 08-07-89

George P. Nulton  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

8/21/89  
DATE

NOTE: Non-quantitative recoveries were obtained for nitrobenzene during these analysis. Modifications made to Method LW02 to analyze MM-5 samples resulted in the loss of nitrobenzene during analysis. Although certified detection limits have been reported, it is likely that actual detection limits are higher than the detection limits reported.

## RFFW Batch Number: 8907L158

Page: 1

**CLIENT:**

USATHAMA-HAWTHORNE

## Sample Information

## Client

II ::

RFW#:

D. E. :

T2-2

AO

050

1.0

**BLANK**

055

1.0

IMX.....	< 3180	16.6G	< 3180	6.24G	4.08G	< 1.27
RDX.....	< 2450	< 0.98	< 2450	< 0.98	< 0.98	< 0.98
1,3,5-TNB.....	< 5230	5.90G	< 5230	< 2.09	< 2.09	< 2.09
1,3-DNB.....	< 1480	2.78G	< 1480	2.42G	2.18G	< 0.59
NITROBENZENE.....	< 1050	< 0.42	< 1050	< 0.42	< 0.42	< 0.42
TETRYL.....	< 12,500	< 5.00	< 12,500	< 5.00	< 5.00	< 5.00
2,4,6-TNT.....	70,400	< 1.92	39,500	< 1.92	< 1.92	< 1.92
2,6-DNT.....	< 1000	< 0.40	< 1000	< 0.40	0.42G	< 0.40
2,4-DNT.....	< 1050	< 0.42	< 1050	< 0.42	< 0.42	< 0.42

**client**

**ID :**

**RFW:**

**D.F.:**

**Units:**

## Sample Information

## 20XSS

0.1

**Total**

**100XSS**

1.0

**Total**

100XSGD

2

Total use

HMX.....	21.9(86.2%)
RDX.....	17.3(88.3%)
1,3,5-TNB.....	31.0(74.2%)
1,3-DNB.....	7.68(65.1%)
NITROBENZENE.....	< 0.42(0.0%)
TETRYL.....	55.0(55.0%)
2,4,6-TNT.....	26(67.7%)
2,6-DNT.....	3.09(38.6%)
2,4-DNT.....	5.36(63.8%)

106(83.4%)	111(87.4%)
81.6(83.3%)	85.6(87.3%)
158(75.6%)	162(77.5%)
42.3(71.5%)	42.6(72.2%)
3.24(7.71%)	3.19(7.57%)
330(66.0%)	349(69.8%)
130(67.7%)	129(67.1%)
19.6(49.0%)	18.5(46.3%)
28.2(67.1%)	26.9(54.0%)

## G-Elevated

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HAWTHORNE  
REF #: 8907L137, Air  
W.O. #: 2281-08-04

SAMPLES RECEIVED: 07-29-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of XM-5 samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.  
SSD = Designates sample spiked with target compound in duplicate.  
D = Indicates duplicate analysis of a sample.  
NS = Not spiked.  
DL = Diluted below calibration range.  
G = Indicates elevated detection limit due to sample interference.  
NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less than  
> = Greater than

Analysis Summary:

Samples Collected: 07-26-89  
Samples Prepared: 07-29, 31-89  
Samples Analyzed: 08-07-89

*Carter Nulton*  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

*8/21/89*  
DATE



NOTE: Non-quantitative recoveries were obtained for nitrobenzene during these analysis. Modifications made to Method LW02 to analyze MM-5 samples resulted in the loss of nitrobenzene during analysis. Although certified detection limits have been reported, it is likely that actual detection limits are higher than the detection limits reported.

WESTON ANALYTICS  
AIR EXPLOSIVES DATA

RFW Batch Number: 8907L187

CLIENT: USATHAMA-HAWTHORNE

Page: 1

Sample Information	Client		T2-3		T2-3		Total ug		Total ug	
	ID :	FCO	AO	023	BLANK	1.0	Total ug	1	Total ug	20XSS
	RFW#:	022								1
	D.F.:	2.5								
	Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMX.....		8.26G	< 1.27	< 1.27	< 1.27	< 1.27	< 1.27	< 1.27	< 1.27	20.8(81.5%)
RDX.....		< 2.45	2.92G	< 0.98	< 0.98	< 0.98	< 0.98	< 0.98	< 0.98	15.8(80.6%)
1,3,5-TNB.....		< 5.23	< 2.09	< 2.09	< 2.09	< 2.09	< 2.09	< 2.09	< 2.09	29.1(69.6%)
1,3-DNB.....		6.64G	3.05G	< 0.59	< 0.59	< 0.59	< 0.59	< 0.59	< 0.59	6.24(52.9%)
NITROBENZENE.....		< 1.05	< 0.42	< 0.42	< 0.42	< 0.42	< 0.42	< 0.42	< 0.42	< 0.42(0.0%)
TETRYL.....		< 12.5	< 5.00	< 5.00	< 5.00	< 5.00	< 5.00	< 5.00	< 5.00	53.4(53.4%)
2,4,6-TNT.....		93.6	< 1.92	< 1.92	< 1.92	< 1.92	< 1.92	< 1.92	< 1.92	21.0(54.7%)
2,6-DNT.....		< 1.00	< 0.40	< 0.40	< 0.40	< 0.40	< 0.40	< 0.40	< 0.40	2.56(32.0%)
2,4-DNT.....		< 1.05	< 0.42	< 0.42	< 0.42	< 0.42	< 0.42	< 0.42	< 0.42	4.41(52.5%)

Sample Information	Client		100XSS		100XSSD		Total ug		Total ug	
	ID :	RFW#:	D.F.:	Units:	1	1	Total ug	1	Total ug	1
HMX.....							99.2(78.1%)		109(85.8%)	
RDX.....							80.8(82.4%)		84.0(85.7%)	
1,3,5-TNB.....							158(75.6%)		157(75.1%)	
1,3-DNE.....							41.7(70.6%)		39.4(66.8%)	
NITROBENZENE.....							1.26(3.00%)		4.27(10.2%)	
TETRYL.....							322(64.4%)		330(66.0%)	
2,4,6-TNT.....							126(65.6%)		124(64.5%)	
2,6-DNT.....							17.7(44.2%)		16.3(40.8%)	
2,4-DNT.....							26.6(63.3%)		24.6(58.6%)	

G=Elevated

**STACK TEST 3**  
**500°F/36 HOURS**  
**ANALYTICAL DATA SUMMARY**

1311R2

**WILSON**

ROY F. TESTON, INC.  
Lienville Laboratory

CLIENT: USATHAMAHWAAP  
SAMPLES RECEIVED: 7-19, 20, 8-1  
REF#: 3907L060,078,153, 137  
3908L202  
W.O.#: 2231-08-02

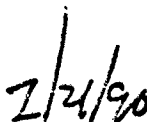
INORGANIC NARRATIVE

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.



Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lienville Analytical Laboratory

  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CLP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

## ROY F. WESTON INC.

## INORGANICS DATA SUMMARY REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
 WORK ORDER: 2291-03-04-0000

WESTON BATCH #: 390/L060

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-027	UH-PART-FCO-BHW-T3-1	NITRATED ESTERS	26200	UG	5250
-028	UH-PART-FCO-BHA-T3-1	NITRATED ESTERS	9980	UG	1720
-029	UH-PART-AO-FHA-T3-L1	PARTICULATE	0.0009	grams	0.0000
-030	UH-PART-AO-FILT-T3-1	PARTICULATE	0.0016	grams	0.0000
-031	UH-PART-AO-BHW-T3-1	NITRATED ESTERS	3650	UG	3500
-032	UH-PART-AO-BHA-T3-1	NITRATED ESTERS	300 u	UG	800
-035	UH-PART-FCO-BHW-T3-2	NITRATED ESTERS	8330	UG	1900
-036	UH-PART-FCO-BHA-T3-2	NITRATED ESTERS	1860 u	UG	1880
-037	UH-PART-AO-FHA-T3-2	PARTICULATE	0.0030	grams	0.0000
-038	UH-PART-AO-FLT-T3-2	PARTICULATE	0.0019	grams	0.0000
-039	UH-PART-AO-BHW-T3-2	NITRATED ESTERS	2670	UG	2620
-040	UH-PART-AO-BHA-T3-2	NITRATED ESTERS	500 u	UG	500
-045	UH-BLK-FILT-PART	PARTICULATE	0.0001	grams	0.0000
-046	UH-BLK-ACETONE-PART	PARTICULATE	0.0000	grams	0.0000
-047	UH-BLK-PART-WATER	NITRATED ESTERS	975 u	UG	975
-053	COMP FCO PART T3-1	NITRATED ESTERS	12.7	UG	10.0
-054	COMP AO PART T3-1	NITRATED ESTERS	12.9	UG	10.0
-055	COMP FCO PART T3-2	NITRATED ESTERS	10.0 u	UG	10.0
-056	COMP AO PART T3-2	NITRATED ESTERS	11.4	UG	10.0
-057	COMP OF PART BLANK	NITRATED ESTERS	10.0 u	UG	10.0

## ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/15/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-03-04-0000

WESTON BATCH #: 3907L061

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC004-MB1	NITRATED ESTERS	5.0	u MG/L	5.
BLANK20	89LNC004-MB2	NITRATED ESTERS	5.0	u MG/L	5.
BLANK10	89LNC006-MB1	NITRATED ESTERS	5.0	u MG/L	5.
BLANK20	89LNC006-MB2	NITRATED ESTERS	5.0	u MG/L	5.

## ROY F. WESTON INC.

## INORGANICS ACCURACY REPORT 02/16/90

CLIENT: USATHAMA-RVAAP  
WORK ORDER: 2231-03-04-0000

WESTON BATCH #: 8907LC50

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC004-MB1	NITRATED ESTERS	10.9	5.0 u	10.0	109
BLANK20	89LNC004-MB2	NITRATED ESTERS	47.8	5.0 u	50.0	95.5
		NITRATED ESTERS	47.9	5.0 u	50.0	95.9
BLANK10	89LNC006-MB1	NITRATED ESTERS	9.0	5.0 u	10.0	90.0
BLANK20	89LNC006-MB2	NITRATED ESTERS	46.7	5.0 u	50.0	93.3
		NITRATED ESTERS	48.9	5.0 u	50.0	97.7



ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/15/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-03-04-0000

WESTON BATCH #: 8907106

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC004-MB2	NITRATED ESTERS	95.5	95.9	0.30
BLANK20	89LNC006-MB2	NITRATED ESTERS	93.3	97.7	4.6

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/16/50

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2281-08-04-0000

WESTON BATCH #: 3907L073

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-015	UH-FCO-PART-BHW-T3-3	NITRATED ESTERS	8080	UG	3120
-016	UH-FCO-PART-BHA-T3-3	NITRATED ESTERS	1120	u UG	1120
017	UH-AO-PART-FHA-T3-3	PARTICULATE	0.0033	grams	0.0000
-018	UH-AO-PART-FILT-T3-3	PARTICULATE	0.0024	grams	0.0000
-019	UH-AO-PART-BHW-T3-3	NITRATED ESTERS	6200	UG	3450
-020	UH-AO-PART-BHA-T3-3	NITRATED ESTERS	1200	u UG	1200
-021	UH-PT-FCO-PRE-H2O	NITRATED ESTERS	725	u UG	725
-022	UH-PT-FCO-PRE-ACE	NITRATED ESTERS	1250	u UG	1250
-023	UH-PT-AO-PRE-H2O	NITRATED ESTERS	600	u UG	600
-024	UH-PT-AO-PRE-ACE	NITRATED ESTERS	975	u UG	975
-031	COMP FLO PT T3-3	NITRATED ESTERS	11.5	UG	10.0
-032	COMP AO PT T3-3	NITRATED ESTERS	10.0	u UG	10.0

## ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2291-08-04-0000

WESTON BATCH #: 3907L078

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC004-MB1	NITRATED ESTERS	5.0	u MG/L	5.
BLANK20	89LNC004-MB2	NITRATED ESTERS	5.0	u MG/L	5.
BLANK10	89LNC006-MB1	NITRATED ESTERS	5.0	u MG/L	5.
BLANK20	89LNC006-MB2	NITRATED ESTERS	5.0	u MG/L	5.

ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/16/90

CLIENT: USATHAMA-HVAAP  
WORK ORDER: 2291-08-04-0000

WESTON BATCH #: 8907L078

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%RECOV
BLANK10	89LNC004-MB1	NITRATED ESTERS	10.9	5.0 u	10.0	109
BLANK20	89LNC004-MB2	NITRATED ESTERS	47.3	5.0 u	50.0	95.5
		NITRATED ESTERS	47.9	5.0 u	50.0	95.9
BLANK10	89LNC006-MB1	NITRATED ESTERS	9.0	5.0 u	10.0	90.0
BLANK20	89LNC006-MB2	NITRATED ESTERS	46.7	5.0 u	50.0	93.3
		NITRATED ESTERS	48.9	5.0 u	50.0	97.7

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-03-04-0000

WESTON BATCH #: 3907L01

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	89LNC004-MB2	NITRATED ESTERS	95.5	95.3	0.20
BLANK20	89LNC006-MB2	NITRATED ESTERS	93.3	97.7	4.6



ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HAWTHORNE  
RFW #: 3907L060, Air  
W.O. #: 2281-08-04

SAMPLES RECEIVED: 07-19-89

#### EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of MM-5 samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

<u>Abbreviation</u>	<u>Description</u>
---------------------	--------------------

BLK	= Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.
-----	---

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS	= Designates sample spiked with target compound.
SSD	= Designates sample spiked with target compound in duplicate.
D	= Indicates duplicate analysis of a sample.
NS	= Not spiked.
DL	= Diluted below calibration range.
G	= Indicates elevated detection limit due to sample interference.
NR	= Not reported.

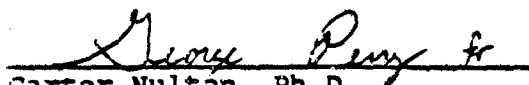
NOTE: Spikes have been reported as result (% recovery).

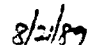
#### Data Qualifiers

<	= Less than
>	= Greater than

#### Analysis Summary:

Samples Collected: 07-17-89  
Samples Prepared: 07-20-89  
Samples Analyzed: 08-07-89

  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

  
DATE

NOTE: Non-quantitative recoveries were obtained for nitrobenzene during these analysis. Modifications made to Method LW02 to analyze MM-5 samples resulted in the loss of nitrobenzene during analysis. Although certified detection limits have been reported, it is likely that actual detection limits are higher than the detection limits reported.

**RFW Batch Number: 8907L060**

**CLIENT:**

**USA'THAMA-HAWTHORNE**

Page: 1

## Sample Information

client  
ID :  
REFW#:  
D.F.:  
Units:

T3-1  
FCO  
048  
2500  
Total

T3-1  
AO  
049  
1.0  
Total

T3-2	FCO	C50	25	Total
------	-----	-----	----	-------

T3-2  
AO  
051  
1.0  
Total

BLANK	052
	1.0
	Total

BLANK 1.0  
Total

HMX.....  
 RDX.....  
 1,3,5-TNB.....  
 1,3-DNB.....  
 NITROBENZENE.....  
 TETRYL.....  
 2,4,6-TNT.....  
 2,6-DNT.....  
 2,4-DNT.....

3180	<
2450	<
5230	<
1480	<
1050	<
12,500	<
89,200	<
1000	<
1050	<

1.27	<
3.81G	<
2.09	<
5.60G	<
0.42	<
5.00	<
1.92	<
0.40	<
0.42	<

31.8	<	3
24.5		3
52.3		8
14.8		2
10.5	<	
125	<	
64.2	<	
10.0	<	
10.5	<	

1.27	<	1
3.82G	<	0
3.46G	<	2
8.40G	<	0
20.2G	<	0
5.00	<	5
1.92	<	1
0.40	<	0
0.42	<	0

1.27	<	1.
0.98	<	0.
2.09	<	2.
0.59	<	0.
0.42	<	0.
5.00	<	5.
1.92	<	1.
0.40	<	0.
0.42	<	0.

**Sample Information**

---  
20XSS  
1  
Total ug

100XSS  
1  
Total ug

10 To

100XSSD  
1  
Total ug

HMX.....  
 RDX.....  
 1,3,5-TNB.....  
 1,3-DNB.....  
 NITROBENZENE.....  
 TETRYL.....  
 2,4,6-TNT.....  
 2,6-DNT.....  
 2,4-DNT.....

26.7(105%)  
20.2(103%)  
44.9(107%)  
11.4(96.6%)  
0.42(0.0%)  
94.4(94.4%)  
35.7(92.9%)  
7.46(93.2%)  
7.96(94.8%)

124 (97.6%)  
99.2 (101%)  
213 (102%)  
58.3 (98.8%)  
16.2 (38.6%)  
475 (95.0%)  
185 (96.3%)  
40 (100%)  
40.3 (96.0%)

13  
10  
21  
53  
47  
18  
35  
38

130(102%)  
100(102%)  
210(100%)  
53.4(90.5%)  
0.42(0.0%)  
472(94.4%)  
187(97.4%)  
35.7(89.3%)  
38.3(91.1%)

## G-Elevated



**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HAWTHORNE  
RFW #: 9907L073, Air  
W.O. #: 2231-08-04

SAMPLES RECEIVED: 07-19-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of MM-5 samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.  
SSD = Designates sample spiked with target compound in duplicate.  
D = Indicates duplicate analysis of a sample.  
NS = Not spiked.  
DL = Diluted below calibration range.  
G = Indicates elevated detection limit due to sample interference.  
NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

Data Qualifiers

< = Less than  
> = Greater than

Analysis Summary:

Samples Collected: 07-18-89  
Samples Prepared: 07-21-89  
Samples Analyzed: 08-07-89

George Perry Jr.  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

8/21/89  
DATE

NOTE: Non-quantitative recoveries were obtained for nitrobenzene during these analysis. Modifications made to Method LW02 to analyze MM-5 samples resulted in the loss of nitrobenzene during analysis. Although certified detection limits have been reported, it is likely that actual detection limits are higher than the detection limits reported.

WESTON ANALYTICS  
AIR EXPLOSIVES DATA

RFW Batch Number: 3907L078

CLIENT: USATHANA-HAWTHORNE

Page: 1

Client ID : T3-3 AO  
RFW# : 1-6 COM. BLANK  
D.Y. : 10 1.0  
Units: Total ug Total ug Total ug

HNX.....	< 12.7	< 1.27	< 1.27	28.4(111%)
RDX.....	< 9.80	2.80G	< 0.98	23.5(120%)
1,3,5-TNB.....	21.7G	2.78G	< 2.09	47.9(115%)
1,3-DNB.....	< 5.90	5.37G	< 0.59	10.4(36.1%)
NITROBENZENE.....	22.0G	< 0.42	< 0.42	0.42(0.0%)
TETRYL.....	< 50.0	< 5.00	< 5.00	111(111%)
2,4,6-TNT.....	171	< 1.92	< 1.92	40.1(104%)
2,6-DNT.....	< 4.00	< 0.40	< 0.40	6.49(81.1%)
2,4-DNT.....	< 4.20	< 0.42	< 0.42	7.79(92.7%)

20XSS  
1.0  
Total ug

Client ID :  
RFW# :  
D.F. :  
Units:

100XSS  
1  
Total ug

100XSS  
1  
Total ug

HNX.....	135(106%)
RDX.....	110(112%)
1,3,5-TNB.....	226(108%)
1,3-DNB.....	61.3(104%)
NITROBENZENE.....	8.80(21.0%)
TETRYL.....	528(106%)
2,4,6-TNT.....	195(102%)
2,6-DNT.....	40.1(100%)
2,4-DNT.....	42.0(100%)

131(103%)
105(107%)
213(102%)
55.4(93.9%)
6.00(14.3%)
496(99.2%)
178(97.2%)
35.8(89.5%)
38.5(91.7%)

G-Elevated

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMA - HAWTHORNE      SAMPLES RECEIVED: 07-19-89  
RFW #: 8907L060, GC/MS SEMIVOLATILE  
W.O.#: 2281-08-02

NARRATIVE

The set of samples consisted of three HPLC extracts prepared on 07-28-89.

The samples were analyzed by GC/MS for HSL Semivolatile target compounds on 09-06-89.

The following is a summary of the QC results accompanying these sample results and a description of any problems encountered during their analysis:

1. The reported results should be considered qualitative only. Concentrations are not reported for the Tentatively Identified Compounds (TIC's).
2. The samples contained a variety of unknowns and a large unresolved complex of hydrocarbons and fatty acids (C14 and greater). Sample FCO-T3-1 contained higher levels than sample AO-T3-1.

Cm-L  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

9/13/89  
DATE

Roy F. Weston, Inc. - Lionville Laboratory  
DNA ANALYTICAL DATA PACKAGE FOR  
USATHAMA-HWAAP

DATE RECEIVED: 07/19/89

RFW LOT # :3907L060

CLIENT ID	RFW #	MTX	PREP #	COLLECTION	EXTR/PREP	ANALYSIS
COMP-FCO-EXP-T3-1	048	AI	89LE0826	07/18/89	07/28/89	09/06/89
COMP AO-EXP-T3-1	049	AI	89LE0826	07/17/89	07/28/89	09/06/89
COMP BLK-EXP	052	AI	89LE0826	07/18/89	07/28/89	09/06/89

Cust ID: COMP-FOO-EXP   
 COMP AO-EXP-   
 COMP BLK-EXP

Sample Information     
 Ref#: 048     
 049     
 052  
 Matrix: AIR     
 AIR     
 AIR  
 D.F.: 1.00     
 1.00     
 1.00  
 Units: total ug     
 total ug     
 total ug

Surrogate	Matrix	Ref#	048	049	052
Recovery					
Nitrobenzene-d5			NS	NS	NS
2-Fluorobiphenyl			NS	NS	NS
p-Terphenyl-d14			NS	NS	NS
Phenol-d5			NS	NS	NS
2-Fluorophenol			NS	NS	NS
2,4,6-Trichlorophenol			NS	NS	NS
Phenol		64	3	20	20
bis(2-Chloroethyl)ether		20	20	20	20
2-Chlorophenol		20	20	20	20
1,3-Dichlorobenzene		20	20	20	20
1,4-Dichlorobenzene		20	20	20	20
Benzyl alcohol		20	20	20	20
1,2-Dichlorobenzene		20	20	20	20
2-Methylphenol		20	20	20	20
bis(2-Chloroisopropyl)ether		20	20	20	20
4-Methylphenol		20	20	20	20
N-Nitroso-Di-n-propylamine		20	20	20	20
Hexachloroethane		20	20	20	20
Nitrobenzene		20	20	20	20
Isophorone		20	20	20	20
2-Nitrophenol		20	20	20	20
2,4-Dimethylphenol		20	20	20	20
benzoic acid		20	20	20	100
bis(2-Chloroethoxy)methane		20	20	20	20
2,4-Dichlorophenol		20	20	20	20
1,2,4-Trichlorobenzene		20	20	20	20
naphthalene		42	15	20	20
4-Chloroaniline		20	20	20	20
Hexachlorobutadiene		20	20	20	20
4-Chloro-3-methylphenol		20	20	20	20
2-Methylnaphthalene		11	20	20	20
Hexachlorocyclopentadiene		20	20	20	20

\* Outside of EPA CLP GC limits.

Ref:

046

049

052

2,4,6-Trichlorophenol	20 U	20 U	20 U
2,4,5-Trichlorophenol	100 U	100 U	100 U
2-Chloronaphthalene	20 U	20 U	20 U
2-Nitroaniline	100 U	100 U	100 U
Dimethylphthalate	20 U	20 U	20 U
Acenaphthylene	20 U	20 U	20 U
2,6-Dinitrotoluene	20 U	20 U	20 U
3-Nitroaniline	100 U	100 U	100 U
Acenaphthene	20 U	20 U	20 U
2,4-Dinitrophenol	100 U	100 U	100 U
4-Nitrophenol	100 U	100 U	100 U
Dibenzofuran	20 U	20 U	20 U
2,4-Dinitrotoluene	270 U	20 U	20 U
Diethylphthalate	20 U	140 U	4 U
4-Chlorophenyl-phenylether	20 U	20 U	20 U
Fluorene	20 U	20 U	20 U
4-Nitroaniline	100 U	100 U	100 U
4,6-Dinitro-2-Methylphenol	100 U	100 U	100 U
N-Nitrosodiphenylamine (1)	20 U	20 U	20 U
4-Bromophenyl-phenylether	20 U	20 U	20 U
Hexachlorobenzene	20 U	20 U	20 U
Pentachlorophenol	100 U	100 U	100 U
Phenanthrene	20 U	20 U	20 U
Anthracene	20 U	20 U	20 U
Di-n-Butylphthalate	82 U	68 U	7 U
Fluoranthene	20 U	20 U	20 U
Pyrene	20 U	20 U	20 U
Butylbenzylphthalate	20 U	5 U	2 U
2,3'-Dichlorobenzidine	40 U	40 U	40 U
Benzo(a)anthracene	20 U	20 U	20 U
Chrysene	20 U	20 U	20 U
Bis(2-ethylhexyl)phthalate	29 U	40 U	11 U
Di-n-Octyl phthalate	2 U	4 U	20 U
Benzo(b)fluoranthene	20 U	20 U	20 U
Benzo(k)fluoranthene	20 U	20 U	20 U
Benzo(a)pyrene	20 U	20 U	20 U
Indeno(1,2,3-cd)pyrene	20 U	20 U	20 U
Dibenzo(a,h)anthracene	20 U	20 U	20 U
Benzo(g,h,i)perylene	20 U	20 U	20 U

(1) - Cannot be separated from Diphenylamine. \* = Outside of EPA CLP QC limits.

17  
 SEMI-VOLATILE ORGANIC ANALYSIS SHEET  
 POSITIVELY IDENTIFIED COMPOUNDS

CLIENT SAMPLE NO.

COMP-PCO-KIP-F3-1

Lab Name: Roy Z. Weston, Inc. Work Order: 2281-08-02-0000

Client: DEATHAMA-HEAP

Matrix: AIR

Lab Sample ID: 9907L060-048

Sample wt/vol: (g/mL)

Lab File ID: 8090605

Level: (low/med) LOW

Date Received: 07/19/89

% Moisture: not dec. dec.

Date Extracted: 07/28/89

Extraction: (SepF/Cont/Sonc)

Date Analyzed: 09/06/89

GPC Cleanup: (Y/N) N pH:

Dilution Factor: 1.00

Number TICs found: 22

CONCENTRATION UNITS:  
 (ug/L or ug/Kg) total ug

CAS NUMBER	COMPOUND NAME	RT	EST. CONC.	Q
1.	TNT	16.35	NA	
2.	TNT	16.53	NA	
3.	UNKNOWN	18.18	NA	
4.	FATTY ACID	18.60	NA	
5.	PHTHALATE	18.73	NA	
6.	UNKNOWN	19.00	NA	
7.	UNKNOWN	19.17	NA	
8.	FATTY ACID	19.58	NA	
9.	UNKNOWN	19.65	NA	
10.	UNKNOWN	19.72	NA	
11.	UNKNOWN	19.85	NA	
12.	FATTY ACID	2 NAO	NA	
13.	UNKNOWN	20.17	NA	
14.	UNKNOWN	20.87	NA	
15.	UNKNOWN	21.05	NA	
16.	UNKNOWN	21.33	NA	
17.	UNKNOWN	21.45	NA	
18.	ALKANE	22.03	NA	
19.	UNKNOWN	22.58	NA	
20.	ALKANE	24.83	NA	
21.	UNKNOWN	25.38	NA	
22.	UNKNOWN	25.77	NA	



17  
SEMI-VOLATILE ORGANICS ANALYSIS REPORT  
PRELIMINARILY IDENTIFIED COMPOUNDS

CLIENT SAMPLE NO.

Lab Name: ROY F. Weston, Inc. Work Order: 2281-08 JA-0000

CCMP AO-ZXP-T3-1

Client: NEATHAMA-SWAAP

Matrix: AIR

Lab Sample ID: 9907L060-049

Sample wt/vol:            (g/mL)           

Lab File ID: 3090604

Level: (low/med) LOW

Date Received: 07/19/99

% Moisture: not dec.            dec.           

Date Extracted: 07/28/99

Extraction: (SepF/Cont/Sonc)           

Date Analyzed: 09/06/99

GPC Cleanup: (Y/N) N pH:           

Dilution Factor: 1.00

CONCENTRATION UNITS:

Number TICs found: 21

(ug/L or ug/Kg) total ug

CAS NUMBER	COMPOUND NAME	RT	EST. CONC.	Q
1.	UNKNOWN	6.82	NA	
2.	UNKNOWN	7.28	NA	
3.	C4 BENZENE	7.72	NA	
4.	UNKNOWN	8.95	NA	
5.	UNKNOWN	9.23	NA	
6.	UNKNOWN	10.25	NA	
7.	UNKNOWN	10.43	NA	
8.	BENZAMIDE	11.38	NA	
9.	ETHYLBENZOIC ACID	11.55	NA	
10.	ETHYLBENZOIC ACID	11.72	NA	
11.	UNKNOWN	17.58	NA	
12.	FATTY ACID	18.50	NA	
13.	UNKNOWN	19.22	NA	
14.	UNKNOWN	19.90	NA	
15.	FATTY ACID ESTER	19.98	NA	
16.	UNKNOWN	21.47	NA	
17.	UNKNOWN	22.18	NA	
18.	UNKNOWN	22.32	NA	
19.	UNKNOWN	23.15	NA	
20.	UNKNOWN	24.47	NA	
21.	UNKNOWN	25.37	NA	

17  
 SEMI-VOLATILE ORGANICS ANALYSIS SHEET  
 TENTATIVELY IDENTIFIED COMPOUNDS

CLIENT SAMPLE NO.

COMP BLX-EXP

Lab Name: Ray F. Weston, Inc. Work Order: 2281-08-02-0000

Client: SEATEMA-SWAAP

Matrix: AIR

Lab Sample ID: 89071060-052

Sample wt/vol:        (g/mL)       

Lab File ID: 6090603

Level: (low/med) LOW

Date Received: 07/19/89

% Moisture: not dec.        dec.       

Date Extracted: 07/28/89

Extraction: (SepF/Cont/Sonc)       

Date Analyzed: 09/06/89

GPC Cleanup: (Y/N) N pH:       

Dilution Factor: 1.00

Number TICs found: 12

CONCENTRATION UNITS:  
 (ug/L or ug/Kg) total ug

CAS NUMBER	COMPOUND NAME	RT	EST. CONC.	Q
1.	UNKNOWN	14.20	NA	
2.	UNKNOWN	19.77	NA	
3.	UNKNOWN	22.53	NA	
4.	UNKNOWN	23.40	NA	
5.	UNKNOWN	23.48	NA	
6.	UNKNOWN	23.55	NA	
7.	UNKNOWN	23.73	NA	
8.	UNKNOWN	23.82	NA	
9.	UNKNOWN	23.93	NA	
10.	UNKNOWN	24.45	NA	
11.	UNKNOWN	24.48	NA	
12.	UNKNOWN	24.78	NA	

July 1990  
Revision: Final

STACK TEST 5  
500°F/24 HOURS  
ANALYTICAL DATA SUMMARY

1311R2

**WESTON**

ROY F. WESTON, INC.  
Lionville Laboratory

CLIENT: USATHAMAHWAAP  
SAMPLES RECEIVED: 7-19, 20, 8-1  
RW#: 3907L060, 073, 158, 137  
3908L202  
W.O.#: 2231-08-02

**INORGANIC NARRATIVE**

The following is a summary of the quality control results and a description of any problems encountered during the analysis of this batch of samples:

1. All sample holding times as required by 40CFR136 were met for water samples. Note: Holding times for soil samples have not been promulgated by the USEPA.
2. All preparation blanks were analyzed below the required detection limit.
3. All calibration verification checks were within the required control limits of 90-100%. Calibration verification is performed using independent standards.
4. All laboratory control standards (blank spikes) were within the control limits of 80-120%.
5. The methodology used to analyze these samples for nitrocellulose and nitroglycerine is not specific enough to resolve these compounds as separate analytes. The data have been averaged together and reported as nitrated esters.



Jack R. Tuschall, Ph.D.  
Laboratory Manager  
Lionville Analytical Laboratory

  
Date

ROY F. WESTON, INC.

GLOSSARY OF TERMS - INORGANIC REPORTS

DATA QUALIFIERS

- U - Indicates that the parameter was not detected at or above the reported limit. The associated numerical value is the sample detection limit.
- \* - Indicates that the original sample result is greater than 4x the spike amount added. The USEPA-CIP has determined that spike results on samples where this occurs may be unreliable and, therefore, the control limits are not applicable.

ABBREVIATIONS

- MB - Method or preparation blank.
- MS - Matrix Spike.
- MSD - Matrix Spike Duplicate.
- REP - Sample Replicate.
- LC - Indicates a method LCS or Blank Spike.
- NC - Not calculable, result below the detection limit.

LABORATORY CHRONOLOGY AND HOLDTIME REPORT

The test code listed indicates the specific analysis or preparation procedure employed. The codes may be interpreted as follows:

- MAAW - Metals prep test for AA digestion, water matrix.
- MAAS - Metals prep test for AA digestion, soil matrix.
- MICW - Metals prep test for ICP digestion, water matrix.
- MICS - Metals prep test for ICP digestion, soil matrix.
- M\*\*TO- This type of code indicates a total metal analysis (eg. MAGTO indicates an analysis for total silver).
- M\*\*SO- This type of code indicates a soluble metal analysis. (eg. MAGSO indicates an analysis for soluble silver).
- M\*\*EP- This type of code indicates an EPTOXICITY metals analysis (eg. MAGEP indicates an analysis for eptox silver).
- I\*\*TO- This type of code indicates a non-metallic total analysis. There is also a complimentary soluble analysis for each of these codes (eg. ICNTO indicates an analysis for total cyanide).

A suffix of -R or -S following these codes indicates a replicate or spike analysis respectively.

ROY F. WESTON INC.

INORGANICS DATA SUMMARY REPORT 02/16/90

CLIENT: USATHAMA-NHAAP  
WORK ORDER: 2231-08-04-0000

WESTON BATCH #: 8903L202

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
-003	UH-FCO-PART-BHW T5-1	NITRATED ESTERS	17800	UG	1120
-004	UH-FCO-PART-BHA T5-1	NITRATED ESTERS	6050	UG	950
-005	UH-FCO-PART-FHA T5-1	PARTICULATE	0.0043	grams	0.0000
-006	UH-AO-PART-FILT T5-1	PARTICULATE	0.0015	grams	0.0000
-007	UH-AO-PART-BHW T5-1	NITRATED ESTERS	2240	UG	1550
-008	UH-AO-PART-BHA T5-1	NITRATED ESTERS	238	u UG	288
-023	UH-FCO-PART-BHW T5-2	NITRATED ESTERS	1340	UG	1180
-024	UH-FCO-PART-BHA T5-2	NITRATED ESTERS	238	u UG	238
-025	UH-AO-PART-FHA T5-2	PARTICULATE	0.0025	grams	0.0000
-026	UH-AO-PART-FILT T5-2	PARTICULATE	0.0005	grams	0.0000
-027	UH-AO-PART-BHW T5-2	NITRATED ESTERS	1820	u UG	1820
-028	UH-AO-PART-BHA T5-2	NITRATED ESTERS	750	u UG	750
-029	UH-BLK TRAIN FHA T5-	PARTICULATE	0.0007	grams	0.0000
-030	UH BLK TRAIN BHAT5-	PARTICULATE	0.0001	grams	0.0000
-031	UHBLK TRAIN BHW T5-2	NITRATED ESTERS	688	u UG	688
-032	UHBLK TRAIN BHA T5-2	NITRATED ESTERS	225	u UG	225
-047	UH-FCO-PART-BHW T5-3	NITRATED ESTERS	1060	UG	1080
-048	UH-FCO-PART-BHA T5-3	NITRATED ESTERS	462	u UG	462
-049	UH-AO-PART-FHA T5-3	PARTICULATE	0.0016	grams	0.0000
-050	UH-AO-PART-FILT T5-3	PARTICULATE	0.0000	grams	0.0000

ROY F. NESTON INC.

INORGANICS DATA SUMMARY REPORT 02/16/00

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-08-04-0000

NESTON BATCH #: 8908L20

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORT LIMIT
-051	UH-AO-PART-BHW T5-3	NITRATED ESTERS	1220	u UG	1220
-052	UH-AO-PART-BHA T5-3	NITRATED ESTERS	138	u UG	138
-065	COMP-FLO-PT-T5-1	NITRATED ESTERS	5.0	u UG	5.
-066	COMP-AO-PT-T5-1	NITRATED ESTERS	5.0	u UG	5.
-069	COMP FLO-PT-T5-2	NITRATED ESTERS	5.0	u UG	5.
-070	COMP AO-PT-T5-2	NITRATED ESTERS	5.0	u UG	5.
-071	COMP-BT-PT	NITRATED ESTERS	5.0	u UG	5.
-074	COMP FLO-PT-T5-3	NITRATED ESTERS	5.0	u UG	5.
-075	COMP AG-PT-T5-3	NITRATED ESTERS	5.0	u UG	5.

ROY F. WESTON INC.

INORGANICS METHOD BLANK DATA SUMMARY PAGE 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-08-04-0000

WESTON BATCH #: 8908LE02

SAMPLE	SITE ID	ANALYTE	RESULT	UNITS	REPORTING LIMIT
BLANK10	89LNC008-MB1	NITRATED ESTERS	2.5 u	MG/L	2.5
BLANK20	89LNC008-MB2	NITRATED ESTERS	2.5 u	MG/L	2.5



ROY F. WESTON INC.

INORGANICS ACCURACY REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-08-04-0000

WESTON BATCH #: 8908L20

SAMPLE	SITE ID	ANALYTE	SPIKED SAMPLE	INITIAL RESULT	SPIKED AMOUNT	%REC
BLANK10	89LNC009-MB1	NITRATED ESTERS	10.3	2.5 u	10.0	100
BLANK20	89LNC009-MB2	NITRATED ESTERS	49.6	2.5 u	50.0	99
		NITRATED ESTERS	49.5	2.5 u	50.0	99

ROY F. WESTON INC.

INORGANICS DUPLICATE SPIKE REPORT 02/16/90

CLIENT: USATHAMA-HWAAP  
WORK ORDER: 2231-08-04-0000

WESTON BATCH #: 8902L202

SAMPLE	SITE ID	ANALYTE	SPIKE#1 %RECOV	SPIKE#2 %RECOV	%DIFF
BLANK20	69LNC008-MB2	NITRATED ESTERS	99.3	99.0	0.20

**WESTON**

ROY F. WESTON, INC.  
Lionsville Laboratory

CLIENT: USATHAMA -- HAWTHORNE  
RFW #: 8907L202, Air  
W.O.#: 2231-08-04

SAMPLES RECEIVED: 03-01-89

EXPLOSIVE NARRATIVE

Samples have been prepared and analyzed according to USATHAMA Method LW02, Explosives in Soil, modified for the analysis of MM-5 samples.

The following QA/QC control samples have been analyzed concurrently with each extraction batch. Abbreviations noted below have been used in the data summary.

Abbreviation

Description

BLK = Reagent blank analyzed to provide an indication of lab contamination and its' effect on reported analytical data.

Samples (soil or water) are spiked with target compounds to provide precision and accuracy data.

SS = Designates sample spiked with target compound.

SSD = Designates sample spiked with target compound in duplicate.

D = Indicates duplicate analysis of a sample.

NS = Not spiked.

DL = Diluted below calibration range.

G = Indicates elevated detection limit due to sample interference.

NR = Not reported.

NOTE: Spikes have been reported as result (% recovery).

NOTE: Results for T5-1 FCO represent a minimum value as the front half XAD sample was broken during sample preparation. Observations indicate that the majority of explosives have been contained in the front half solvent rinse for Hawthorne MM-5 explosives in air samples.

Data Qualifiers

< = Less than  
> = Greater than

NOTE: Non-quantitative recoveries were obtained for nitrobenzene during these analysis. Modifications made to Method LW02 to analyze MM-5 samples resulted in the loss of nitrobenzene during analysis. Although certified detection limits have been reported, it is likely that actual detection limits are higher than the detection limits reported.

Analysis Summary:

Samples Collected: 07-29,30-89

Samples Prepared: 08-02-89

Samples Analyzed: 08-10-89

George Perry  
Carter Nulton, Ph.D.  
Vice President/Laboratory Manager  
Lionville Analytical Laboratory

8/31/89

DATE

WESTON ANALYTICS  
AIR EXPLOSIVES DATA

RFW Batch Number: 8907L202

CLIENT:

USATHAMA-HAWTHORNE

Page: 1

Sample Information	Client	T5-1	T5-1	T5-2	T5-2	T5-3	T5-3	Total ug	Total ug	Total ug
	ID :	FCO	FCO	FCO	FCO	FCO	FCO			
	RFW#:	67	68	72	72	73	76			
	D.F.:	1875	1	100	100	1	10			
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMx.....	< 2380	12.7G	< 127	< 127	1.47G	< 12.7	< 12.7	< 1.27	< 1.27	< 1.27
RDX.....	< 1840	2.76G	< 98.0	< 98.0	2.57G	< 9.80	< 9.80	< 2.84G	< 2.84G	< 2.84G
1,3,5-TNB.....	< 3920	< 2.09	< 209	< 209	2.19G	< 20.9	< 20.9	< 7.62G	< 7.62G	< 7.62G
1,3-DNB.....	< 1110	2.63G	< 59.0	< 59.0	7.60G	< 5.90	< 5.90	< 1.90G	< 1.90G	< 1.90G
NITROBENZENE.....	< 788	< 0.42	< 42.0	< 42.0	1.56G	< 4.20	< 4.20	< 1.91G	< 1.91G	< 1.91G
TETRYL.....	< 9380	< 5.00	< 500	< 500	< 5.00	< 50.0	< 50.0	< 5.00	< 5.00	< 5.00
2,4,6-TNT.....	76,800	< 1.92	677	677	< 1.92	184	< 1.92	< 1.92	< 1.92	< 1.92
2,6-DNT.....	< 750	< 0.40	< 40	< 40	< 0.40	< 4.00	< 4.00	< 0.40	< 0.40	< 0.40
2,4-DNT.....	< 780	< 0.42	< 42	< 42	< 0.42	< 4.20	< 4.20	< 0.42	< 0.42	< 0.42

Sample Information	Client	BLANK	20XSS	100XSS	100XSSD	Total ug	Total ug
	ID :	1	1	1	1		
	RFW#:	1	1	1	1		
	D.F.:	1	1	1	1		
Units:	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug	Total ug
HMx.....	< 1.27	24.2(95.3%)	126(99.2%)	126(99.2%)	126(99.2%)	126(99.2%)	126(99.2%)
RDX.....	< 0.98	20.2(103%)	106(108%)	106(108%)	106(108%)	106(108%)	106(108%)
1,3,5-TNB.....	< 2.09	43.6(104%)	230(110%)	230(110%)	230(110%)	230(110%)	230(110%)
1,3-DNB.....	< 0.59	5.32(70.5%)	57.9(98.1%)	57.9(98.1%)	57.9(98.1%)	57.9(98.1%)	57.9(98.1%)
NITROBENZENE.....	< 0.42	< 0.42(0.0%)	< 0.42(0.0%)	< 0.42(0.0%)	< 0.42(0.0%)	< 0.42(0.0%)	< 0.42(0.0%)
TETRYL.....	< 5.00	102(102%)	565(113%)	565(113%)	565(113%)	565(113%)	565(113%)
2,4,6-TNT.....	< 1.92	39.4(103%)	215(112%)	215(112%)	215(112%)	215(112%)	215(112%)
2,6-DNT.....	< 0.40	4.78(59.8%)	37.6(94.0%)	37.6(94.0%)	37.6(94.0%)	37.6(94.0%)	37.6(94.0%)
2,4-DNT.....	< 0.42	6.40(76.1%)	43.5(104%)	43.5(104%)	43.5(104%)	43.5(104%)	43.5(104%)

G=Elevated

**APPENDIX H**

**ANALYTICAL DATA SUMMARY TABLES FOR TEST ITEMS**

## COMPUTER GENERATED ANALYTICAL DATA SUMMARY TABLES

Appendix H contains computer-generated analytical data summary tables. The tables have been prepared for pre-test and post-test sampling events.

The tables provide the following information:

- Equipment (test item) type.
- Sample matrix (wipe, rinsate or solid).
- Units.
- Contaminant mass or concentration.
- Total explosives concentration (sum of individual explosives contaminants (excludes nitrocellulose and nitroglycerin)).

A key of the sample identification conventions is provided in Table H-1.

Sample results exceeding the method detection limit (or estimated as J values) are shown in bold print.

If the analysis indicated that the compound was present below the method detection limit, the detection limit is shown with the classification U (e.g., 635U signifies that the contaminant was not present above the detection level of 635 ug).

Detection limits vary by matrix and dilution factor. In some cases, if the TNT concentration in a particular sample was high, a dilution was required to bring the concentration within the calibration range. The detection limits for the remainder of explosives analytes (e.g., tetryl) were increased proportionately.

In some cases, the mass of some contaminants is shown as a "J" value (i.e., 3.36J). This indicates that the compound was determined to be present but below the detection level. The value is estimated.

The presence of nitrobenzene in many of the wipe samples is attributable to field/laboratory contamination as discussed in Section 8 of the main report. Table 8-9 summarizes all of the nitrobenzene results.

The concentrations of some contaminants, specifically TNT in the sediment from the clay pipe, are reported as over one million parts per million (e.g., for pre-Test 15 samples, the concentration of TNT is reported as 1,246,000 ug/g). This anomaly is due to the reporting procedure. Concentrations are reported



Table H-1

Sample Identification Conventions

U	-	Below Detection Limit
J	-	Estimated Concentration
ug	-	Microgram
CP	-	Clay Pipe
PB	-	Powder Box
HN	-	Naip Mine
SSR	-	Shell Support Rack
SP	-	Steel Pipe
AP	-	Aluminum Pipe
CHAM WALL	-	Flash Chamber Wall
SHR	-	Steam-Heated Riser
SHV	-	Steam-Heated Valve
FLD BLNK	-	Field Blank
R	-	Rinsate Sample
W	-	Wipe Sample
SPK	-	Spike Applicator
DUP	-	Duplicate
S	-	Spike Rinsate

as weight of TNT to weight of soil. Apparently, in this case, if the weight of TNT exceeded the weight of soil, the concentration is over 100 percent, as shown for the following hypothetical case:

- Initial TNT mass - 100 grams
- Initial soil mass - 50 grams
- Concentration (ppm) = mass TNT/mass soil x 100%  
= 100 grams/50 grams x 100%  
= 200%

July 1990  
Revision: Final

TEST RUN 2  
400°F/24 HOURS

1311R2

HWAAP - Hot Gas Pilot Study  
 Pile Test 2 - 400 Deg F, 24 Hrs

TEST ITEM	MATERIAL	UNITS	HLK	FOX	1,3- TMS	1,3- L, 13	N3	TE13VL	2,4,6- TMT	2,6- DET	2,4- DET	TOTAL EXPLOSIVE
MOTOR SOAK	RAISE	Total U	6500 U	24100 U	11500 U	31000 U	22700 U	270000 U	10500 U	21000 U	12500 U	400000
PA 1	RAISE	Total U	650 U	400 U	1000 U	205 U	210 U	2500 U	900 U	200 U	210 U	0
PA 2	RAISE	Total U	650 U	400 U	1000 U	205 U	210 U	2500 U	900 U	200 U	210 U	0
SSR 1	WIPE	Total U	127 U	0 U	209 U	600 U	640	500 U	470	400 U	420 U	470
SSR 1 SPK	RAISE	Total U	1300 U	10500 U	25000 U	6000 U	4410 U	82500 U	13100 U	4200 U	4410 U	13100
SSR 1 DECON	WIPE	Total U	127 U	950 U	209 U	600 U	670	500 U	192 U	400 U	420 U	870
SSR 2	WIPE	Total U	127 U	950 U	209 U	600 U	410	500 U	192 U	400 U	420 U	410
SSR 2 SPK	RAISE	Total U	3500 U	2740 U	5000 U	1850 U	1100 U	14000 U	14100 U	1120 U	1180 U	14100
SSR 2 DECON	WIPE	Total U	127 U	950 U	209 U	600 U	640	500 U	192 U	400 U	420 U	850

TEST NAME	MATERIAL	Units	Prod	Fact	1,2- Total	1,2 Prod	4,3 Total	YIELD	2,4- Total	2,4- Prod	2,4- Yield	2,4- Total	2,4- Prod	2,4- Yield
CHALK WALL	WPE	Total	127 U	93 U	209 U	50 U	159	50 U	192 U	400 U	420 U	192 U	400 U	420 U
CLAY PIPE	SOIL	Total	127 U	0.60 U	209 U	0.60 U	0.420 U	500 U	192 U	0.400 U	0.420 U	192 U	0.400 U	0.420 U
FIELD WALK	PIPE	Total	121 U	93 U	209 U	86 U	369 U	47.5 U	182 U	360 U	360 U	182 U	360 U	360 U
FB 1R1	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
FB 1R2	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
FB 1R3	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
FB 1R4	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
SH 1R1	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R2	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R3	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R4	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R1	PIPE	Total	181 U	147 U	315 U	63 U	630 U	750 U	268 U	600 U	600 U	268 U	600 U	600 U
SH 1R2	PIPE	Total	181 U	147 U	315 U	63 U	630 U	750 U	268 U	600 U	600 U	268 U	600 U	600 U
SH 1R3	PIPE	Total	181 U	147 U	315 U	63 U	630 U	750 U	268 U	600 U	600 U	268 U	600 U	600 U
SH 1R4	PIPE	Total	181 U	147 U	315 U	63 U	630 U	750 U	268 U	600 U	600 U	268 U	600 U	600 U
SH 1R1	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
SH 1R2	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
SH 1R3	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
SH 1R4	PIPE	Total	635 U	400 U	1030 U	245 U	210 U	2500 U	660 U	200 U	210 U	660 U	200 U	210 U
SH 1R1	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R2	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R3	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R4	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R1	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R2	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R3	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R4	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R1	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	420 U
SH 1R2	WPE	Total	127 U	980 U	209 U	560 U	124	500 U	192 U	400 U	420 U	192 U	400 U	4

12. Evolving literature, etc. new

5

July 1980  
Revision: Final

TEST RUN 3  
500°F/36 HOURS

1311R2

HWAAP - Hot Gas Pilot Study  
Pre Test 3 - 500 Deg F, 30 hrs

TEST ITEM	MATRIX	UNIT	INX	POX	1,3,4 1,3	1,3 Unit	NR	TECH	2,4,6 THY	2,6 DHT	2,4 DHT	INITIAL CALC	TOTAL CALC
CLAY WALL	WPE	Total Uq	127 U	960 U	209 U	520 U	18.1	520 U	192 U	400 U	420 U	N/A (I)	19.1
CLAY WPE	SOL	Uq	12700 U	620 U	2090 U	520 U	4200 U	5200 U	19200 U	4000 U	4200 U	N/A (I)	19200
PA1 R1	RINSE	Total Uq	635 U	460 U	1050 U	283 U	210 U	2800 U	960 U	200 U	210 U	N/A (I)	0
PA2 R1	RINSE	Total Uq	635 U	460 U	1050 U	283 U	210 U	2500 U	960 U	200 U	210 U	N/A (I)	0
PA PF WPE	WPE	Total Uq	127 U	960 U	209 U	520 U	420 U	520 U	192 U	400 U	420 U	N/A (I)	0
SHAP WPE W1	WPE	Total Uq	127 U	960 U	209 U	520 U	420 U	520 U	192 U	400 U	420 U	N/A (I)	4.30
SHR1 R1	RINSE	Total Uq	190.5 U	337	315 U	88.5 U	630 U	750 U	268 U	600 U	630 U	N/A (I)	337
SHR2 R1	RINSE	Total Uq	190.5 U	236	315 U	88.5 U	630 U	750 U	268 U	600 U	630 U	N/A (I)	236
SHV1 R1	RINSE	Total Uq	1430	400 U	10500 U	283 U	210 U	2300 U	5600 U	200 U	4160 U	N/A (I)	4200
SHV1 R1	RINSE	Total Uq	6350 U	400 U	10500 U	283 U	210 U	2300 U	5600 U	200 U	4160 U	N/A (I)	0
SHV1 R2	RINSE	Total Uq	635 U	400 U	1050 U	283 U	210 U	2300 U	560 U	200 U	8100	N/A (I)	2100
SHV2 R1	RINSE	Total Uq	635 U	400 U	1050 U	283 U	210 U	2300 U	560 U	200 U	2100	N/A (I)	2100
SHV2 R1	RINSE	Total Uq	6350 U	400 U	10500 U	283 U	210 U	2300 U	5600 U	200 U	14500	N/A (I)	14500
SHV2 R2	RINSE	Total Uq	635 U	400 U	1050 U	283 U	210 U	2300 U	560 U	200 U	1700	N/A (I)	1700
SHV2 R3	RINSE	Total Uq	635 U	400 U	1050 U	283 U	210 U	2300 U	560 U	200 U	210 U	N/A (I)	0
SHV WPE WPE 3	WPE	Uq	127 U	960 U	209 U	520 U	420 U	520 U	192 U	400 U	420 U	N/A (I)	0
SSH1 DECON	WPE	Total Uq	21.4	28.6	20.9 U	560 U	420 U	520 U	192 U	400 U	420 U	N/A (I)	47.4
SSH1 BPK	RINSE	Total Uq	19100 U	4700 U	31500 U	8650 U	6300 U	7500 U	19200 U	6000 U	6300 U	N/A (I)	19200

(1) - Nitrated Esters not Analyzed

(2) - Explosives Compounds not Analyzed

HWAAP - Hot Gas Pilot Study  
 Pre Test 3 - 500 Day F, 3d Hrs

TEST ITEM	MATRIX	UNITS	HEAT	NOX	1,3,5- Total	1,3- Lys	NB	TEHRA	2,4,6- Total	2,6- Diff	2,4- Diff	Activated Carbon	TOTAL Particulate
SSR1W1	WPE	Total U	127 U	910 U	209 U	590 U	840	600 U	192 U	400 U	420 U	N/A (1)	500
SSR1W1	WPE	Total U	644	634	703 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	1500
SSR1W2	WPE	Total U	460	960 U	209 U	590 U	810	600 U	192 U	400 U	420 U	N/A (1)	455
SSR1W2	WPE	Total U	127 U	720	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	720
SSR1W3	WPE	Total U	260	960 U	209 U	590 U	420 U	500 U	214	400 U	420 U	N/A (1)	293
SSR1W3	WPE	Total U	127 U	493	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	493
SSR1W4	WPE	Total U	181	311	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	422
SSR1W5	WPE	Total U	127 U	645	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	545
SSR1W5	WPE	Total U	243	960 U	209 U	590 U	420 U	500 U	491	400 U	420 U	N/A (1)	319
SSR2 DECON	WPE	Total U	243	762	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	162
SSR2 8PK	FWSE	Total U	16500 U	12700 U	27300 U	7870 U	5460 U	6000 U	131500	5200 U	5400 U	N/A (1)	133000
SSR2 W1	WPE	Total U	613	960 U	209 U	590 U	720	500 U	192 U	400 U	420 U	N/A (1)	520
SSR2 W1	WPE	Total U	127 U	676	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	978
SSR2 W2	WPE	Total U	365	467	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	742
SSR2 W3	WPE	Total U	221	418	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	659
SSR2 W4	WPE	Total U	167	327	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	464
SSR2 W5	WPE	Total U	149	394	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	443
SHIP TO JE V2	WPE	U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	100 U	0
CHUB 1001 W1	WPE	U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	100 U	0

(1) - Polycyclic and Nitrogenous not Analyzed.

(2) - Explosives Compounds not Analyzed.



[illegible]

المجلة الدولية لدراسات حقوق الإنسان

HWAAP - Hot Gas Pilot Study  
Post Test 3 - 500 Deg F, 35 Hrs

TEST ITEM	WAVE	FLUX	FLUX	1.5- YAG	1.3- YAG	NA	TECHNL	2.4- YNT	2.0- LNT	2.4- DNT	Unlabeled Analysis	TOTAL Explosives
SR2R1	WAVE Total US	181 U	147 U	515 U	625 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SR2R2	WAVE Total US	181 U	147 U	515 U	625 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SR2R3	WAVE Total US	181 U	147 U	515 U	625 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SR2R4	WAVE Total US	181 U	147 U	515 U	625 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SR2R5	WAVE Total US	181 U	147 U	515 U	625 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SR2R6	WAVE Total US	181 U	147 U	515 U	625 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SR1R1	WAVE Total US	635 U	480 U	1050 U	725 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SR1R2	WAVE Total US	635 U	480 U	1050 U	725 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SR1R3	WAVE Total US	635 U	480 U	1050 U	725 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SR1R4	WAVE Total US	635 U	480 U	1050 U	725 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SSR1W1	WAVE Total US	127 U	950 U	208 U	580 U	107	500 U	192 U	400 U	420 U	N/A (1)	10.7
SSR1W2	WAVE Total US	127 U	950 U	208 U	580 U	9.47	500 U	192 U	400 U	420 U	N/A (1)	9.67
SSR1W3	WAVE Total US	127 U	950 U	208 U	580 U	8.66	500 U	192 U	400 U	420 U	N/A (1)	8.69
SSR1W4	WAVE Total US	127 U	950 U	208 U	580 U	8.83	500 U	192 U	400 U	420 U	N/A (1)	8.83
SSR1W5	WAVE Total US	127 U	950 U	208 U	580 U	12.0	500 U	192 U	400 U	420 U	N/A (1)	12.0
SSR1W6	WAVE Total US	127 U	950 U	208 U	580 U	14.7	500 U	192 U	400 U	420 U	N/A (1)	14.7
SSR1W7	WAVE Total US	127 U	950 U	208 U	580 U	13.9	500 U	192 U	400 U	420 U	N/A (1)	13.9
SSR1W8	WAVE Total US	127 U	950 U	208 U	580 U	8.23	500 U	192 U	400 U	420 U	N/A (1)	8.23
SRUP MRIE V2	WAVE Total US	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.0 U	N/A (2)

(1) - Nitrocellulose not Analyzed.

(2) - Explosives Compounds not Analyzed.

July 1990  
Revision: Final

TEST RUN 5  
500°F/24 HOURS

1311R2

HWAAP - Hot Gas Pilot Study  
 Pre Test 5 - 500 Deg F, 24 Hrs

TEST ITEM	MATRIX	UNITS	MAX	MAX	1,3,5-THF	1,3-GLY	NO	TETRAH	2,4,6-TNT	2,3-DNT	2,4-DNT	UNSATURATED	TOTAL
CLAY PIPE	SOIL	Wt%	12700 U	6500 U	20000 U	5300 U	4500 U	50000 U	530000	4000 U	4500 U	N/A (1)	650000
GEAR OIL	OIL	Wt%	144 U	215 U	237 U	633 U	476 U	552 U	217 U	453 U	476 U	N/A (1)	2150
PR 1 R/R2	RINSE	Total Wt	835 U	400 U	1050 U	293 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
PR 2 R/R2	RINSE	Total Wt	835 U	400 U	1050 U	293 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
SRP MUSE W1	WIPE	Total Wt	43.9	9.6 U	20.9 U	8.77 U	4.20 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	43.9
SRP MUSE W1	WIPE	Total Wt	127 U	30.0 U	20.9 U	59.0 U	42.00 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	133
SSR 1 SPK	RINSE	Total Wt	7940 U	0150 U	13100 U	3300 U	2636 U	31300 U	403000	2500 U	2300 U	N/A (1)	430000
SSR 1 TOP W	WIPE	Total Wt	127 U	0.80 U	20.9 U	5.90 U	4.20 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	0
SSR 1 WI/W4	WIPE	Total Wt	209	0.80 U	20.9 U	5.90 U	4.20 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	218
SSR 1 WI/W4	WIPE	Total Wt	127 U	6.7	20.9 U	59.00 U	42.0 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	637
SSR 2 SPK	RINSE	Total Wt	12700 U	9500 U	21000 U	5900 U	4200 U	50000 U	340000	4000 U	4200 U	N/A (1)	340000
SSR 2 TOP W	WIPE	Total Wt	127 U	0.80 U	20.9 U	5.90 U	4.20 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	0
SSR 2 WI/W4	WIPE	Total Wt	127 U	0.80 U	20.9 U	5.90 U	4.20 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	0
SP BLK	WIPE	Total Wt	127 U	0.80 U	20.9 U	5.90 U	4.20 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	4.53
SP BLK	WIPE	Total Wt	127 U	0.80 U	20.9 U	5.90 U	4.20 U	50.0 U	19.2 U	4.00 U	4.20 U	N/A (1)	0
SRP MUSE W2	WIPE	Total Wt	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)
SU FLD BLK	WIPE	Total Wt	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)

(1) - Nitroated Enrich not Analyzed

(2) - Explosives Compounds not Analyzed

**HWAAP - Hot Gas Pilot Study**  
**Post Test 5 - 600 Deg F, 24 Hrs**

TEST ITEM	MATRIX	UNIT	MAX	NOX	1,2,4 THU	1,3- DMS	NB	TECHN	2,4,6- THF	2,6- DHF	2,4- DHF	INITIALS	TOTAL
CHL 3 WALL	WPE	Total UG	127 U	960 U	209 U	560 U	176	600 U	192 U	400 U	420 U	N/A (1)	175
CHL 3 WALL BL	WPE	Total UG	127 U	960 U	209 U	560 U	826	530 U	192 U	400 U	420 U	N/A (1)	830
CLAY PPE	SOAL	UG/L	127 U	0.590 U	2.09 U	0.390 U	0.42 U	600 U	1.02 U	0.400 U	0.420 U	N/A (1)	0
CP FLD BLK	RIUSE	Total UG	65.0 U	73.5 U	157.5 U	44.3 U	31.5 U	375 U	144 U	30.0 U	31.5 U	N/A (1)	0
MOTOR RIUSE	RIUSE	Total UG	60.0 U	61.00 U	100.00 U	30.00 U	21.60 U	200.00 U	92.00 U	2.300 U	21.60 U	N/A (1)	0
PB 1 R1	RIUSE	Total UG	65.5 U	466 U	105.3 U	205 U	210 U	2500 U	560 U	200 U	210 U	N/A (1)	0
PB 1 R2	RIUSE	Total UG	63.5 U	490 U	105.3 U	295 U	210 U	2500 U	560 U	200 U	210 U	N/A (1)	0
PB 1 R3	RIUSE	Total UG	63.5 U	490 U	105.3 U	295 U	210 U	2500 U	560 U	200 U	210 U	N/A (1)	0
PB 1 R4	RIUSE	Total UG	65.5 U	490 U	105.3 U	295 U	210 U	2500 U	560 U	200 U	210 U	N/A (1)	0
PB FLD BLK	RIUSE	Total UG	114 U	68.2 U	189 U	53.1 U	37.8 U	450 U	172.8 U	38.0 U	37.8 U	N/A (1)	0
SHIP LANE W1	WPE	Total UG	127 U	960 U	209 U	560 U	201	500 U	192 U	400 U	420 U	N/A (1)	201
SHR 1 R1	RIUSE	Total UG	191 U	147 U	315 U	68.5 U	63.0 U	760 U	268 U	60.0 U	63.0 U	N/A (1)	0
SHR 1 R2	RIUSE	Total UG	191 U	147 U	315 U	68.5 U	63.0 U	750 U	268 U	60.0 U	63.0 U	N/A (1)	0
SHR 1 R3	RIUSE	Total UG	191 U	147 U	315 U	68.5 U	63.0 U	750 U	268 U	60.0 U	63.0 U	N/A (1)	0
SHR 1 R4	RIUSE	Total UG	191 U	147 U	315 U	68.5 U	63.0 U	750 U	268 U	60.0 U	63.0 U	N/A (1)	0
SHR FLD BLK	RIUSE	Total UG	95.3 U	73.5 U	158 U	44.3 U	31.5 U	375 U	144 U	30.0 U	31.5 U	N/A (1)	0
SSR 2 W1	WPE	Total UG	127 U	960 U	209 U	560 U	242	500 U	162 U	400 U	420 U	N/A (1)	242
SSR 2 W2	WPE	Total UG	127 U	960 U	209 U	560 U	724	500 U	162 U	400 U	420 U	N/A (1)	724
SSR 2 W3	WPE	Total UG	127 U	280 U	209 U	560 U	494	600 U	192 U	400 U	420 U	N/A (1)	494
SSR 2 W4	WPE	Total UG	127 U	960 U	209 U	560 U	302 J	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 2 W5	WPE	Total UG	127 U	960 U	209 U	560 U	256	500 U	192 U	400 U	420 U	N/A (1)	256
SSR 2 W6	WPE	Total UG	127 U	960 U	209 U	560 U	671	500 U	192 U	400 U	420 U	N/A (1)	671
SSR 2 W7	WPE	Total UG	127 U	960 U	209 U	560 U	484	500 U	192 U	400 U	420 U	N/A (1)	484
SSR 2 W8	WPE	Total UG	127 U	960 U	209 U	560 U	306 J	500 U	192 U	400 U	420 U	N/A (1)	0
CHL 8 WALL V2	WPE	Total UG	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	0
SHIP LANE W2	WPE	Total UG	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	0

(1) - Nitrated Esters not Analyzed.

(2) - Explosives Compounds not Analyzed.

July 1990  
Revision: Final

TEST RUN 3  
400°F/36 HOURS

1311R2

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[illegible]

**(24) - Explosives Compounds not Analyzed.**

**HWAAP - Hot Gas Fluct Study**  
**Post Test 8 - 400 Deg F, 36 hrs**

TEST ITEM	MATRIX	Units	HMX	RDX	1,3,5- THB	1,3- DAB	MB	TETRAV	2,4,6- TMC	2,6- DIT	2,4- DIT	INITIAL GAS, U	TOTAL GAS, U
SSR1 W1	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	520 U	N/A (1)	0
SSR1 W2	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR1 W3	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR1 W4	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR1 W5	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR1 W6	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR1 W7	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR1 W8	WIPE	Total U	127 U	960 U	209 U	600 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SP R1	RAISE	Total U	635 U	490 U	1050 U	285 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SP R2	RAISE	Total U	635 U	490 U	1050 U	285 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SP R3	RAISE	Total U	635 U	490 U	1050 U	285 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SP R4	RAISE	Total U	635 U	490 U	1050 U	285 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
CHAB WALL W2	WIPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	7.50	N/A (2)
SHIP L2/E W2	WIPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	8.3	N/A (2)
SM FL3 B1JK	WIPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.00 U	N/A (2)

(1) - Nitroated Esters not Analyzed.

(2) - Explosives Compounds not Analyzed.



**HW/AP - Hot Gas Pilot Study**  
**Post Test 8 - 400 Deg F, 30 Hrs**

TEST ITEM	MATRIX	UNIT	MAX	FDY	1,3,5- TOL	1,3- DIB	NA	TETRAH	2,4,6- TNT	2,6- DIB	2,4- DIB	ESTIMATED ISOTENE	TOTAL EXPLOSIVE
BEAKER FUSE	FWSE	Total Wt	153 U	123 U	203 U	738 U	525 U	825 U	240 U	500 U	525 U	N/A (1)	0
CHUB WALL	WPE	Total Wt	127 U	980 U	209 U	560 U	420 U	530 U	192 U	400 U	420 U	N/A (1)	0
CHUB WALL BL	WPE	Total Wt	127 U	980 U	209 U	560 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
CLAY PTE	SOA	Wt/W	127 U	625 U	209 U	560 U	0.420 U	500 U	603	0.400 U	0.420 U	N/A (1)	603
CPFD BUNK	FWSE	Total Wt	159 U	123 U	263 U	733 U	125 U	825 U	240 U	500 U	525 U	N/A (1)	0
PB 1 R1	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	1130
PB 1 R1 DUP	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	1130
PB 1 R2	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	0
PB 1 R3	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	0
PB 1 R4	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	0
PB 2 R1	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	0
PB 2 R2	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	0
PB 2 R3	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	0
PB 2 R4	FWSE	Total Wt	635 U	460 U	1050 U	263 U	210 U	2500 U	1130	200 U	210 U	N/A (1)	0
SHIP MATE W1	WPE	Total Wt	127 U	980 U	209 U	560 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SHR 1 F1	FWSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SHR 1 F2	FWSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SHR 1 R3	FWSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SHR 1 R4	FWSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0
SHR 1 F1 W1K	FWSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	268 U	600 U	630 U	N/A (1)	0

(1) - Mixed Explosive not Analyzed.

(2) - Explosive Components not Analyzed.

July 1990  
Revision: Final

TEST RUN 13  
500°F/12 HOURS

1311R2

**hWAAAP - Hot Gas Pilot Study**  
**Pre Test 13 - ECU Day F, 12 Hrs**

[illegible]

(1) - Number: Esters not Analyzed.

(2) - Explosives Compounds not Analyzed

**HWAAP - Hot Gas Pilot Study**  
**Post Test 13 - 600 Deg F, 12 Hrs**

TEST ITEM	SAMPLE	UNITS	IRUX	FDX	1,3,5- Tolu	1,3- DIB	NB	TETRA	2,4,6- TNT	2,3- DIT	2,4- DIT	INITIAL Exposure	TOTAL Exposure
APR1	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
APR2	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
APR3	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
APR4	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
CHWB WALL	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
CHWB WALL BL	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
CLAY PFE	SOIL	Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
CP FLD BLNK	RHSE	Total Wt	159 U	123 U	203 U	7175 U	525 U	635 U	240 U	500 U	525 U	N/A (1)	0
PB 2 R1	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
PB 2 R2	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
PB 2 R3	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
PB 2 R4	RHSE	Total Wt	635 U	400 U	1050 U	203 U	210 U	2500 U	630 U	200 U	210 U	N/A (1)	0
PB FLD BLNK	RHSE	Total Wt	159 U	123 U	203 U	7175 U	525 U	635 U	240 U	500 U	525 U	N/A (1)	0
SHIP MINE W1	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SHIP 1 R1	RHSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	288 U	600 U	630 U	N/A (1)	0
SHIP 1 R2	RHSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	288 U	600 U	630 U	N/A (1)	0
SHIP 1 R3	RHSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	288 U	600 U	630 U	N/A (1)	0
SHIP 1 R4	RHSE	Total Wt	191 U	147 U	315 U	885 U	630 U	750 U	288 U	600 U	630 U	N/A (1)	0
SHIP FLD BLNK	RHSE	Total Wt	185 U	127 U	273 U	787 U	518 U	650 U	250 U	520 U	548 U	N/A (1)	0
SSR 1 W1	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1 W2	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1 W3	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1 W4	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1 W5	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1 W6	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1 W7	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1 W8	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SHIP MINE W2	WIPE	Total Wt	127 U	960 U	209 U	890 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
CHWB WALL W2	WIPE	Total Wt	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	N/A (2)
SM FLD BLNK	WIPE	Total Wt	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	N/A (2)
												750	N/A (2)

(1) - Harmed Expos not Analyzed.

(2) - Explosives Compounds not Analyzed.

... Retrieval File: HWAAP Post Test 13

July 1990  
Revision: Final

TEST RUN 14  
400°F/12 HOURS

1311R2

HWAAP - Hot Gas Pilot Study  
Pre Test 14 - 400 Deg F, 12 Hrs

TEST ITEM	MATRIX	UNIT	HDX	HDX	RDX	1,3,5- TMS	1,3- DMS	NB	TETRA	2,4,6- TMS	2,5- DIT	2,4- DIT	INITIAL	TOTAL
CLAY P/E	BOL	U/g	127.00	127.00	600.00	200.00	500.00	4200 U	50000 U	554000	4000 U	4200 U	N/A (1)	554000
OP FLD BLANK	RINSE	Total U/g	159 U	159 U	123 U	283 U	73.8 U	52.5 U	625 U	240 U	500 U	52.5 U	N/A (1)	0
PB 1 RI/R4	RINSE	Total U/g	635 U	635 U	490 U	1050 U	205 U	210 U	2500 U	600 U	200 U	210 U	N/A (1)	0
PB 2 RI/R4	RINSE	Total U/g	635 U	635 U	490 U	1050 U	205 U	210 U	2500 U	600 U	200 U	210 U	N/A (1)	0
PB FLD BLANK	RINSE	Total U/g	159 U	159 U	123 U	283 U	73.8 U	52.5 U	625 U	240 U	500 U	52.5 U	N/A (1)	0
SRP MJE W1	WIPE	Total U/g	127 U	127 U	99 U	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SR FLD BLANK	WIPE	Total U/g	127 U	127 U	99 U	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SSR 1SPK	RINSE	Total U/g	1588 U	1588 U	1230 U	2630 U	733 U	525 U	6250 U	201000	500 U	184	N/A (1)	62500
SSR 1SPK	RINSE	Total U/g	15200 U	15200 U	12300 U	26300 U	7330 U	5250 U	62500 U	643000	5000 U	5250 U	N/A (1)	643000
SSR 1SPK	RINSE	Total U/g	19100 U	19100 U	14700 U	31800 U	8850 U	6300 U	75000 U	280000	6000 U	6300 U	N/A (1)	0
SSR 1W1/W4	WIPE	Total U/g	127 U	127 U	99 U	209 U	590 U	18.9	500 U	192 U	400 U	420 U	N/A (1)	16.9
SSR 1W5/W8	WIPE	Total U/g	127 U	127 U	99 U	209 U	590 U	16.6	500 U	192 U	400 U	420 U	N/A (1)	16.6
SSR 2SPK	RINSE	Total U/g	19100 U	19100 U	14700 U	31800 U	8850 U	6300 U	75000 U	340000	6000 U	6300 U	N/A (1)	340000
SSR 2SPK	RINSE	Total U/g	1890 U	1890 U	1030 U	2300 U	738 U	525 U	6250 U	355000	500 U	415	N/A (1)	355000
SSR 2SPK	RINSE	Total U/g	1590 U	1590 U	1030 U	2300 U	738 U	525 U	6250 U	240000	500 U	5250 U	N/A (1)	0
SSR 2W1/W4	WIPE	Total U/g	127 U	127 U	99 U	209 U	590 U	25.4	600 U	192 U	400 U	420 U	N/A (1)	25.4
SSR 2W5/W8	WIPE	Total U/g	127 U	127 U	99 U	209 U	590 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SRP MJE W2	WIPE	Total U/g	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	N/A (2)
SR FLD BLANK	WIPE	Total U/g	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	N/A (2)

(1) - Nitroed Esters not Analyzed

(2) - Explosives Compounds not Analyzed

**HWAAF - Hot Gas Pilot Study  
Post Test 14 - 400 Deg F, 12 Hrs**

TEST ITEM	MATRIX	URATS	DMX	ROX	1.3- Tnd	1.3- Dnd	NA	TEHVL	2.4- Tnd	2.4- Dnd	collected Emissions	TOTAL Emissions
CHG3 WALLB	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
CLAY PIPE	SOIL	Total Uq	127 U	0.00 U	20.0 U	0.00 U	0.00 U	51.0 U	1.92 U	0.00 U	N/A (1)	0
CP FLD BLK	RINSE	Total Uq	150 U	103 U	263 U	73.0 U	240 U	240 U	240 U	50.0 U	N/A (1)	0
FB : R1	RINSE	Total Uq	835 U	400 U	1033 U	225 U	210 U	2400 U	240 U	210 U	N/A (1)	0
PB1 R2	RINSE	Total Uq	635 U	400 U	1033 U	225 U	210 U	2400 U	240 U	210 U	N/A (1)	0
PB1 R3	RINSE	Total Uq	635 U	400 U	1033 U	225 U	210 U	2400 U	240 U	210 U	N/A (1)	0
PB1 R4	RINSE	Total Uq	635 U	400 U	1033 U	225 U	210 U	2400 U	240 U	210 U	N/A (1)	0
PB FLD BLK	RINSE	Total Uq	150 U	103 U	263 U	73.0 U	240 U	240 U	240 U	50.0 U	N/A (1)	0
SP1 M1E W1	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	1.92 U	4.00 U	N/A (1)	0
SSR1 R1	RINSE	Total Uq	732 U	430 U	600 U	60.0 U	630 U	750 U	81.0 U	60.0 U	N/A (1)	0
SSR1 R2	RINSE	Total Uq	732 U	430 U	600 U	60.0 U	630 U	750 U	81.0 U	60.0 U	N/A (1)	0
SSR1 R3	RINSE	Total Uq	450 U	20.0 U	33.0 U	60.0 U	630 U	750 U	81.0 U	60.0 U	N/A (1)	0
SSR1 R4	RINSE	Total Uq	284 U	84.0 U	318 U	60.0 U	630 U	750 U	81.0 U	60.0 U	N/A (1)	0
SSR FLD BLK	RINSE	Total Uq	150 U	103 U	263 U	73.0 U	240 U	240 U	240 U	50.0 U	N/A (1)	0
SSR1 W1	WIPE	Total Uq	34.3 U	9.80 U	27.2 U	5.90 U	4.20 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SSR1 W2	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SSR1 W3	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SSR1 W4	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SSR1 W5	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SSR1 W6	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SSR1 W7	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SSR1 W8	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SP R1	RINSE	Total Uq	593 U	400 U	1033 U	225 U	210 U	2400 U	240 U	210 U	N/A (1)	0
SP R2	RINSE	Total Uq	605 U	400 U	1033 U	225 U	210 U	2400 U	240 U	210 U	N/A (1)	0
SP R3	RINSE	Total Uq	450 U	20.0 U	33.0 U	60.0 U	630 U	750 U	81.0 U	60.0 U	N/A (1)	0
SP R4	RINSE	Total Uq	450 U	20.0 U	33.0 U	60.0 U	630 U	750 U	81.0 U	60.0 U	N/A (1)	0
WALL FLD BLK	WIPE	Total Uq	127 U	0.00 U	20.0 U	0.00 U	4.00 U	50.0 U	19.2 U	4.00 U	N/A (1)	0
SHIP M1E W2	WIPE	Total Uq	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.00 U	1.00 U
CHG3 WALL V2	WIPE	Total Uq	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	20.0 U	10.0 U
SM FLD BLK	WIPE	Total Uq	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.00 U	1.00 U

July 1990  
Revision: Final

TEST RUN 15  
600°F/12 HOURS

1311R2





HWAAP - Hot Gas Pilot Study  
Post Test 15 - 600 Deg F, 12 Hrs

TEST ITEM	MATRIX	UNITS	HMX	RDX	1,3,5- THB	1,3- DIB	NB	TETRA	2,4,6- TNT	2,6- DIT	2,4- DIT	INITIATED RATING	TOTAL EXPLOSIVES
SSR 1W1	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	4.80 J	4.00 U	1.30 J	N/A (1)	0
SSR 1W2	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	2.50 J	1.20 J	4.20 U	N/A (1)	0
SSR 1W3	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	1.40 J	4.00 U	4.20 U	N/A (1)	0
SSR 1W4	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	1.60 J	4.00 U	4.20 U	N/A (1)	0
SSR 1W5	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	3.60 J	4.00 U	1.30 J	N/A (1)	0
SSR 1W6	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	2.50 J	4.00 U	1.40 J	N/A (1)	0
SSR 1W7	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	2.50 J	4.00 U	1.40 J	N/A (1)	0
SSR 1W8	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	2.30 J	4.00 U	1.40 J	N/A (1)	0
SSR FLD BLNK	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	2.30 J	4.00 U	1.40 J	N/A (1)	0
WALL FLD BLNK	WPE	Total U	127 U	660 U	20.9 U	560 U	420 U	500 U	3.60 J	4.00 U	1.50 J	N/A (1)	0
SHIP W/IE V2	WPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.00 U	N/A (2)
SM FLD BLNK	WPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.00 U	N/A (2)
CHUB WALL W2	WPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	7.50	N/A (2)
CHUB WALL BLNK	WPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.00 U	N/A (2)

(1) - Initiated Cases not Analyzed

(2) - Explosives Compounds not Analyzed

HWAAP - Hot Gas Pilot Study  
Post Test 15 - 600 Deg F, 12 Hrs

TEST ITEM	MATRIX	Units	MAX	FDK	1.3.4- TNT	1.3- DNT	Na	TRIMVL	2.4.4- TNT	2.4- DNT	2.4- DNT	RETURNED CHARGE	Total Explosives
AP 1 R1	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
AP 1 R2	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
AP 1 R3	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
AP 1 R4	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
AP FLD BLNK	RIUSE	Total Uq	159 U	121 U	283 U	73.8 U	52.5 U	625 U	240 U	50.0 U	52.5 U	N/A (U)	0
CHUG WALL W1	WPE	Total Uq	127 U	98.0 U	20.9 U	6.90 U	4.20 U	50.0 U	1.90 J	4.00 U	1.90 J	N/A (U)	0
CLAY PIPE	BCAL	Uq	127 U	0.50 U	2.09 U	0.550 U	0.40 U	500 U	1.02 U	0.400 U	0.420 U	N/A (U)	0
CP FLD BLNK	RIUSE	Total Uq	159 U	123 U	263 U	73.8 U	52.5 U	625 U	240 U	50.0 U	52.5 U	N/A (U)	0
PB 1 R1	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
PB 1 R2	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
PB 1 R3	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
PB 1 R4	RIUSE	Total Uq	635 U	400 U	1050 U	235 U	210 U	2300 U	600 U	200 U	210 U	N/A (U)	0
PB FLD BLNK	RIUSE	Total Uq	159 U	123 U	263 U	73.8 U	52.5 U	625 U	240 U	50.0 U	52.5 U	N/A (U)	0
SHR MADE W1	WPE	Total Uq	127 U	98.0 U	20.9 U	6.90 U	4.20 U	50.0 U	1.90 J	4.00 U	1.70 J	N/A (U)	0
SHR 1 R1	RIUSE	Total Uq	191 U	147 U	315 U	88.5 U	63.0 U	750 U	288 U	60.0 U	63.0 U	N/A (U)	0
SHR 1 R2	RIUSE	Total Uq	191 U	147 U	315 U	88.5 U	63.0 U	750 U	288 U	60.0 U	63.0 U	N/A (U)	0
SHR 1 R3	RIUSE	Total Uq	191 U	147 U	315 U	88.5 U	63.0 U	750 U	288 U	60.0 U	63.0 U	N/A (U)	0
SHR 1 R4	RIUSE	Total Uq	191 U	147 U	315 U	88.5 U	63.0 U	750 U	288 U	60.0 U	63.0 U	N/A (U)	0
SHR FLD BLNK	RIUSE	Total Uq	191 U	147 U	315 U	88.5 U	63.0 U	750 U	288 U	60.0 U	63.0 U	N/A (U)	0
SM FLD BLNK	WPE	Total Uq	127 U	98.0 U	20.9 U	6.90 U	4.20 U	50.0 U	1.90 J	4.00 U	1.40 J	N/A (U)	0

(1) - Narrated Explosives not Analyzed.

(2) - Explosives Compounds not Analyzed.

July 1990  
Revision: Final

TEST RUN 16  
600° F/6 HOURS

1311R2

HWAAP - Hot Gas Pilot Study  
Pre Test 18 - 600 Deg F, 5 Hrs

TEST ITEM	MATRIX	UNIT	FLUX	ROX	1,3,5- TOL	1,3- DOL	NB	TEDYL	2,4- DOL	2,4- DOL	2,4- DOL	INITIAL CONC	TOTAL CONC
CLAY F/E	SOE	U/1	12700 U	600 U	2000 U	5000 U	4200 U	5000 U	4000 U	4000 U	4000 U	N/A (1)	10000
CP FLD BLNK	PUSE	Total U	150 U	120 U	200 U	700 U	525 U	625 U	500 U	500 U	500 U	N/A (1)	0
PR 1 R/R4	PUSE	Total U	635 U	400 U	1000 U	200 U	210 U	2500 U	200 U	200 U	210 U	N/A (1)	0
PR 2 R/R4	PUSE	Total U	635 U	400 U	1000 U	200 U	210 U	2500 U	200 U	200 U	210 U	N/A (1)	0
PR FLD BLNK	PUSE	Total U	150 U	120 U	200 U	700 U	525 U	625 U	500 U	500 U	525 U	N/A (1)	0
SIIP W/WE W1	WIPE	Total U	127 U	320 J	820 J	400 J	420 U	500 U	400 U	400 U	300	N/A (1)	630
SM FLD BLNK	WIPE	Total U	127 U	900 U	2000 U	500 U	420 U	500 U	400 U	400 U	130 J	N/A (1)	0
SSR 1 SPK	PUSE	Total U	19100 U	1470 U	3150 U	885 U	630 U	7500 U	600 U	600 U	485 J	N/A (1)	0
SSR 1 SPK	PUSE	Total U	19100 U	1470 U	3150 U	885 U	630 U	7500 U	600 U	600 U	485 J	N/A (1)	0
SSR 1 W/W4	WIPE	Total U	127 U	900 U	2000 U	500 U	420 U	500 U	400 U	400 U	420	N/A (1)	10000
SSR 1 W/W4	WIPE	Total U	324	240	170 J	310 J	194	500 U	400 U	400 U	420	N/A (1)	420
SSR 2 SPK	PUSE	Total U	19100 U	1470 U	3150 U	885 U	630 U	7500 U	600 U	600 U	485 J	N/A (1)	0
SSR 2 SPK	PUSE	Total U	19100 U	1470 U	3150 U	885 U	630 U	7500 U	600 U	600 U	485 J	N/A (1)	0
SSR 2 W/W4	WIPE	Total U	127 U	900 U	2000 U	500 U	420 U	500 U	400 U	400 U	420	N/A (1)	0
SSR 2 W/W4	WIPE	Total U	127 U	900 U	2000 U	500 U	420 U	500 U	400 U	400 U	420	N/A (1)	0
SSR 2 W/W4	WIPE	Total U	378	1610	200 U	500 U	420 U	500 U	400 U	400 U	420	N/A (1)	0
SSR 2 W/W4	WIPE	Total U	127 U	900 U	2000 U	500 U	420 U	500 U	400 U	400 U	420	N/A (1)	0
SSR FLD BLNK	WIPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (1)	0
SIIP W/WE W2	WIPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	N/A (2)
SM FLD BLNK	WIPE	Total U	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	500 U	N/A (2)

(1) - Nitrated Esters not Analyzed.

(2) - Explosives Compounds not Analyzed.

**HW/AP - Hot Gas Pilot Study  
Post Test 18 - 600 Deg F, 6 Hrs**

TEST ITEM	MATRIX	UNIT3	HEX	ROX	1,3,5- T.M.J	1,3- D.M.J	NB	TELHVL	2,4,6- THT	2,6- DHT	2,4- DHT	Initiated cellulose	TOTAL Explosives
CLAY/PE	SOL	U/31	127 U	0.60 U	2.00 U	0.60 U	0.42 U	5.00 U	1.82 U	0.400 U	0.420 U	N/A (1)	0
CP FLD BLK	PUSE	Total U	159 U	123 U	233 U	73.8 U	52.5 U	625 U	240 U	50.0 U	52.5 U	N/A (1)	0
FC FLD BLK	W/PE	Total U	127 U	9.83 U	20.9 U	5.90 U	4.20 U	50.0 U	10.8 J	4.00 U	1.16 J	N/A (1)	0
FL CHLW WALL	W/PE	Total U	127 U	9.80 U	20.9 U	5.90 U	4.20 U	50.0 U	14.8 J	4.00 U	2.39 J	N/A (1)	0
PE 1 DUP	PUSE	Total U	254 U	108 U	418 U	118 U	84.0 U	1000 U	384 U	80.0 U	84.0 U	N/A (1)	0
PB FLD BLK	PUSE	Total U	150 U	123 U	283 U	73.8 U	52.5 U	625 U	240 U	50.0 U	52.5 U	N/A (1)	0
PB1 R1	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
PB1 R2	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
PB1 R3	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
PB1 R4	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
SHIP/PAWIE W1	TYPE	Total U	127 U	9.83 U	20.9 U	5.90 U	4.20 U	50.0 U	7.89 J	4.00 U	2.39 J	N/A (1)	0
SHR1 DUP	PUSE	Total U	254 U	108 U	418 U	118 U	84.0 U	1000 U	384 U	80.0 U	84.0 U	N/A (1)	0
SHR FLD BLK	PUSE	Total U	153 U	123 U	283 U	73.8 U	52.5 U	625 U	240 U	50.0 U	52.5 U	N/A (1)	0
SHR1 R1	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
SHR1 R2	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
SHR1 R3	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0
SHR1 R4	PUSE	Total U	635 U	450 U	1050 U	295 U	210 U	2500 U	950 U	200 U	210 U	N/A (1)	0

(1) - Nitrocellulose not Analyzed.

(2) - Explosives Compounds not Analyzed.

HW/AAP - Hot Gas Pilot Study  
Post Test 16 - 500 Deg F, 6 hrs

TEST ITEM	MATRIX	UNITS	FWT	EDX	13.5- TINT	1.3- Dist	ND	TEHVL	2.4.8- TINT	2.8- Dist	2.4- TINT	W/FACTOR L. EN.	Total Expos. Time
SH1 DAP	RIUSE	Total Uq	234 U	1.3 U	418 U	118 U	840 U	10.0 U	364 U	8.0 U	4.0 U	N/A (1)	0
SH1 FLD BLNK	RIUSE	Total Uq	159 U	123 U	263 U	738 U	525 U	635 U	240 U	500 U	52.0 U	N/A (1)	0
SH1 R1	RIUSE	Total Uq	635 U	450 U	1050 U	265 U	210 U	2500 U	7.3 U	210 U	210 U	N/A (1)	0
SH1 R2	RIUSE	Total Uq	635 U	400 U	1050 U	265 U	210 U	2500 U	660 U	260 U	210 U	N/A (1)	0
SH1 R3	RIUSE	Total Uq	635 U	400 U	1050 U	265 U	210 U	2500 U	660 U	260 U	210 U	N/A (1)	0
SH1 R4	RIUSE	Total Uq	635 U	400 U	1050 U	265 U	210 U	2500 U	660 U	260 U	210 U	N/A (1)	0
SH1 FLD BLNK	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	10.5 U	4.0 U	1.00 U	N/A (1)	0
SSRW1	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	12.1 U	4.0 U	1.00 U	N/A (1)	0
SSRW2	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	0.70 U	4.0 U	4.20 U	N/A (1)	0
SSRW3	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	10.3 U	4.0 U	4.20 U	N/A (1)	0
SSRW4	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	8.65 U	4.0 U	1.00 U	N/A (1)	0
SSRW5	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	0.70 U	4.0 U	4.20 U	N/A (1)	0
SSRW6	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	13.2 U	4.0 U	4.2 U	N/A (1)	0
SSRW7	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	1.1 U	4.0 U	1.00 U	N/A (1)	0
SSRW8	WIPE	Total Uq	127 U	98 U	209 U	590 U	420 U	500 U	10.2 U	4.0 U	4.20 U	N/A (1)	0
SH1 FLD BLNK W2	WIPE	Total Uq	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)
SH1 FLD BLNK	WIPE	Total Uq	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)
CHUB WALL W2	WIPE	Total Uq	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)
CHUB WALL BL	WIPE	Total Uq	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)

(1) - Material Exposed not Analyzed

(2) - Explosives Compounds not Analyzed

July 1980  
Revision: Final

TEST RUN 17  
600°F/26 HOURS

1311R2



HWAAP - Hot Gas Pilot Study  
Pre Test 17 - 600 Deg F, 48 Hrs

EQUIPMENT	UNIT	HMIX	RMX	1,3,5 TGA	1,3 DIF	PL	TETRA	2,4,6 THT	2,6 DIF	2,4 DIF	Estimated Excess	Total Excess
AP 1	RMSE Total U	8400	450 U	1050 U	235 U	210 U	2500 U	7250 U	200 U	210 U	N/A (1)	12700
AP 1	RMSE Total U	6350 U	3050 U	1050 U	2050 U	2100 U	2500 U	5600 U	2000 U	2100 U	N/A (1)	5600 U
AP 2	RMSE Total U	6750	17300	1050 U	205 U	210 U	2500 U	845 J	200 U	210 U	N/A (1)	24100
AP FLD BLK	RMSE Total U	155 U	125 U	265 U	738 U	525 U	625 U	240 U	500 U	525 U	N/A (1)	0
PB FLD BLK	RMSE Total U	159 U	123 U	263 U	38 U	525 U	625 U	240 U	500 U	525 U	N/A (1)	0
PB 1	RMSE Total U	635 U	490 U	1050 U	265 U	210 U	2500 U	110 J	200 U	210 U	N/A (1)	0
PB 2	RMSE Total U	635 U	100 J	1050 U	265 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
PB 3	RMSE Total U	635 U	110 J	1050 U	265 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SHR 1	RMSE Total U	725 U	0.14 J	1260 U	354 U	252 U	3000 U	1150 U	240 U	252 U	N/A (1)	0
SHR 2	RMSE Total U	240 J	3250	1260 U	354 U	252 U	3000 U	150 J	240 U	252 U	N/A (1)	3400
SHR FLD BLK	RMSE Total U	180 U	123 U	263 U	738 U	525 U	625 U	240 U	500 U	525 U	N/A (1)	0
SHV 1	RMSE Total U	100 J	400 U	1050 U	205 U	210 U	2500 U	960 U	200 U	2340 U	N/A (1)	0
SHV 2	RMSE Total U	635 U	400 U	1050 U	205 U	210 U	2500 U	960 U	240 U	1770 U	N/A (1)	1770
SHV FLD BLK	RMSE Total U	159 U	123 U	263 U	738 U	525 U	625 U	240 U	500 U	525 U	N/A (1)	0
SP FLD BLK	RMSE Total U	159 U	123 U	263 U	738 U	525 U	625 U	240 U	500 U	525 U	N/A (1)	0
SP 1	RMSE Total U	635 U	490 U	1050 U	265 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0
SP 2	RMSE Total U	635 U	490 U	1050 U	265 U	210 U	2500 U	960 U	200 U	210 U	N/A (1)	0

(1) - Nitrided Esters not Analyzed

(2) - Explosives Compounds not Analyzed

**HWAAP - Hot Gas Pilot Study**  
**Post Test 17 - 800 Deg F, 48 Hrs**

EQUIPMENT	MATRIX	UNITS	AMMONIUM PICRATE
AP 1 R1	RINSE	Total ug	10000 U
AP 1 R2	RINSE	Total ug	10000 U
AP 1 R3	RINSE	Total ug	10000 U
AP 1 R4	RINSE	Total ug	10000 U
AP FLD BLNK	RINSE	Total ug	10000 U
CHMB WALL BLK	WIPE	Total ug	10.0 U
CHMB WALL W1	WIPE	Total ug	10.0 U
PB 1 R1	RINSE	Total ug	10000 U
PB 1 R2	RINSE	Total ug	10000 U
PB 1 R3	RINSE	Total ug	10000 U
PB 1 R4	RINSE	Total ug	10000 U
PB FLD BLNK	RINSE	Total ug	10000 U
SHR 1 R1	RINSE	Total ug	10000 U
SHR 1 R2	RINSE	Total ug	10000 U
SHR 1 R3	RINSE	Total ug	10000 U
SHR 1 R4	RINSE	Total ug	10000 U
SHR FLD BLK	RINSE	Total ug	10000 U
SHV 1 R1	RINSE	Total ug	10000 U
SHV 1 R2	RINSE	Total ug	10000 U
SHV 1 R3	RINSE	Total ug	10000 U
SHV 1 R4	RINSE	Total ug	10000 U
SHV FLD BLK	RINSE	Total ug	10000 U
SP FLD BLNK	RINSE	Total ug	10000 U
SP R1	RINSE	Total ug	10000 U
SP R2	RINSE	Total ug	10000 U
SP R3	RINSE	Total ug	10000 U
SP R4	RINSE	Total ug	10000 U

July 1990  
Revision: Final

TEST RUN 13  
500°F/6 HOURS

1311R2

HWAAP - Hot Gas Pilot Study  
Pre Test 18 - 500 Deg F, 6 Hrs

TEST ITEM	MATRIX	UNITS	HDR	GRX	1,3,6- TOL	1,3- DOL	NH	YET/VE	2,4,6- TOL	2,6- DIT	2,4- DIT	Estimated Estimate	TOTAL Estimate
CLAY PIPE	SOIL	Wt	1270 U	600 U	2000 U	500 U	4200 U	5000 U	10500 U	4000 U	4200 U	N/A (1)	0
CLAY PIPE	SOIL	Wt	127 U	60 U	200 U	50 U	420 U	500 U	1050 U	400 U	420 U	N/A (1)	4200
CP FLD BLK	RNISE	Total Wt	159 U	123 U	203 U	738 U	525 U	625 U	1300 U	500 U	525 U	N/A (1)	0
PF FLD BLK	RNISE	Total Wt	159 U	123 U	203 U	738 U	525 U	625 U	1300 U	500 U	525 U	N/A (1)	0
P3 1	RNISE	Total Wt	635 U	143 U	1050 U	295 U	210 U	2500 U	600 U	200 U	210 U	N/A (1)	0
P3 2	RNISE	Total Wt	635 U	143 U	1050 U	295 U	210 U	2500 U	600 U	200 U	210 U	N/A (1)	0
SHIP ALICE	WIFE	Total Wt	127 U	90 U	105 U	500 U	210 U	500 U	192 U	400 U	39 U	N/A (1)	326
SHIP ALICE	WIFE	Total Wt	4430	800 U	203 U	580 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	4430
SHIP ALICE	WIFE	Total Wt	12700 U	20300	20300 U	5000 U	4200 U	50000 U	4820	4000 U	4200 U	N/A (1)	37100
SHIP FLD BLK	WIFE	Total Wt	127 U	90 U	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SHIP FLD BLK	WIFE	Total Wt	127 U	203 U	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	0
SHIP FLD BLK	WIFE	Total Wt	635 U	493 U	105 U	235 U	210 U	250 U	1500	200 U	700	N/A (1)	1310
SHIP W1 W4	WIFE	Total Wt	210 J	143	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	249
SHIP W5 W8	WIFE	Total Wt	481	900 U	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	657
SHIP W5 W8	WIFE	Total Wt	127 U	1000	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	1630
SHIP2 SPICE H	RNISE	Total Wt	635 U	493 U	105 U	235 U	210 U	250 U	1500	200 U	700	N/A (1)	3000
SHIP2 W1 W4	WIFE	Total Wt	127 U	350 J	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	657
SHIP2 W5 W8	WIFE	Total Wt	127 U	900 U	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	1630
SHIP2 W5 W8	WIFE	Total Wt	127 U	900 U	203 U	500 U	420 U	500 U	192 U	400 U	420 U	N/A (1)	657
SHIP ALICE W2	WIFE	Total Wt	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	27.9	N/A (2)
SHIP FLD BLK	WIFE	Total Wt	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	N/A (2)	5.00 U	N/A (2)

(1) - N/A (2) - Explosives Compounds not Analyzed.

HWAAP - Hot Gas Pilot Study  
Post Test 18 - 600 Deg F, 6 Hrs

TEST ITEM	MATRIX	UNITS	HMX	RDX	1,3,5- Trib	1,3- DiB	NB	TETROL	2,4,6- TNT	2,6- DNT	2,4- DNT	Unanalyzed Compounds	TOTAL
CHRS WALL BL	WIPE	Total Uq	127 U	960 U	209 U	500 U	430 U	500 U	192 U	400 U	420 U	N/A (1)	0
CHRS WALL WI	WIPE	Total Uq	127 U	960 U	209 U	500 U	430 U	500 U	192 U	400 U	420 U	N/A (1)	0
CLAY PIPE	LOW	Uq/L	127 U	0 543 U	209 U	0.520 U	0.420 U	500 U	192 U	0.400 U	0.420 U	N/A (1)	0
CLAY PIPE BL	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	997	460 U	100 U	105 U	N/A (1)	0
PB 1 R1	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
PB 1 R2	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
PB 1 R3	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
PB 1 R4	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
PB FLD BULK	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
GRAP MATE WI	WIPE	Total Uq	127 U	960 U	209 U	500 U	430 U	500 U	192 U	400 U	420 U	N/A (1)	0
SHR 1 R1	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
SHR 1 R2	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
SHR 1 R3	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
SHR 1 R4	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
SHR FLD BULK	RINSE	Total Uq	318 U	245 U	523 U	148 U	105 U	1250 U	480 U	100 U	105 U	N/A (1)	0
SM FLD BULK	WIPE	Total Uq	127 U	960 U	209 U	500 U	430 U	500 U	192 U	400 U	420 U	N/A (1)	0

(1) - Unanalyzed Compounds not Analyzed

(2) - Excluded Excess not Analyzed



APPENDIX I  
EXAMPLE CALCULATIONS

1311R2

Appendix I contains the following calculations:

- Calculations to determine time for slab to reach temperature.
- Heat balance calculations for Test Runs T2, T3, and T5.



July 1990  
Revision: Final

**CALCULATIONS TO  
DETERMINE TIME FOR SLAB  
TO REACH TEMPERATURE**

1311R2

SHEET 1 of 6

CLIENT/SUBJECT _____	W.O. NO. _____
TASK DESCRIPTION <u>Time For Slab To Reach Temperature</u>	TASK NO. _____
PREPARED BY <u>NPS</u> DEPT <u>1311</u> DATE _____	APPROVED BY _____ DEPT _____ DATE _____
MATH CHECK BY _____ DEPT _____ DATE _____	
METHOD REV. BY _____ DEPT _____ DATE _____	

The following calculations have been prepared  
to determine the time required for items to reach  
target temperature.

#### Assumptions:

- 1) Rectangular slab will be evaluated
- 2) Length = 1 FT
- 3) Height = 1 FT
- 4) Material of Construction = Steel

Calculations will be prepared for 4 separate cases:

- 500 lb slab
- 1000 lb slab
- 1500 lb slab
- Slab that is as large as permissible in chamber (6 FT H x 20 FT L x 6 FT E)

Unsteady-state conditions exist. Slab will be placed  
at front of chamber (near door) in vicinity  
of air discharge duct (i.e., worst case -  
lowest air temperatures).

The heat transfer coefficient for the system was  
calculated to be 1.44 BTU/hr Ft<sup>2</sup> °F (see WORKSHEET -  
insulation calculations for flash chamber).

#### DATA:

$$\begin{aligned}k_{\text{steel}} &= 25.9 \text{ BTU/hr Ft}^2 (^\circ\text{F}/\text{Ft}) @ 212^\circ\text{F} \text{ (Bennett; Myers, 2nd Ed, Page 773)} \\C_{\text{steel}} &= 0.12 \text{ BTU/lb } ^\circ\text{F} \text{ (Bennett; Myers, 2nd Ed, Page 773)} \\P_{\text{steel}} &= 489 \text{ lb/Ft}^3 \text{ (Bennett; Myers, 2nd Ed, Page 773)}\end{aligned}$$

SHEET 2 of 6

CLIENT/SUBJECT _____	W.O. NO. _____
TASK DESCRIPTION <u>Time for Slab to Reach Temperature</u>	TASK NO. _____
PREPARED BY <u>NJS</u> DEPT. <u>1311</u> DATE _____	APPROVED BY _____
MATH CHECK BY _____ DEPT. _____ DATE _____	
METHOD REV. BY _____ DEPT. _____ DATE _____	DEPT. _____ DATE _____

To estimate time, the "Chart for determining the temperature history of points at the centers of rectangular shapes" was utilized (Process Heat Transfer, Kern, p. 650). A copy of the chart is shown on Figure 18-11.

$$\text{In chart, } Y = \frac{T_s - t_{1/2}}{T_s - t_o}$$

where  $T_s$  = temperature of surrounding (air)  
 $t_{1/2}$  = temperature of the center plane  
 $t_o$  = initial temperature

In this application:

$$\begin{aligned} T_s &= 550^\circ\text{F} \text{ (during pour-up)} \\ t_{1/2} &= 500^\circ\text{F} \\ t_o &= 70^\circ\text{F} \end{aligned}$$

$$\text{In chart, } X = \frac{hL}{2k}$$

where  $h$  = heat transfer coefficient  
 $L$  = principal depth  
 $k$  = thermal conductivity

For illustration, 4 masses of steel are evaluated.

$$L = \frac{m}{\rho H \ell}$$

where  $H$  = height of slab (1 FT in cases 1, 2, 3; 6 FT in case 4)  
 $\ell$  = length of slab (1 FT in cases 1, 2, 3; 6 FT in case 4)



SHEET 3 of 4

CLIENT/SUBJECT \_\_\_\_\_ W.O. NO. \_\_\_\_\_

TASK DESCRIPTION Time for Slab to Reach Temperature TASK NO. \_\_\_\_\_

PREPARED BY NDS DEPT 1911 DATE \_\_\_\_\_ APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

Therefore,

$$X = \frac{h L}{2 k}$$

$$= \frac{h m}{2 k \rho h u}$$

On chart, curve =  $\frac{4 \alpha b}{L^2}$

where:  $\alpha = \frac{k}{C_p}$

$C_p$  = Specific heat

$\theta$  = time

Therefore, curve =  $\frac{4 k \theta}{C_p \left( \frac{m}{\rho h u} \right)^2}$

Case 1  $m = 500 \text{ lb}$

$$Y = \frac{T_s - t_{1/2}}{T_s - t_s} = \frac{550^\circ \text{F} - 500^\circ \text{F}}{550^\circ \text{F} - 70^\circ \text{F}} = 0.10$$

$$X = \frac{h m}{2 k \rho h u}$$

$X = \frac{1.44 \text{ BTU}}{\text{hr Ft}^2 ^\circ \text{F}}$	$\frac{500 \text{ lb}}{\text{Ft}^3}$	$\frac{\text{hr Ft}^2 ^\circ \text{F}}{2}$	$\frac{\text{Ft}^3}{25.9 \text{ BTU Ft}}$	$\frac{1 \text{ Ft}}{489 \text{ lb}}$	$\frac{1 \text{ Ft}}{1 \text{ Ft}}$
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$$X = 0.028$$



SHEET 4 of 6

CLIENT/SUBJECT \_\_\_\_\_ W.O. NO. \_\_\_\_\_

TASK DESCRIPTION Time for Slab to Reach Temperature TASK NO. \_\_\_\_\_

PREPARED BY NPS DEPT 1811 DATE \_\_\_\_\_ APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

At  $x = 0.028$  and  $y = 0.10$  there is no curve.

Extrapolating (For  $x = 0.028$ )

$$\text{Curve} = \frac{0.046 - 0.057}{50 - 45} = \frac{0.046 - 0.028}{50 - \text{curve}}$$

$$\text{Curve} = 61$$

$$b1 = \frac{4 \times 0}{C_p \left( \frac{m}{P_{he4}} \right)^2} = \frac{4 \times 25.9 \text{ BTU F.} \times 0}{\text{hr F}^2 \text{ in}} \times \frac{16 \text{ OF}}{0.12 \text{ BTU}} \times \frac{\left( \frac{489 \text{ lb/Ft}^3 \right) (1 \text{ ft})}{(500 \text{ lb})^2}$$

$$0 = 0.074 \text{ hr (4.4 min)}$$

Case 2  $m = 1000 \text{ lb}$

$$y = 0.10$$

$$X = \frac{h m}{2 \times P_{he4}} = \frac{1.44 \text{ BTU} \times 1000 \text{ lb}}{\text{hr F}^2 \text{ OF}} \times \frac{1 \text{ hr F}^2 \text{ OF}}{2 \times 25.9 \text{ BTU F.}} \times \frac{1 \text{ F}^3}{489 \text{ lb}} \times \frac{1 \text{ F}^3}{1 \text{ F}^3}$$

$$X = 0.057$$

At  $x = 0.057$  and  $y = 0.10$

$$\text{Curve} = 42$$



SHEET 5 of 6

CLIENT/SUBJECT \_\_\_\_\_ W.C. NO. \_\_\_\_\_  
 TASK DESCRIPTION Time for Slab to Reach Temperature TASK NO. \_\_\_\_\_  
 PREPARED BY NPS DEPT ISU DATE \_\_\_\_\_ APPROVED BY \_\_\_\_\_  
 MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_  
 METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

$$42 = \frac{4 \times \theta}{C_p \left( \frac{m}{\rho h_c \ell} \right)^2} = \frac{4}{\frac{1}{\text{hr Ft}^2 \text{ } ^\circ\text{F}}} \left| \frac{25.9 \text{ BTU Ft}}{\text{hr Ft}^2 \text{ } ^\circ\text{F}} \right| \left| \frac{\theta}{0.12 \text{ BTU}} \right| \left| \frac{[(499 \text{ lb/Ft}^3)(1 \text{ Ft})(1 \text{ Ft})]^2}{(1000 \text{ lb})^2} \right|$$

$$\theta = 0.20 \text{ hr (12 minutes)}$$

CASE 3  $m = 1500 \text{ lb}$

$$Y = 0.10$$

$$X = \frac{h m}{2 k \rho h_c \ell} = \frac{1.44 \text{ BTU}}{\text{hr Ft}^2 \text{ } ^\circ\text{F}} \left| \frac{1500 \text{ lb}}{2} \right| \left| \frac{\text{hr Ft}^2 \text{ } ^\circ\text{F}}{25.9 \text{ BTU Ft}} \right| \left| \frac{\text{Ft}^3}{499 \text{ lb}} \right| \left| \frac{1 \text{ Ft}}{1 \text{ Ft}} \right|$$

$$X = 0.085$$

At  $Y = 0.10$  and  $X = 0.085$ , Curve = 40

$$40 = \frac{4 \times \theta}{C_p \left( \frac{m}{\rho h_c \ell} \right)^2} = \frac{4}{\frac{1}{\text{hr Ft}^2 \text{ } ^\circ\text{F}}} \left| \frac{25.9 \text{ BTU Ft}}{\text{hr Ft}^2 \text{ } ^\circ\text{F}} \right| \left| \frac{\theta}{0.12 \text{ BTU}} \right| \left| \frac{[(499 \text{ lb/Ft}^3)(1 \text{ Ft})(1 \text{ Ft})]^2}{(1500 \text{ lb})^2} \right|$$

$$\theta = 0.43 \text{ hr (26 min)}$$

CASE 4 SLAB = 6 FT H x 20 FT L x 6 FT D

$$m = \frac{(6 \text{ Ft} \times 20 \text{ Ft} \times 6 \text{ Ft})}{\text{Ft}^3} \left| \frac{499 \text{ lb}}{\text{Ft}^3} \right| = 352,080 \text{ lb}$$

$$Y = 0.10$$

$$X = \frac{h m}{2 k \rho h_c \ell} = \frac{1.44 \text{ BTU}}{\text{hr Ft}^2 \text{ } ^\circ\text{F}} \left| \frac{352,080 \text{ lb}}{2} \right| \left| \frac{\text{hr Ft}^2 \text{ } ^\circ\text{F}}{25.9 \text{ BTU Ft}} \right| \left| \frac{\text{Ft}^3}{499 \text{ lb}} \right| \left| \frac{6 \text{ Ft}}{20 \text{ Ft}} \right|$$

$$X = 0.17$$

At  $Y = 0.10$  and  $X = 0.17$ , Curve = 20 =  $\frac{4}{\frac{1}{\text{hr Ft}^2 \text{ } ^\circ\text{F}}} \left| \frac{25.9 \text{ BTU Ft}}{\text{hr Ft}^2 \text{ } ^\circ\text{F}} \right| \left| \frac{\theta}{0.12 \text{ BTU}} \right| \left| \frac{(6 \text{ Ft})^2}{(6 \text{ Ft})^2} \right|$

$$\theta = 0.83 \text{ hr (50 min)}$$

Time for Slab to Reach Temperature  
NPS 10:11

Sheet 6 of 6

350

PROCESS HEAT TRANSFER

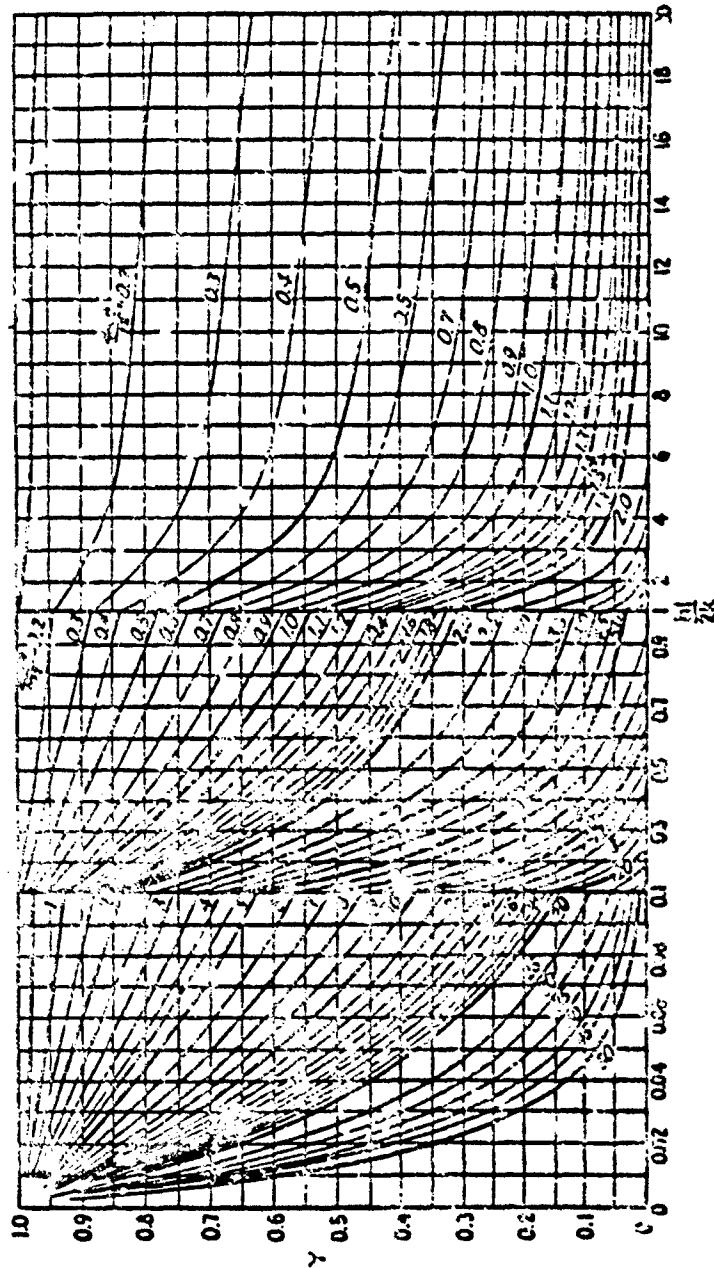


FIG. 18.11. Chart for determining the temperature history of points at the corners of rectangular slabs. (Neuman, Industrial Heat Treating Chemistry, 2nd Edition.)

July 1969  
Revision: Final

## HEAT BALANCE CALCULATIONS

### TEST RUNS

2, 3, & 5

1311R2



# WILSON

SHEET 1 of 20

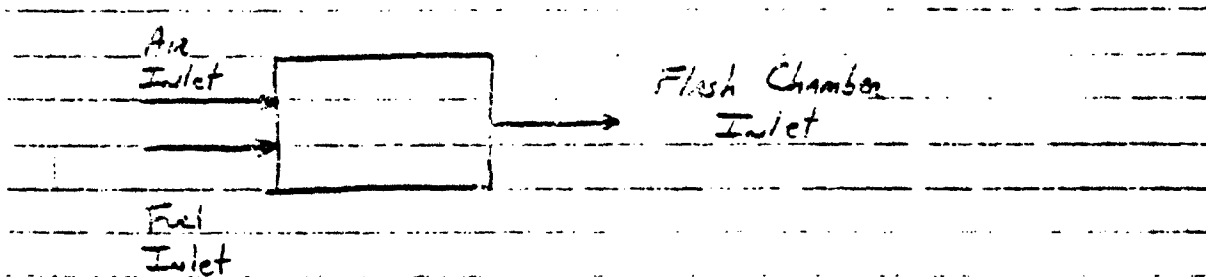
CLIENT/SUBJECT USATHAMA W.O. NO. 7000-00-24

TASK DESCRIPTION Test Run #2 Heat Balance TASK NO. 2

PREPARED BY M. Cosmas DEPT. 1711 DATE 14 Feb 70 APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_



Average Inlet Air Flow PI-202 1.05 in<sup>3</sup>/min ± .18

Test Elapsed Time 1400-4400

Average Fuel Gas Pressure PI 310 1.70 psig ± .14

Test Elapsed Time 1400-4400

Average Flash Chamber Inlet measured data

1566 dscfm ± 74%

312 °F (733 °F on process thermocouple)

4400 wacfm

1.8% CO<sub>2</sub> by volume dry basis

17.22 O<sub>2</sub>

80.22 N<sub>2</sub>

3.22 H<sub>2</sub>O by volume

$$\text{CO}_2 (1566 \text{ dscfm}) (.018 \text{ CO}_2) (.11378 \text{ lb/scf}) = 3.21 \text{ lb/min}$$

$$\text{O}_2 (1566 \text{ dscfm}) (.1720) (.09275 \text{ lb/scf}) = 22.28 \text{ lb/min}$$

$$\text{N}_2 (1566 \text{ dscfm}) (.802 \text{ N}_2) (.07246 \text{ lb/scf}) = 91.50 \text{ lb/min}$$

$$\text{H}_2\text{O} \quad x = .032$$

$$1566 + x$$

$$x = (.77 \text{ cfm}) (.49654 \text{ lb/scf}) = 2.41 \text{ lb/min}$$

113.40 lb/min



SHEET 2 of 10

CLIENT SUBJECT USATHAMA W.D. NO. 7602-00-24  
 TASK DESCRIPTION Test Run #2 Heat Balance TASK NO. 2  
 PREPARED BY M. Colman DEPT. 1811 DATE 16 Feb 90  
 APPROVED BY \_\_\_\_\_  
 MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_  
 METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Correction to gas flow for altitude

$$\text{corr} = e^{(.000036024(4500\text{ft}))} = 1.176$$

$$\text{Design location} = e^{(.000036024(1750\text{ft}))} = 1.066$$

$$\text{Density ratios} = 1.176 / 1.066 = 1.103$$

$$P_{\text{scat}} = (P_{\text{act}} / \rho_{\text{scat}}) (P_{\text{act}})$$

$$= 1.103 (1.70 \text{ psig})$$

$$= 1.875 \text{ psig}$$

From Vendor Graph 802 1.875 psig = 1.75 mm H<sub>2</sub>O/hr  
 LHV

$$(1,750,000 \text{ BTU/hr}) / (2316 \text{ BTU/scf}) = 753$$

$$756 \text{ scf/hr} = 12.6 \text{ scfm propane}$$

$$(12.59 \text{ scfm}) (0.1196 \text{ lb/scf}) = 1.51 \text{ lb/min}$$

Combustion Air Flow by

$$\text{Flow} = 1433 + 406 (\ln(1.05 \text{ mmHg})) = 1453 \text{ scfm}$$

$$(1450 \text{ scfm}) (0.075 \text{ lb/scf}) = 105 \text{ lb/min}$$

Moisture load under worst conditions

$$60^\circ \text{F} = 0.01 \text{ lb H}_2\text{O/lb air}$$

**WISTEN**

SHEET 3 of 90

CLIENT/SUBJECT US-TH 3m.4 S.O. NO. 7000-00-24  
TASK DESCRIPTION Test Run #2 Heat Balance TASK NO. 2  
PREPARED BY M. Cassino DEPT 1811 DATE 16 Feb 90  
MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_  
METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_  
APPROVED BY \_\_\_\_\_  
CSPT \_\_\_\_\_ DATE \_\_\_\_\_

Maximum water Load

$$(105 \text{ lb/min}) (0.01 \text{ } ^{15}\text{H}_2\text{O/lb air}) = 1.05 \text{ } ^{15}\text{lb/min}$$

Mass Balance Check

$$\frac{(119.40 \text{ } ^{15}\text{lb/min}) - [1.51 \text{ } ^{15}\text{lb/min} + 105 \text{ } ^{15}\text{lb/min} + 1.05 \text{ } ^{15}\text{lb/min}]}{117.4 \text{ } ^{15}\text{lb/min}}$$

= 9.92 % closure within  
measurement  
errors

Combustion of Propane 1% basis

CO<sub>2</sub> 2.99 lb/lb

H<sub>2</sub>O 1.63 lb/lb

N<sub>2</sub> 12.07 lb/lb

Total 15.69 lb/lb - 1 lb/lb = 15.69 lb/lb comb air

Combustion of Fuel

CO<sub>2</sub> (1.51 <sup>15</sup>lb/min) (2.99 lb/lb) = 4.51 <sup>15</sup>lb/min

H<sub>2</sub>O (1.51 <sup>15</sup>lb/min) (1.63 lb/lb) + (1.05 <sup>15</sup>lb/min) = 3.51 <sup>15</sup>lb/min

N<sub>2</sub> (1.51 <sup>15</sup>lb/min) (12.07 lb/lb) = 18.23 <sup>15</sup>lb/min

Excess Air = inlet air - combustion air

$$(105 \text{ } ^{15}\text{lb/min}) - (1.51 \text{ } ^{15}\text{lb/min}) (15.69 \text{ } ^{15}\text{lb/lb}) = 81.31 \text{ } ^{15}\text{lb/min}$$

$$\text{O}_2 = (81.31 \text{ } ^{15}\text{lb/min}) (0.21 \text{ } ^{15}\text{O}_2) = 17.07 \text{ } ^{15}\text{lb/min}$$

**WILSON**

CLIENT/SUBJECT Unlabeled

W.D. NO. 7000-00-27

TASK DESCRIPTION Test Run #2 Heat Balance

TASK NO. 2

PREPARED BY M. Cosmos DEPT 1911 DATE 16 Feb 90

APPROVED BY

WITH CHECK BY DEPT DATE

METHOD REV. BY DEPT DATE

DEPT DATE

Heat Balance

Heat Released by Fuel

$$(1.51 \text{ lb/min}) (19,944 \text{ BTU/lb}) = 30,115 \text{ BTU/min}$$

Heat Absorbed by Combustion Products

$$\text{CO}_2 (4.51 \text{ lb/min}) (0.225 \text{ BTU/lb}^\circ\text{F}) (812-70^\circ\text{F}) = 753 \text{ BTU/min}$$

$$\text{H}_2\text{O} (3.51 \text{ lb/min}) (0.478 \text{ BTU/lb}^\circ\text{F}) (812-70^\circ\text{F}) = 1,244 \text{ BTU/min}$$

$$\text{N}_2 (18.23 \text{ lb/min}) (0.25 \text{ BTU/lb}^\circ\text{F}) (812-70^\circ\text{F}) = 3,382 \text{ BTU/min}$$

Heat Absorbed by Xs Air

$$(81.31 \text{ lb/min}) (0.24 \text{ BTU/lb}^\circ\text{F}) (812-70^\circ\text{F}) = 14,480 \text{ BTU/min}$$

19,852 BTU/min

Radiation Loss

Surface Area

$$\pi (20 \text{ inch}) \left( \frac{\pi}{12 \text{ inch}} \right) (6.5 \text{ ft} + 24.5 \text{ ft}) = 162 \text{ ft}^2$$

$$(162 \text{ ft}^2) (2.8 \text{ BTU/hr ft}^2 \text{ }^\circ\text{F}) (200^\circ\text{F} - 70^\circ\text{F}) \left( \frac{1}{60 \text{ min}} \right) = 1,742 \text{ BTU/min}$$

Heat Balance Comparison

$$(30,115 \text{ BTU/min}) - (19,852 \text{ BTU/min} + 1,742 \text{ BTU/min}) = 2,239 \text{ BTU/min}$$

30,115 BTU/min

CLIENT/SUBJECT USATHAMA W.O. NO. 2000-00-24

TASK DESCRIPTION Test Run # 2 Heat Balance TASK NO. 2

PREPARED BY M. Cosmas DEPT. 1511 DATE 16 Feb 93

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT. _____	DATE _____

Average Flash Chamber Outlet

2067 dscfm  $\pm 5\%$   
 391 °F  $\pm 37^\circ\text{F}$   
 3917 wacfm  
 1.13 % CO<sub>2</sub>  
 15.97 % O<sub>2</sub>  
 81.25 % N<sub>2</sub>  
 2.87 % H<sub>2</sub>O

CO<sub>2</sub> (2067 dscfm)(0.0113)(0.1138<sup>lb</sup>/scf) = 2.66<sup>lb</sup>/min

O<sub>2</sub> (2067 dscfm)(0.1597)(0.0827<sup>lb</sup>/scf) = 27.30<sup>lb</sup>/min

N<sub>2</sub> (2067 dscfm)(0.8125)(0.07240<sup>lb</sup>/scf) = 121.59<sup>lb</sup>/min

H<sub>2</sub>O  $\frac{x}{2267 + x} = 0.0287$

$x = (61.08 \text{ scfm})(0.04654 \text{ }^{lb}/\text{scf}) = 2.84 \text{ }^{lb}/\text{min}$

Total Exit Gas Flow 154.39<sup>lb</sup>/min

Leakage Estimate

$\frac{154.39 \text{ }^{lb}/\text{min} - 119.40 \text{ }^{lb}/\text{min}}{154.39 \text{ }^{lb}/\text{min}} = 22.67\%$

Leakage Volume

$(154.39 \text{ }^{lb}/\text{min} - 119.40 \text{ }^{lb}/\text{min}) = 34.99 \text{ }^{lb}/\text{min}$

**WESTERN**

SHEET 6 of 15

CLIENT/SUBJECT USATHAMA W.O. NO. 7600-00-24  
TASK DESCRIPTION Test Run #2 Heat Balance TASK NO. 2  
PREPARED BY M. Cosmos DEPT 1811 DATE 16 Feb 99  
MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_  
METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT	DATE

Heat Balance Around Test Chamber

Heat Lost by Process Gas

$$\text{CO}_2 \left( \frac{2.21 + 2.66}{2} \right) (0.225 \text{ scfm/lb}^\circ\text{F}) (812 - 391^\circ\text{F}) = 278 \frac{\text{BTU}}{\text{min}}$$

$$\text{H}_2\text{O} \left( \frac{2.41 + 2.84}{2} \right) (0.478 \text{ scfm/lb}^\circ\text{F}) (812 - 391^\circ\text{F}) = 528 \frac{\text{BTU}}{\text{min}}$$

$$\text{N}_2 \left( \frac{91.50 + (121.59 - .79(34.99))}{2} \right) (0.25) (812 - 391^\circ\text{F}) = 9,759 \frac{\text{BTU}}{\text{min}}$$

$$\text{O}_2 \left( \frac{22.28 + (27.30 - .71(34.99))}{2} \right) (0.24) (812 - 391^\circ\text{F}) = 2,134 \frac{\text{BTU}}{\text{min}}$$

$$\text{Total Heat Lost by Hot Gas} = 12,599 \frac{\text{BTU}}{\text{min}}$$

Heat Absorbed by Leak Air

$$(34.99 \text{ scfm/min}) (0.24 \text{ scfm/lb}^\circ\text{F}) (391 - 70^\circ\text{F}) = 2,696 \frac{\text{BTU}}{\text{min}}$$

Heat Lost Through Walls

$$(12,599 \text{ BTU/min}) - (2,696 \text{ BTU/min}) = 9,903 \frac{\text{BTU}}{\text{min}}$$
$$= 594,202 \frac{\text{BTU}}{\text{hr}}$$

CLIENT/SUBJECT USATRUMA A.O. NO 7060-00-24

TASK DESCRIPTION Test Run #2 Heat Balance TASK NO. \_\_\_\_\_

PREPARED BY M. Cosmos DEPT 1311 DATE \_\_\_\_\_ APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

Average Fuel Gas Pressure 6.34 psig

Average T.O. Exit Gas \_\_\_\_\_

2467 dscfm  $\pm$  5.5%  
 1718 °F (  
 12,500 wafm  
 6.5 % CO<sub>2</sub>  
 10.7 % O<sub>2</sub>  
 32.8 % N<sub>2</sub>  
 8.6 % H<sub>2</sub>O

CO<sub>2</sub> (2467 dscfm) (0.065 CO<sub>2</sub>) (.11378 <sup>15</sup>/dscf) = 18.2 <sup>15</sup>/min

O<sub>2</sub> (2467 dscfm) (.107 O<sub>2</sub>) (.08275 <sup>15</sup>/dscf) = 21.8 <sup>15</sup>/min

N<sub>2</sub> (2467 dscfm) (.828 N<sub>2</sub>) (.07240 <sup>15</sup>/dscf) = 147.9 <sup>15</sup>/min

H<sub>2</sub>O  $\frac{x}{2467 + x} = .086$

$x = (2467 \text{ dscfm}) (.04654 \text{ }^{15}/\text{dscf}) = 114.80 \text{ }^{15}/\text{min}$

198.7 <sup>15</sup>/min

GAS FLOW

P<sub>gatch</sub> = (1.103) (6.34 psia)

= 6.99 psia = 4.5 mm BTU/min



CLIENT/SUBJECT USATH4m.1 W.O. NO. 7000-00-24 SHEET 3 of 10  
 TASK DESCRIPTION Test Run #2 Test Balance TASK NO. \_\_\_\_\_  
 PREPARED BY M. Cosmos DEPT 1811 DATE \_\_\_\_\_ APPROVED BY \_\_\_\_\_  
 MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_  
 METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

$$(4,570,000 \text{ Btu/hr}) / 2316 \text{ }^{\circ}\text{F} = 1943 \text{ scfh}$$

$$32.4 \text{ scfm}$$

$$(32.4 \text{ scfm})(0.1196 \text{ }^{\circ}\text{F}) = 3.87 \text{ }^{\circ}\text{F/min}$$

Air Leakage

$$198.7 \text{ }^{\circ}\text{F/min} - (154.4 \text{ }^{\circ}\text{F/min} + 3.87 \text{ }^{\circ}\text{F/min}) = 40.4 \text{ }^{\circ}\text{F/min}$$

$$20.32$$

Combustion Product

$$\text{CO}_2 (3.87 \text{ }^{\circ}\text{F/min})(2.99 \text{ }^{\circ}\text{F}) = 11.57 \text{ }^{\circ}\text{F/min}$$

$$\text{H}_2\text{O} (3.87 \text{ }^{\circ}\text{F/min})(1.63 \text{ }^{\circ}\text{F}) = 6.31 \text{ }^{\circ}\text{F/min}$$

$$\text{N}_2 (3.87 \text{ }^{\circ}\text{F/min})(12.07 \text{ }^{\circ}\text{F}) = 46.71 \text{ }^{\circ}\text{F/min}$$

$$\text{Air Consumed} (3.87 \text{ }^{\circ}\text{F/min})(15.69 \text{ }^{\circ}\text{F}) = 60.72 \text{ }^{\circ}\text{F/min}$$

Mass Balance Check

$$\text{CO}_2 \quad 18.2 \text{ }^{\circ}\text{F/min} - (11.57 \text{ }^{\circ}\text{F/min} + 2.99 \text{ }^{\circ}\text{F/min}) = 20.32$$

$$18.2 \text{ }^{\circ}\text{F/min}$$

$$\text{H}_2\text{O} \quad 10.80 \text{ }^{\circ}\text{F/min} - (6.31 \text{ }^{\circ}\text{F/min} + 2.62 \text{ }^{\circ}\text{F/min}) = 17.32$$

$$10.8 \text{ }^{\circ}\text{F/min}$$

$$\text{N}_2 \quad 142.9 \text{ }^{\circ}\text{F/min} - (421.59 + .79(40.4 \text{ }^{\circ}\text{F/min})) = -3.82$$

$$142.9 \text{ }^{\circ}\text{F/min}$$



CLIENT/SUBJECT USATHAMA W.O. NO. 7000-00-24

TASK DESCRIPTION Test Run #2 Heat Balance TASK NO. \_\_\_\_\_

PREPARED BY M. Cosmos DEPT. 1311 DATE 24 Feb 90

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT. _____	DATE _____

$$O_2 \quad \frac{(21.8^{lb/min}) - (27.30^{lb/min} + 21(40.4^{lb/min}) - 21(60.72))}{21.8^{lb/min}} = -5.66\%$$

## Heat Balance Check

### Heat Released by Fuel

$$(3.87^{lb/min})(19,944^{BTU/lb}) = 77,183^{BTU/min}$$

### Heat Absorbed by F.C. Exit Gases

$$CO_2 \quad (2.94^{lb/min})(0.225^{BTU/lb \cdot F})(1718 - 391^{F}) = 87.8^{BTU/min}$$

$$H_2O \quad (2.62^{lb/min})(0.478^{BTU/lb \cdot F})(1718 - 391^{F}) = 1662^{BTU/min}$$

$$N_2 \quad (121.59^{lb/min})(.25^{BTU/lb \cdot F})(1718 - 391^{F}) = 40337^{BTU/min}$$

$$O_2 \quad (27.30 - 21(60.72))(.22^{BTU/lb \cdot F})(1718 - 391^{F}) = 4,247^{BTU/min}$$

$$46,334^{BTU/min}$$

### Heat Absorbed by Combustion Products

$$CO_2 \quad (11.57^{lb/min})(0.225^{BTU/lb \cdot F})(1718 - 391^{F}) = 3455^{BTU/min}$$

$$H_2O \quad (6.31^{lb/min})(0.478^{BTU/lb \cdot F})(1718 - 391^{F}) = 4002^{BTU/min}$$

$$7457^{BTU/min}$$

### Heat Absorbed by Leak Air

$$Air \quad (40.4^{lb/min})(0.24^{BTU/lb \cdot F})(1787 - 73^{F}) = 16,648^{BTU/min}$$



SHEET 10 of 10

CLIENT/SUBJECT USAT43M9 W.O. NO. 7000-00-27TASK DESCRIPTION Test Run #2 Heat Balance TASK NO. \_\_\_\_\_PREPARED BY M. Cosmis DEPT. 1811 DATE 24 Feb 90

MATH CHECK BY. \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT. _____	DATE _____

Radiation LossesSurface Area

$$\pi (5 \text{ ft})(20 \text{ ft}) = 314 \text{ ft}^2$$

Heat Loss

$$(314 \text{ ft}^2)(2.8 \text{ BTU/hr ft}^2 \text{ } ^\circ\text{F})(300-70 \text{ } ^\circ\text{F})(\frac{1}{60 \text{ min}}) = 3370 \frac{\text{BTU}}{\text{min}}$$

Total Losses

$$(46,334 \frac{\text{BTU}}{\text{min}} + 745 \frac{\text{BTU}}{\text{min}} + 16,648 \frac{\text{BTU}}{\text{min}} + 3370 \frac{\text{BTU}}{\text{min}}) = 73,809 \frac{\text{BTU}}{\text{min}}$$

Closure Balance

$$\frac{(77,193 \frac{\text{BTU}}{\text{min}} - 73,809 \frac{\text{BTU}}{\text{min}})}{77,193 \frac{\text{BTU}}{\text{min}}} = 4.42$$

CLIENT/SUBJECT USATHAMA W.O. NO. 7200-20-24

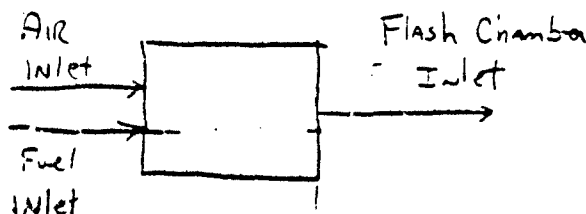
TASK DESCRIPTION Test Run #3 Heat Balance TASK NO. \_\_\_\_\_

PREPARED BY M. Cosgrove DEPT. 1811 DATE 20 Sep 89

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT. _____	DATE _____



Average Inlet Air flow PI202 1.11 inwg ±

Average Fuel Gas Pressure PI310 2.8 lpsig ±

Average Flash Chamber Inlet measured data

1633 dscfm ± 7%

1031 °F (959°F on process thermometer)

5533 wacfm

2.1 % CO<sub>2</sub> by Volume d.basis

16.3 % O<sub>2</sub> by Volume d.basis

31.5 % N<sub>2</sub> by Volume d.basis

3.2 % H<sub>2</sub>O by Volume

$$\text{CO}_2 (1633 \text{ dscfm}) (.021 \text{ CO}_2) (.11378 \text{ lb/scf}) = 3.90 \text{ lb/min}$$

$$\text{O}_2 (1633 \text{ dscfm}) (.163 \text{ O}_2) (.08275 \text{ lb/scf}) = 22.03 \text{ lb/min}$$

$$\text{N}_2 (1633 \text{ dscfm}) (.815 \text{ N}_2) (.07210 \text{ lb/scf}) = 96.36 \text{ lb/min}$$

$$\text{H}_2\text{O} \quad \frac{x}{1633 \text{ scfm} + x} = .032$$

$$x = (53.98 \text{ cfm}) (.04654 \text{ lb/l}) = 2.51 \text{ lb/min}$$

124.80 lb/min

# WISCONSIN

SHEET 2 of 11

CLIENT/SUBJECT <u>USATHAMA</u>			W.O. NO. <u>7000-CO-24</u>	
TASK DESCRIPTION <u>Test Run #3 Heat Balance</u>			TASK NO. _____	
PREPARED BY <u>M. P. Smith</u>	DEPT. <u>1811</u>	DATE <u>205089</u>	APPROVED BY _____ DEPT. _____ DATE _____	
MATH CHECK BY _____	DEPT. _____	DATE _____		
METHOD REV. BY _____	DEPT. _____	DATE _____		

Correction to gas flows for Altitude

$$\text{corr} = e^{(.0000360286(4500\text{ft}))} = 1.176$$

$$\text{Design location} = e^{(.0000360286(1070\text{ft}))} = 1.066$$

$$\text{Density ratios} = 1.176 / 1.066 = 1.103$$

$$\begin{aligned} P_{\text{graph}} &= (P_{\text{act}} / P_{\text{norm}})(P_{\text{act}}) \\ &= 1.103 (2.81 \text{ psig}) \\ &= 3.10 \text{ psig} \end{aligned}$$

$$\text{From vendor graph 802 } 3.10 \text{ psig} = 2.15 \text{ MM BTU/hr LHV}$$

$$2,150,000 \text{ BTU/hr} / (2316 \text{ BTU/lb}) =$$

$$928 \text{ scfh} = 15.47 \text{ scfm propane}$$

$$(15.47 \text{ scfm})(0.1196 \text{ lb/scf}) = 1.85 \text{ lb/min}$$

Combustion Airflow by correlation curve

$$\text{Flow} = 1433 \pm 40.6 (\ln(1.11/\text{mag})) = 1475 \text{ scf}$$

$$(1475 \text{ scfm})(0.075 \text{ lb/scf}) = 108.7 \text{ lb/min}$$

Moisture loading under worst observed

$$\text{Conditions } 60^\circ\text{F} = .01 \text{ lb H}_2\text{O/lb dA}$$

# WILSON

SHEET 3 of 11

CLIENT/SUBJECT USATHAMA

W.O. NO. 7000-00-24

TASK DESCRIPTION \_\_\_\_\_

TASK NO. \_\_\_\_\_

PREPARED BY \_\_\_\_\_

DEPT \_\_\_\_\_

DATE \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_

DEPT \_\_\_\_\_

DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_

DEPT \_\_\_\_\_

DATE \_\_\_\_\_

APPROVED BY

DEPT \_\_\_\_\_

DATE \_\_\_\_\_

Maximum water / sec

$$(108.7 \text{ lb/min})(.01 \text{ lb}_{\text{H}_2\text{O}}/\text{lb}_{\text{A}}) = 1.1 \text{ lb/min H}_2\text{O}$$

Mass Balance Check out-in / out =

$$\frac{124.80 \text{ lb/min} - (1.85 \text{ gal} + 108.7 \text{ Air} + 1.1 \text{ H}_2\text{O})}{124.8 \text{ lb/min}} =$$

10.5% closure within measurement errors

Combustion of Propane one lb bases

CO<sub>2</sub> 2.99 lb/lb

H<sub>2</sub>O 1.63 lb/lb

N<sub>2</sub> 12.07 lb/lb

$$\text{Total } 16.69 \text{ lb/lb} - 1 \text{ lb/lb} = 15.69 \text{ lb/lb}$$

Combustion of Fuel

$$\text{CO}_2 = (1.85)(2.99 \text{ lb/lb}) = 5.53 \text{ lb/min}$$

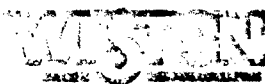
$$\text{H}_2\text{O} = (1.85)(1.63 \text{ lb/lb}) = 3.02 + 1.1 = 4.12 \text{ lb/min}$$

$$\text{N}_2 = (1.85)(12.07 \text{ lb/lb}) = 22.33$$

Excess Air

$$(108.7 \text{ lb/min} - (1.85 \text{ lb/min} \times 15.69 \text{ lb/min})) = 79.57 \text{ lb/min}$$

$$\text{O}_2 = (79.57 \text{ lb/min})(.21) = 16.73 \text{ lb/min}$$



CLIENT/SUBJECT USATAMA W.O. NO. 7000-00-2V  
 TASK DESCRIPTION Test Run #3 - Heat Balance TASK NO. \_\_\_\_\_  
 PREPARED BY M. Casanova DEPT RII DATE 21 Sep 69 APPROVED BY \_\_\_\_\_  
 MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_  
 METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

## Heat Balance

### Heat Released by Fuel

$$(1.85 \text{ lb/min})(19,944 \text{ BTU/lb}) = 36,896 \text{ BTU/min}$$

### Heat Absorbed by Combustion Products

$$\text{CO}_2 (5.53 \text{ lb/min})(0.225 \text{ BTU/lb}^\circ\text{F})(1031-70^\circ) = 1,196 \text{ BTU/min}$$

$$\text{H}_2\text{O} (4.12 \text{ lb/min})(0.478 \text{ BTU/lb}^\circ\text{F})(1031-70) = 1,893 \text{ BTU/min}$$

$$\text{N}_2 (22.33 \text{ lb/min})(0.25 \text{ BTU/lb}^\circ\text{F})(1031-70) = 5,365 \text{ BTU/min}$$

$$\text{Ex Air} (79.67 \text{ lb/min})(0.24 \text{ BTU/lb}^\circ\text{F})(1031-70) = 18,375 \text{ BTU/min}$$

---


$$26,829 \text{ BTU/min}$$

### Radiation Losses

#### Surface Area

$$\pi (20 \text{ inch}) \left( \frac{1 \text{ ft}}{12} \right) (6.5 \text{ ft} + 24.5 \text{ ft}) = 162 \text{ ft}^2$$

$$(162 \text{ ft}^2)(23 \text{ BTU/hr ft}^2)(300^\circ\text{F} - 70^\circ\text{F}) \left( \frac{1 \text{ hr}}{60 \text{ min}} \right) = 1,742 \text{ BTU/min}$$

### Heat Balance Comparison

$$\frac{(36,896 \text{ BTU/min}) - (26,829 + 1,742)}{36,896 \text{ BTU/min}} = 22.6\% \text{ close}$$

SHEET 5 of 11CLIENT/SUBJECT USATHAMAV.O. NO. 2000-CO-24TASK DESCRIPTION Test Run #3 Heat Balance

TASK NO. \_\_\_\_\_

PREPARED BY 17 Correas DEPT 1811 DATE 21 Sep 89

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

DEPT \_\_\_\_\_ DATE \_\_\_\_\_

## Average Flash Chamber Outlet

$$1833 \text{ dscfm} \pm 3\%$$

$$482^\circ\text{F} \pm 37^\circ\text{F}$$

$$3700 \text{ wacfm}$$

$$1.26 \text{ } \% \text{ CO}_2 \text{ by vol}$$

$$17.43 \text{ } \% \text{ O}_2 \text{ by vol}$$

$$81.30 \text{ } \% \text{ N}_2 \text{ by vol}$$

$$3.83 \text{ } \% \text{ H}_2\text{O by vol}$$

$$\text{CO}_2 (1833 \text{ dscfm})(0.0126 \text{ CO}_2)(0.11378 \text{ } \frac{\text{lb}}{\text{scf}}) = 2.63 \text{ } \frac{\text{lb}}{\text{min}}$$

$$\text{O}_2 (1833 \text{ dscfm})(0.1743 \text{ O}_2)(0.0827 \text{ } \frac{\text{lb}}{\text{scf}}) = 26.42 \text{ } \frac{\text{lb}}{\text{min}}$$

$$\text{N}_2 (1833 \text{ dscfm})(0.8130 \text{ N}_2)(0.07270 \text{ } \frac{\text{lb}}{\text{scf}}) = 107.69 \text{ } \frac{\text{lb}}{\text{min}}$$

$$\text{H}_2\text{O} \quad \frac{x}{1833 + x} = .0283$$

$$x = (72.00 \text{ cfm})(.04654 \text{ } \frac{\text{lb}}{\text{scf}}) = 3.40 \text{ } \frac{\text{lb}}{\text{min}}$$

$$\text{Total exit mass flow} \quad \underline{140.34 \text{ } \frac{\text{lb}}{\text{min}}}$$

## Leakage Estimate

$$\frac{140.34 \text{ } \frac{\text{lb}}{\text{min}} - 124.80 \text{ } \frac{\text{lb}}{\text{min}}}{140.34} = 11\%$$

## Leakage Volume

$$140.34 - 124.80 = 15.54 \text{ } \frac{\text{lb}}{\text{min}}$$

# WESTERN

SHEET 6 of 11

CLIENT/SUBJECT USATHAMA W.D. NO. 7000-00-24  
 TASK DESCRIPTION Test Run #3 Heat Balance TASK NO. \_\_\_\_\_  
 PREPARED BY M. Calmes SEPT. 1911 DATE 21 Sep 89 APPROVED BY \_\_\_\_\_  
 MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_  
 METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Heat Balance Around Test Chamber

Heat Lost by Process Gas

$$\text{CO}_2 \left( \frac{2.40 + 2.63}{2} \text{ lb/min} \right) (0.225 \text{ BTU/lb}^\circ\text{F}) (1031 - 482^\circ\text{F}) = 403 \text{ BTU/min}$$

$$\text{H}_2\text{O} \left( \frac{2.51 + 3.40}{2} \text{ lb/min} \right) (0.478 \text{ BTU/lb}^\circ\text{F}) (1031 - 482^\circ\text{F}) = 775 \text{ BTU/min}$$

$$\text{N}_2 \left( \frac{95.36 + (102.89 - 27(15.54))}{2} \right) (.25 \text{ BTU/lb}^\circ\text{F}) (1031 - 482^\circ\text{F}) = 13,174 \text{ BTU/min}$$

$$\text{O}_2 \left( \frac{32.03 + (26.72 - .21(15.54))}{2} \right) (.22 \text{ BTU/lb}^\circ\text{F}) (1031 - 482^\circ\text{F}) = 2,729 \text{ BTU/min}$$

Total Heat Lost

17,081 BTU/min

Heat Absorbed by Leak Air

$$(15.54 \text{ lb/min}) (0.24 \text{ BTU/lb}^\circ\text{F}) (482 - 70^\circ\text{F}) = 1,537 \text{ BTU/min}$$

Heat Lost Through Walls

$$(17,081 \text{ BTU/min}) - (1,537 \text{ BTU/min}) = 15,544 \text{ BTU/min}$$

932,664 BTU/hr



# WESTERN

SHEET 7 of 11

CLIENT/SUBJECT USATHAM4 W.O. NO. 2000-00-24

TASK DESCRIPTION Test Run #3 Heat Balance TASK NO. \_\_\_\_\_

PREPARED BY M. Combs DEPT. 1811 DATE 21 Sep 89 APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Average Fuel Gas Pressure 6.58 psig

Average T.O. exit Gas

2000 dscfm  $\pm$  5%

1787 °F

10,700 wacfm

6.47% CO<sub>2</sub> by vol

10.83% O<sub>2</sub> by vol

82.70% N<sub>2</sub> by vol

10.07% H<sub>2</sub>O by volume

$$\text{CO}_2 (2000 \text{ dscfm}) (.0647 \text{ CO}_2) (.11378 \text{ }^{\circ}\text{B}/\text{scf}) = 14.72 \text{ }^{\circ}\text{B}/\text{min}$$

$$\text{O}_2 (2000 \text{ dscfm}) (.1083 \text{ O}_2) (.0822 \text{ }^{\circ}\text{B}/\text{scf}) = 17.92 \text{ }^{\circ}\text{B}/\text{min}$$

$$\text{N}_2 (2000 \text{ dscfm}) (.8270 \text{ N}_2) (.07246 \text{ }^{\circ}\text{B}/\text{scf}) = 119.75 \text{ }^{\circ}\text{B}/\text{min}$$

$$\text{H}_2\text{O} \frac{x}{2000 + x} = .1007$$

$$x = (224 \text{ scfm}) (.0465 \text{ }^{\circ}\text{B}/\text{scf}) = 10.42 \text{ }^{\circ}\text{B}/\text{min}$$

---


$$162.81 \text{ }^{\circ}\text{B}/\text{min}$$

Gas Flow

$$P_{\text{graph}} = (1.103)(6.58 \text{ psig})$$

$$= 7.25 \text{ psig} = 4.3 \text{ mm BTU/hr}$$

# WILSON

SHEET 3 of 11

CLIENT/SUBJECT <u>USF YAMA</u>			W.D. NO. <u>7000-00-27</u>	
TASK DESCRIPTION <u>Test Run #3 Hvac Balance</u>			TASK NO. _____	
PREPARED BY <u>M. Cosmopoulos</u>	DEPT <u>181</u>	DATE <u>2/5/89</u>	APPROVED BY _____	
MATH CHECK BY _____	DEPT _____	DATE _____	_____	
METHOD REV. BY _____	DEPT _____	DATE _____	DEPT _____	DATE _____

$$(4,800,000 \text{ minBtu/hr}) / (231.6 \text{ Btu/lb}) = 2073 \text{ scfm} \\ = 34.5 \text{ scfm}$$

$$(34.5 \text{ scfm}) (0.1196 \text{ lb/scf}) = 4.13 \text{ lb/min}$$

Air In Leakage

$$\frac{162.8 \text{ lb/min} - (140.3 \text{ lb/min} + 4.13 \text{ lb/min})}{11.32} = 18.37 \text{ lb/min}$$

Combustion Product from propane

$$\text{CO}_2 (4.13 \text{ lb/min}) (2.99 \text{ lb/lb}) = 12.35 \text{ lb/min}$$

$$\text{H}_2\text{O} (4.13 \text{ lb/min}) (1.63 \text{ lb/lb}) = 6.73 \text{ lb/min}$$

$$\text{N}_2 (4.13 \text{ lb/min}) (12.07 \text{ lb/lb}) = 49.85 \text{ lb/min}$$

$$\text{Air Consumed } (4.13 \text{ lb/min}) (15.69 \text{ lb/min}) = 64.80 \text{ lb/min Air}$$

Mass Balance Check

$$\text{CO}_2 \quad \frac{14.72 \text{ lb/min} - (12.35 \text{ lb/min} + 2.63)}{14.72 \text{ lb/min}} = -1.7\%$$

$$\text{H}_2\text{O} \quad \frac{10.42 \text{ lb/min} - (6.73 \text{ lb/min} + 3.40)}{10.42} = 2.8\%$$

$$\text{N}_2 \quad \frac{119.75 - (49.85 \text{ lb/min} + 79(14.22))}{119.75} = 2.2\%$$

# WISCON

SHEET 9 of 11

CLIENT/SUBJECT <u>USATAMA</u>			N.O. NO. <u>2000-00-24</u>	
TASK DESCRIPTION <u>Test Run #3 Heat Balance</u>			TASK NO. _____	
PREPARED BY <u>M. Colman</u>	DEPT <u>1811</u>	DATE <u>21 Sep 89</u>	APPROVED BY  _____ _____ _____ DEPT _____ DATE _____	
MATH CHECK BY _____	DEPT _____	DATE _____		
METHOD REV. BY _____	DEPT _____	DATE _____		

$$O_2 \quad \frac{(17.92 \text{ lb/min}) - (26.42 + 21(18.37) - 21(34.30))}{17.92 \text{ lb/min}} = 7.02$$

Heat Balance Check

Heat Released by Fuel

$$(4.13 \text{ lb/min}) (19,944 \text{ Btu/lb}) = 82,369 \text{ Btu/min}$$

Heat Absorbed by F.C. exit gases

$$CO_2 \quad (2.63 \text{ lb/min}) (0.225 \text{ Btu/lb}^\circ F) (1787 - 482^\circ F) = 772 \text{ Btu/min}$$

$$H_2O \quad (3.46 \text{ lb/min}) (0.478 \text{ Btu/lb}^\circ F) (1787 - 482^\circ F) = 2121 \text{ Btu/min}$$

$$N_2 \quad (107.9 \text{ lb/min}) (0.25 \text{ Btu/lb}^\circ F) (1787 - 482^\circ F) = 35,202 \text{ Btu/min}$$

$$O_2 \quad \frac{(26.42 - 21(64.30))}{(12.31 \text{ lb/min})} (0.22 \text{ Btu/lb}^\circ F) (1787 - 482^\circ F) = 3,678 \text{ Btu/min}$$

41,773 Btu/min

Heat Absorbed by Combustion Products

$$CO_2 \quad (12.35 \text{ lb/min}) (0.225 \text{ Btu/lb}^\circ F) (1787 - 70) = 4,771 \text{ Btu/min}$$

$$H_2O \quad (1.63 \text{ lb/min}) (.478 \text{ Btu/lb}^\circ F) (1787 - 70) = 1,338 \text{ Btu/min}$$

6,109 Btu/min

Heat Absorbed by Leak Air

$$Air \quad (18.37 \text{ lb/min}) (0.24 \text{ Btu/lb}^\circ F) (1787 - 70) = 7,570 \text{ Btu/min}$$

**WISCON**

CLIENT/SUBJECT USATHAMA W.O. NO. 7000-00-24 SHEET 10 of 11  
TASK DESCRIPTION Test Run #3 Heat Balance TASK NO. \_\_\_\_\_  
PREPARED BY M. Gomes DEPT. 1811 DATE 21 Sep 84 APPROVED BY \_\_\_\_\_  
MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_  
METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Radiation Losses

Surface Area

$$A = (5 \text{ ft})(20 \text{ ft}) = 314 \text{ ft}^2$$

Heat Lost

$$(314 \text{ ft}^2)(2.8 \text{ Btu/hr ft}^2 \text{ F})(300 \text{ F} - 70 \text{ F})(\% \text{ min}) = 3,372 \text{ Btu/hr}$$

Total Losses

$$(41,773 \text{ Btu/hr} + 6,109 + 7570 + 3,372) = 58,824 \text{ Btu/hr}$$

Closure Balance

$$\frac{(82,369 - 58,824)}{82,369} = 28.6\%$$

SHEET 1 of 11CLIENT/SUBJECT USATHAMAW.O. NO. 7000-00-24TASK DESCRIPTION Test Run #3 Heat Balance

TASK NO. \_\_\_\_\_

PREPARED BY M. CosmosDEPT 1211DATE 20 Sep 89

APPROVED BY

MATH CHECK BY \_\_\_\_\_

DEPT \_\_\_\_\_

DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_

DEPT \_\_\_\_\_

DATE \_\_\_\_\_

DEPT \_\_\_\_\_

DATE \_\_\_\_\_

Gas Velocity in Air Preheater

$$(18")(\pi/12inch) = 1.5 ft$$

$$\pi/4 (1.5 ft)^2 = 1.767 ft^2$$

$$(5533 acfm) / 1.767 ft^2 = 3131 fpm$$

Gas Velocity in After Burner

$$\pi/4 (5 ft)^2 = 19.63 ft^2$$

$$(10,700 acfm) / 19.63 ft^2 = 545 fpm$$

Assuming same size

$$5533 acfm / 545 fpm = 10 ft^2$$

$$10 ft^2 = (\pi/4)(x ft)^2$$

$$x = 3.6 ft \varnothing$$



SHEET 1 of 10

CLIENT/SUBJECT USATHAM AW.O. NO. 7000-00-27TASK DESCRIPTION Test Run #5 Heat Balance

TASK NO. \_\_\_\_\_

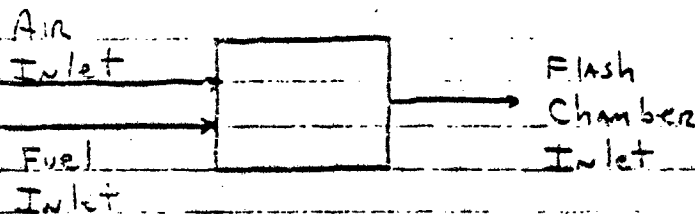
PREPARED BY M. Collins DEPT. 1911 DATE 16 Feb 70

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Average Inlet Air Flow  $P_{I202}$   $1.11 \pm .16$  mwgAverage Gas Pressure  $P_{I310}$   $2.47 \pm .61$  psig

Average Flash Chamber Inlet

1533 dscfm  $\pm 3.3\%$ 

936 °F (

4700 acfm

1.9 %  $CO_2$ 16.9 %  $O_2$ 81.2 %  $N_2$ 3.0 %  $H_2O$ 

$$CO_2 (1533 \text{ dscfm}) (0.019) (.11378^{15}/ft^3) = 3.31^{15}/min$$

$$O_2 (1533 \text{ dscfm}) (.0169) (.08275^{15}/ft^3) = 2.144^{15}/min$$

$$N_2 (1533 \text{ dscfm}) (.812) (.07240^{15}/ft^3) = 90.12^{15}/min$$

$$H_2O \quad X \quad .020$$

$$1533 + X$$

$$X = (47.41 \text{ acfm}) (.041654^{15}/ft^3) = 2.21^{15}/min$$

$$117.08^{15}/min$$

# WISSEN

SHEET 2 of 10

CLIENT/SUBJECT USATHAMAW.O. NO. 7000-00-24TASK DESCRIPTION Test Run T-5 Heat BalanceTASK NO. 2PREPARED BY M. Cosmos DEPT 1311 DATE 16 Feb 90

APPROVED BY

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

DEPT \_\_\_\_\_ DATE \_\_\_\_\_

Correction to Gas Flow An Altitude

$$\text{correction} = e (0.0000360286 (4500 \text{ ft})) = 1.176$$

$$\text{design loc} = e (0.0000360286 (1750 \text{ ft})) = 1.066$$

$$\text{density ratio} = 1.176 / 1.066 = 1.103$$

$$P_{\text{graph}} = (\text{Density ratio}) (P_{\text{act}})$$

$$= 1.103 (2.47 \text{ psig}) =$$

$$= 2.72 \text{ psig}$$

$$\text{From vendor graph } 802 \quad 2.72 \text{ psig} = 2.0 \text{ min air/hm}$$

$$(2,000,000 \text{ scfm/hm}) / 2316 \text{ scf} =$$

$$863 \text{ scfh} = 14.39 \text{ scfm of propane}$$

$$(14.39 \text{ scfm}) (0.1196 \text{ lb/scf}) = 1.72 \text{ lb/min}$$

Combustion Air Flow

$$\text{Flow} = 1433 + 406 (\ln (1.11 \text{ mos})) = 1475 \text{ scfm}$$

$$(1475 \text{ scfm}) (0.075 \text{ lb/scf}) = 108.7 \text{ lb/min}$$

moisture loadings under worst observed

$$\text{conditions } 60^\circ \text{F} = 0.01 \text{ lb/h}_2\text{O / lb d.a.}$$

# WESTERN

SHEET 3 of 11

CLIENT/SUBJECT USATHAMA W.O. NO. 7000-00-24  
 TASK DESCRIPTION Test Run T-5 Heat Balance TASK NO. 2  
 PREPARED BY M. Cosmos DEPT. 1311 DATE 16 Feb 90 APPROVED BY \_\_\_\_\_  
 MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_  
 METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Maximum water Load

$$(108.7 \text{ lb/min}) (0.01 \text{ lb H}_2\text{O/lb gas}) = 1.08 \text{ lb H}_2\text{O}$$

Mass Balance Check

$$\frac{117.08 \text{ lb/min} - (1.72 \text{ lb/min gas} + 108.7 \text{ lb/min} + 1.08 \text{ lb/min})}{117.08 \text{ lb/min}}$$

4.772 closure w. this measurement error

Combustion of Propane

CO <sub>2</sub>	2.99	lb/lb gas
H <sub>2</sub> O	1.63	lb/lb gas
N <sub>2</sub>	12.07	lb/lb gas
Total	16.69	lb/lb gas = 15.69 $\frac{\text{lb air}}{\text{lb gas}}$

Combustion of Fuel

$$\begin{aligned} \text{CO}_2 & (1.72 \text{ lb/min}) (2.99 \text{ lb/lb}) = 5.14 \text{ lb/min} \\ \text{H}_2\text{O} & (1.72 \text{ lb/min}) (1.63 \text{ lb/lb}) + 1.08 \text{ lb/min} = 3.88 \text{ lb/min} \\ \text{N}_2 & (1.72 \text{ lb/min}) (12.07 \text{ lb/lb}) = 20.76 \text{ lb/min} \end{aligned}$$

Excess Air

$$(108.7 \text{ lb/min}) - (1.72 \text{ lb/min}) (15.69 \text{ lb/lb}) = 81.71 \text{ lb/min XS Air}$$

$$\text{O}_2 \text{ in XS Air} = (81.71 \text{ lb/min}) (.21) = 17.16 \text{ lb/min}$$



WILSON

SHEET 4 of 11

CLIENT/SUBJECT USATHAIA W.O. NO. 7000-00-24

TASK DESCRIPTION Test Run T-5 Heat Balance TASK NO. 2

PREPARED BY M. Casmas DEPT. 1811 DATE 16 Feb 90

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT	DATE

## Heat Balance

### Heat Released by Fuel

$$(1.72 \text{ lb/min}) (19,944 \text{ Btu/lb}) = 34,303 \text{ Btu/min}$$

### Heat Absorbed by Combustion Products

$$\text{CO}_2 (5.14 \text{ lb/min}) (0.225 \text{ Btu/lb}^\circ\text{F}) (936^\circ\text{F} - 70^\circ\text{F}) = 1002 \text{ Btu/min}$$

$$\text{H}_2\text{O} (3.88 \text{ lb/min}) (0.478 \text{ Btu/lb}^\circ\text{F}) (936 - 70^\circ\text{F}) = 1,606 \text{ Btu/min}$$

$$\text{N}_2 (20.76 \text{ lb/min}) (0.25 \text{ Btu/lb}^\circ\text{F}) (936 - 70^\circ\text{F}) = 4495 \text{ Btu/min}$$

$$\text{xs Air} (81.71 \text{ lb/min}) (0.24 \text{ Btu/lb}^\circ\text{F}) (936 - 70^\circ\text{F}) = 16,983 \text{ Btu/min}$$

$$\text{Total} \quad 24,086 \text{ Btu/min}$$

### Radiation Losses

$$\pi (20 \text{ inches}) \left(\frac{1}{12} \text{ inch}\right) (6.5 \text{ ft} + 24.5 \text{ ft}) = 162 \text{ ft}^2$$

$$(162 \text{ ft}^2) (2.8 \text{ Btu/hr ft}^2^\circ\text{F}) (300 - 70^\circ\text{F}) \left(\frac{\text{hr}}{60 \text{ min}}\right) = 1,742 \text{ Btu/min}$$

### Heat Balance Comparison

$$\frac{(34,303 \text{ Btu/min}) - (24,086 \text{ Btu/min} + 1,742)}{34,303 \text{ Btu/min}} = 24.7\%$$

# WISLEN

SHEET 5 of 10

CLIENT/SUBJECT USATHAMA W.O. NO. 7000-00-24

TASK DESCRIPTION Test Run T-5 Heat Balance TASK NO. 2

PREPARED BY M. Cosmos DEPT. 1711 DATE 16 Feb 90

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT. _____	DATE _____

## Average Flash Chamber Outlet

2033 dscfm  $\pm 5\%$   
 456 °F  $\pm 70\text{°F}$   
 4133 Acfm  
 1.52 CO<sub>2</sub>  
 17.72 O<sub>2</sub>  
 80.92 N<sub>2</sub>  
 2.92 H<sub>2</sub>O

$$\text{CO}_2 (2033 \text{ dscfm}) (0.15 \text{ CO}_2) (0.11378 \text{ }^{15}\text{cf}) = 3.47 \text{ }^{15}\text{min}$$

$$\text{O}_2 (2033 \text{ dscfm}) (0.177 \text{ O}_2) (0.0827 \text{ }^{15}\text{cf}) = 29.76 \text{ }^{15}\text{min}$$

$$\text{N}_2 (2033 \text{ dscfm}) (0.809 \text{ N}_2) (0.072 \text{ }^{15}\text{cf}) = 118.42 \text{ }^{15}\text{min}$$

$$\frac{\text{H}_2\text{O} \quad X}{2033 + X} = 0.029$$

$$X = (60.71 \text{ scfm}) (0.04654 \text{ }^{15}\text{scf}) = 2.83 \text{ }^{15}\text{min}$$

Total Exit Gas Mass Flow 154.48 <sup>15</sup>/min

## Leakage Estimate

$$\frac{154.48 \text{ }^{15}\text{min} - 117.08 \text{ }^{15}\text{min}}{154.48 \text{ }^{15}\text{min}} = 24.2\%$$

## Leakage Volume

$$154.48 \text{ }^{15}\text{min} - 117.08 \text{ }^{15}\text{min} = 37.4 \text{ }^{15}\text{min}$$

# WILSON

SHEET 6 of 10

CLIENT/SUBJECT USAT4AM3 W.O. NO. 2000-00-27

TASK DESCRIPTION Test Run T-5 Heat Balance TASK NO. 2

PREPARED BY M. Cosmos DEPT 1811 DATE 16 Feb 90 APPROVED BY

MATH CHECK BY DEPT DATE

METHOD REV. BY DEPT DATE

Heat Balance Around Flash Chamber

Heat Lost by Process Gas

$$\text{CO}_2 \left( \frac{3.31 + 3.47}{2} \right) (0.225 \text{ gm/lb} \cdot \text{F}) (936 - 456 \text{ F}) = 366 \frac{\text{BTU}}{\text{min}}$$

$$\text{H}_2\text{O} \left( \frac{2.21 + 2.23}{2} \right) (0.478 \text{ gm/lb} \cdot \text{F}) (936 - 456 \text{ F}) = 578 \frac{\text{BTU}}{\text{min}}$$

$$\text{N}_2 \left( \frac{20.12 + (114.42 - .79(37.7))}{2} \right) (0.25 \text{ gm/lb} \cdot \text{F}) (936 - 456 \text{ F}) = 10,740 \frac{\text{BTU}}{\text{min}}$$

$$\text{O}_2 \left( \frac{21.44 + (29.76 - .21(37.7))}{2} \right) (0.24 \text{ gm/lb} \cdot \text{F}) (936 - 456 \text{ F}) = 2,497 \frac{\text{BTU}}{\text{min}}$$

$$\text{Total Heat Lost by Gas} = 14,181 \frac{\text{BTU}}{\text{min}}$$

Heat Absorbed by Leak Air

$$(37.7 \text{ lb/min}) (0.24 \text{ gm/lb} \cdot \text{F}) (456 - 70 \text{ F}) = 3465 \frac{\text{BTU}}{\text{min}}$$

Heat Lost Through Walls

$$(14,181 \frac{\text{BTU}}{\text{min}}) - 3465 \frac{\text{BTU}}{\text{min}} = 10,716 \frac{\text{BTU}}{\text{min}}$$

$$= 642,976 \frac{\text{BTU}}{\text{hr}}$$



CLIENT/SUBJECT USATITAMA SHEET 7 of 13  
H.O. NO. 7000-00-24  
TASK DESCRIPTION Test Run T-5 Heat Balance TASK NO. \_\_\_\_\_  
PREPARED BY M. Cosmos DEPT 1811 DATE 24 Feb 90 APPROVED BY \_\_\_\_\_  
MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_  
METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

Average Fuel Gas Pressure 6.26 psig ± .59

Average T.O. Exit Gas

2467 dscfm

1706 °F

12.617 acfm

6.3 % CO<sub>2</sub>

10.8 % O<sub>2</sub>

82.9 % N<sub>2</sub>

8.7 % H<sub>2</sub>O

$$\text{CO}_2 (2467 \text{ dscfm}) (.063) (.11378 \text{ lb/dscf}) = 17.7 \text{ lb/min}$$

$$\text{O}_2 (2467 \text{ dscfm}) (.108 \text{ O}_2) (.08275 \text{ lb/dscf}) = 22.0 \text{ lb/min}$$

$$\text{N}_2 (2467 \text{ dscfm}) (.829 \text{ N}_2) (.07276 \text{ lb/dscf}) = 148.1 \text{ lb/min}$$

$$\text{H}_2\text{O} \frac{x}{2467 + x} = .084$$

$$x = (226 \text{ cfm}) (.04654 \text{ lb/dscf}) = 10.53 \text{ lb/min}$$

$$198.3 \text{ lb/min}$$

Gas Flow

$$P_{\text{graph}} = (1.103)(6.26 \text{ psig})$$

$$6.90 \text{ psig} = 4,500,000 \text{ BTU/hr}$$

# WASTEN

SHEET 9 of 10

CLIENT/SUBJECT USATHSMA W.O. NO. 2440-00-21

TASK DESCRIPTION Test Run T-5 Heat Balance TASK NO. \_\_\_\_\_

PREPARED BY M. G. Smith DEPT 1811 DATE 24 Feb 90 APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

$$(4,500,000 \text{ BTU/hr}) / (2316 \text{ BTU/scf}) = 1943 \text{ scfh}$$

$$= 32.4 \text{ scfm}$$

$$(32.4 \text{ scfm})(0.1196 \text{ lb/scf}) = 3.87 \text{ lb/min}$$

Air Leakage

$$198.3 \text{ lb/min} - (154.5 \text{ lb/min} + 3.87 \text{ lb/min}) = 39.9 \text{ lb/min}$$

$$= 20.1 \%$$

Combustion Products

$$\text{CO}_2 (3.87 \text{ lb/min})(2.99 \text{ lb/lb}) = 11.57 \text{ lb/min}$$

$$\text{H}_2\text{O} (3.87 \text{ lb/min})(1.63 \text{ lb/lb}) = 6.31 \text{ lb/min}$$

$$\text{N}_2 (3.87 \text{ lb/min})(12.07 \text{ lb/lb}) = 46.71 \text{ lb/min}$$

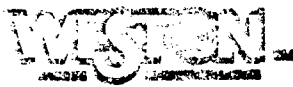
$$\text{Air Consumed} (3.87 \text{ lb/min})(15.69 \text{ lb/lb}) = 60.72 \text{ lb/min}$$

Mass Balance check

$$\text{CO}_2 \quad \frac{17.7 \text{ lb/min} - (11.57 \text{ lb/min} + 3.47 \text{ lb/min})}{17.7 \text{ lb/min}} = 15.6 \%$$

$$\text{H}_2\text{O} \quad \frac{20.53 \text{ lb/min} - (6.31 \text{ lb/min} + 2.83 \text{ lb/min})}{20.53 \text{ lb/min}} = 13.2 \%$$

$$\text{N}_2 \quad \frac{148.1 \text{ lb/min} - (11.812 \text{ lb/min} + 79(39.9 \text{ lb/min}))}{148.1 \text{ lb/min}} = -1.2 \%$$

SHEET 9 of 10CLIENT/SUBJECT USATHAMAW.O. NO. 7030-100-24TASK DESCRIPTION Test Run #5 Heat Balance

TASK NO. \_\_\_\_\_

PREPARED BY M. Cosmos DEPT. 1811 DATE 24 Feb 90

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

$$O_2 \quad 22.0 \text{ lb/min} - (29.76 \text{ lb/min} + .21(39.9 \text{ lb/min}) - .21(60.72 \text{ lb/min}))$$

$$22.0 \text{ lb/min}$$

$$= -15.4\%$$

Heat Balance Check

Heat Released by Fuel

$$(3.87 \text{ lb/min})(19,994 \text{ BTU/lb}) = 77,378 \text{ BTU/min}$$

Heat Absorbed by F.C. Exit Gases

$$CO_2 \quad (3.47 \text{ lb/min})(0.225 \text{ BTU/lb}^\circ\text{F})(1706 - 456^\circ\text{F}) = 976 \frac{\text{BTU}}{\text{min}}$$

$$H_2O \quad (2.83 \text{ lb/min})(0.478 \text{ BTU/lb}^\circ\text{F})(1706 - 456^\circ\text{F}) = 1,691 \frac{\text{BTU}}{\text{min}}$$

$$N_2 \quad (118.42 \text{ lb/min})(0.25 \text{ BTU/lb}^\circ\text{F})(1706 - 456^\circ\text{F}) = 37,006$$

$$O_2 \quad (29.76 \text{ lb/min} - .21(60.72))(0.22 \text{ BTU/lb}^\circ\text{F})(1706 - 456^\circ\text{F}) = 4677$$

$$44,350 \frac{\text{BTU}}{\text{min}}$$

Heat Absorbed by Combustion Products

$$CO_2 \quad (11.57 \text{ lb/min})(0.225 \text{ BTU/lb}^\circ\text{F})(1706 - 456^\circ\text{F}) = 3254 \frac{\text{BTU}}{\text{min}}$$

$$H_2O \quad (6.31 \text{ lb/min})(0.478 \text{ BTU/lb}^\circ\text{F})(1706 - 456^\circ\text{F}) = 3776 \frac{\text{BTU}}{\text{min}}$$

$$7024 \frac{\text{BTU}}{\text{min}}$$

Heat Balance

$$Air \quad (39.9 \text{ lb/min})(0.24 \text{ BTU/lb}^\circ\text{F})(1706 - 70^\circ\text{F}) = 15,666 \frac{\text{BTU}}{\text{min}}$$

**WESTERN**

SHEET 10 of 10

CLIENT/SUBJECT USAF/AMA W.O. NO. 7000-00-27

TASK DESCRIPTION Test Run #5 Heat Balance TASK NO. \_\_\_\_\_

PREPARED BY M. C. Jones DEPT. 121 DATE 24 Feb 90 APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Radiation Losses

Surface Area  $m(5 ft)(20 ft) = 314 ft^2$

Heat Losses

$(314 ft^2)(2.8 \frac{Btu}{hr ft^2 F})(300-70 F)(\frac{hr}{min}) = 3370 \frac{Btu}{min}$

Total Heat Losses

$(44,350 \frac{Btu}{min} + 7024 + 15,666 + 3370) = 70,410 \frac{Btu}{min}$

Closure Balance

$(77,183 \frac{Btu}{min} - 70,410 \frac{Btu}{min}) = 6773$

77,183 Btu/min



SHEET \_\_\_\_\_ of \_\_\_\_\_

CLIENT/SUBJECT \_\_\_\_\_ W.O. NO. \_\_\_\_\_

TASK DESCRIPTION \_\_\_\_\_ TASK NO. \_\_\_\_\_

PREPARED BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

APPROVED BY	
DEPT. _____	DATE _____

Heat Transfer Calculations

Test Runs 1

2, 3, 4 5



SHEET 1 of 5CLIENT/SUBJECT USATHAMAW.O. NO. 7000-00-24TASK DESCRIPTION Insulation Calculations for Flash Chamber TASK NO. Set IIPREPARED BY M. Cosmos DEPT. 1811 DATE \_\_\_\_\_

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

Calculated Heat Losses from chamber Test 3T<sub>gas inlet</sub> = 947.3 data from thermocouplesT<sub>gas outlet</sub> = 527.7Average Gas Temperature = 737.5 °FWall TemperaturesRear Wall 416.5Rear Floor 350.8Roof 527.7Left Wall 524.6Floor 335.7Middle Wall 361.9Average 419.5 ± 87 °FHeat Transfer from Gas to Wall = Q<sub>GW</sub>

$$Q_{GW} = U_g A \Delta T_{GW}$$

Heat Transfer in Wall = Q<sub>W</sub>

$$Q_{W} = U_w A \Delta T_{W}$$



SHEET 2 of 5

CLIENT/SUBJECT USATHAMAW.O. NO. 7000-00-24TASK DESCRIPTION Insulation Calculations

TASK NO. \_\_\_\_\_

PREPARED BY M. Camos DEPT. IRI DATE 24 Feb 90

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

DEPT. \_\_\_\_\_ DATE \_\_\_\_\_

$$A = \pi D L + 2 \left[ \pi \frac{D^2}{4} \right]$$

$$= \pi (12.5 \text{ ft}) (35 \text{ ft}) + 2 \left[ \pi \frac{(12.5 \text{ ft})^2}{4} \right]$$

$$= 1620 \text{ ft}^2 \text{ inside surface area}$$

$$Q = 932,664 \frac{\text{BTU}}{\text{hr}} = U_6 (1620 \text{ ft}^2) (737 - 420^\circ \text{F})$$

$$U_{6w} = 1.82 \text{ BTU/hr ft}^2 \text{ } ^\circ \text{F}$$

Calculations Composite Bldg Resistance

$$Q = 932,664 \frac{\text{BTU}}{\text{hr}} = \frac{h_a A_m}{L_a} (420 - 70^\circ \text{F})$$

$$A_m = \pi D_{avg} L + 2 \left[ \pi \frac{D^2}{4} \right]$$

$$= \pi [(12.5 + 21) / 2] (35 \text{ ft}) + 2$$

$$= 1842 \text{ ft}^2 + 245 \text{ ft}^2$$

$$= 2087 \text{ ft}^2$$

$$L_a = (D_o + D_i) / 2$$

$$= (21.0 - 12.5 \text{ ft}) / 2 = 4.25 \text{ ft}$$

$$932,664 \frac{\text{BTU}}{\text{hr}} = \frac{h_a (2087 \text{ ft}^2) (420 - 70^\circ \text{F})}{4.25 \text{ ft}}$$

$$h_a = 5.43 \text{ BTU/hr ft}^2 \text{ (F/A)}$$

Combine conductivity of building

SHEET 3 of 5CLIENT/SUBJECT USATHAMAW.O. NO. 7000-00-27TASK DESCRIPTION Insulation Calculation

TASK NO. \_\_\_\_\_

PREPARED BY M. Cosmos DEPT 1811 DATE 24 Feb 90

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

DEPT \_\_\_\_\_ DATE \_\_\_\_\_

Calculated Heat Losses from Flash Chamber Test 2T<sub>gas inlet</sub> = 733 °FT<sub>gas outlet</sub> = 391 °FAverage Gas Temperature =  $\frac{733+391}{2} = 562 °F$ Wall TemperaturesRear Wall 267Rear Floor 255Roof 314Left Wall 397Right Floor 212Front Wall 271Average 286 ± 63 °FHeat Transfer To Wall from Gas $Q = U_{gas} A_{wall} (\Delta T)$  $594,202 \text{ Btu/hr} = U (1620 \text{ ft}^2) (562 °F - 216 °F)$  $U = 1.33 \text{ Btu/hr ft}^2 °F$  $594,202 \text{ Btu/hr} = h_c (2087 \text{ ft}^2) (286 - 70 °F)$  $4.25 \text{ ft}^2$  $h_c = 5.60 \text{ Btu/hr ft}^2 (°F/ft)$



SHEET 24 of 5

CLIENT/SUBJECT USATHAMAW.O. NO. 7000-00-27TASK DESCRIPTION Insulation Calculation

TASK NO. \_\_\_\_\_

PREPARED BY M. Gismos DEPT 1611 DATE 24 Feb 90

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_ DATE \_\_\_\_\_

DEPT \_\_\_\_\_ DATE \_\_\_\_\_

Calculated Heat Losses from Flash Chamber T-5T<sub>gas Inlet</sub> = 893 °FT<sub>gas Outlet</sub> = 535 °FAverage Gas Temperature = 714 °FWall TemperaturesRear Floor 392 °FRear wall 408Right Floor 340Left Wall 540Roof 548Middle Wall 361Front Wall 343Average 376 ± 163 °FHeat Transfer To Wall From GasQ = U<sub>gas</sub> A<sub>gas</sub> ΔT642,976 Btu/hr = U<sub>gas</sub> (1620 ft<sup>2</sup>) (714 - 376 °F)U<sub>gas</sub> = 1.17 Btu/hr ft<sup>2</sup> °F642,976 Btu/hr = h<sub>a</sub> (2087 ft<sup>2</sup>) (376 - 70 °F)  
4.25 ft<sup>2</sup>h<sub>a</sub> = 4.28 Btu/hr ft<sup>2</sup> (°F/ft)

SHEET 5 of 5CLIENT/SUBJECT USATHAMAW.O. NO. 7000-00-24TASK DESCRIPTION Insulation Calculations

TASK NO. \_\_\_\_\_

PREPARED BY M. Cosmas DEPT 1891DATE 24 Feb 90

APPROVED BY \_\_\_\_\_

MATH CHECK BY \_\_\_\_\_ DEPT \_\_\_\_\_

DATE \_\_\_\_\_

METHOD REV. BY \_\_\_\_\_ DEPT \_\_\_\_\_

DATE \_\_\_\_\_

DEPT \_\_\_\_\_ DATE \_\_\_\_\_

Test T-2

Gas Velocity in Chamber

$$(4400 \text{ wcfm} + 3917 \text{ wcfm})/2 = 4159 \text{ wcfm}$$

$$Area = \pi D^2 / 4 = \pi (12.5 \text{ ft})^2 / 4 = 123 \text{ ft}^2$$

$$velocity = 4159 / 123 \text{ ft}^2 = 33.9 \text{ fpm}$$

Test T-3

$$(5532 \text{ wcfm} + 3900 \text{ wcfm})/2 = 4717 \text{ wcfm}$$

$$velocity = 4717 \text{ wcfm} / 123 \text{ ft}^2 = 38.3 \text{ fpm}$$

Test T-5

$$(4700 \text{ wcfm} + 4133 \text{ wcfm})/2 = 4417 \text{ wcfm}$$

$$velocity = 4417 \text{ wcfm} / 123 \text{ ft}^2 = 35.9 \text{ fpm}$$